COMUNE di MONTELUPONE

PROVINCIA DI MACERATA

RIQUALIFICAZIONE CAMPO DI CALCIO COMUNALE
REALIZZAZIONE NUOVI SPOGLIATOI
sito in via Alessandro Manzoni - Montelupone (MC)

PROGETTO ESECUTIVO

STATO DI PROGETTO - EDIFICIO SPOGLIATOI

TABULATO DI CALCOLO DELLA STRUTTURA

COMMITTENTE: **COMUNE DI MONTELUPONE**

Il Sindaco
ROLANDO PECORA

Il RUP
ANTONIO SPACCESI

PROGETTISTA: **Ing. GIACOMO COMITE**
iscritto albo Ing. FERMO n. A323

TAVOLA **B.2.f**		Integrazione AGOSTO 2022

4Ex.Ex.Sys. Wind^{mass}

Structural Analysis & Design

Wind^{mass}

Sia Wind^{mass} s.r.l. - Via Tiziano 41 - Cuneo(No di Reno Bologna)

Info Sys

Windmass

Piattaforma software

Microsoft Windows Vista, Microsoft Windows XP Home Professional

Requisiti minimi hw per

Microsoft Vista - Microsoft Vista

Caratteristiche sw

Caratteristiche e dimensioni di sistema in campo elastico lineare.

Elementi finiti implementati

- Trave
- Trave elastoplastica di Tipo I-Plastic
- Trave di Tipo Elastoplastico
- Elementi Shell di Tipo Elastico
- Elementi Shell di Tipo Elastoplastico
- Elementi Shell di Tipo Elastoplastico
- Elementi Impalcato a Piastra Shell (piano piastra)

Elementi di Carico

- Carichi nodali concentrati
- Carichi distribuiti su elementi trave
- Carichi Ingegneristici

Tipi di Analisi

- Analisi di Equilibrio Elastico in campo lineare con e senza deformabilità.
- Analisi Modale
- Analisi Sismica Dinamica
  - Analisi(sismica generica o per di Banchi per Italia)
  - Analisi(sismica generica o per di Banchi per Italia) con Carichi Ingegneristici
- Analisi dinamica, dato caso di carico impulsivo di accelerazioni (utilizzato nazioni (utilizzato nazioni (utilizzato n

►Combinazioni agli Stati Limite di Collasso

Combinazione di carico numero

1	Vento SLU
2	Vento SLU
3	Vento SLU
4	Vento SLU
5	Vento SLU
6	Vento SLU
7	Vento SLU
8	Vento SLU

Code Grad	γ_{G1}	γ_{G2}	γ_{Q1}	γ_{Q2}	γ_{Q3}	γ_{Q4}	γ_{Q5}	γ_{Q6}
1.0 G	1.3	1.5	1.5	0.0	0.0	0.0	0.0	0.0

| | | |

▶Direzione di ingresso del Sisma 3 Angolo 165.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 3 Angolo 165.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 4 Angolo 275.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 4 Angolo 275.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 5 Angolo 0.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 5 Angolo 0.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 6 Angolo 90.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 6 Angolo 90.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 7 Angolo 165.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 7 Angolo 165.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 8 Angolo 275.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 8 Angolo 275.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 9 Angolo 0.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 9 Angolo 0.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 10 Angolo 90.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 10 Angolo 90.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 11 Angolo 165.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 11 Angolo 165.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Direzione di ingresso del Sisma 12 Angolo 275.00

▶Coefficienti di partecipazione e massa modali efficaci per i vari modi di vibrare:

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

Direzione di ingresso del Sisma 12 Angolo 275.00 [1]

Modo	Lambda	Ex [%]	Ey [%]	Ex cum. [%]	Ey cum. [%]
1	0.0000E+00	0.00	0.00	0.00	0.00
2	0.0000E+00	0.00	0.00	0.00	0.00
3	0.0000E+00	0.00	0.00	0.00	0.00
4	0.0000E+00	0.00	0.00	0.00	0.00
5	0.0000E+00	0.00	0.00	0.00	0.00
6	0.0000E+00	0.00	0.00	0.00	0.00
7	0.0000E+00	0.00	0.00	0.00	0.00
8	0.0000E+00	0.00	0.00	0.00	0.00
9	0.0000E+00	0.00	0.00	0.00	0.00
10	0.0000E+00	0.00	0.00	0.00	0.00
11	0.0000E+00	0.00	0.00	0.00	0.00
12	0.0000E+00	0.00	0.00	0.00	0.00
Ex: Sisma direzione X					
Ey: Sisma direzione Y					

▶Spostamenti nodali

▶Direzione sisma:

- la terna di riferimento generale è destrorsa per cui si hanno i seguenti segni positivi per le componenti di spostamento nodale:

- per quanto riguarda le rotazioni:

Nei singoli singolo riportate, per ogni nodo sono riportate del nodo il tipo dell'incrocio (incrociamento, tirato, aperto o parziale, quando esistono), l'asta corrispondente di appartenenza, le componenti di spostamento e le componenti di rotazione.

Nodo	Caso	Dx	Dy	Dz	Rx	Ry	Rz
1	1	0.00	0.00	0.00	0.00	0.00	0.00
2	1	0.00	0.00	0.00	0.00	0.00	0.00
3	1	0.00	0.00	0.00	0.00	0.00	0.00
4	1	0.00	0.00	0.00	0.00	0.00	0.00
5	1	0.00	0.00	0.00	0.00	0.00	0.00
6	1	0.00	0.00	0.00	0.00	0.00	0.00
7	1	0.00	0.00	0.00	0.00	0.00	0.00
8	1	0.00	0.00	0.00	0.00	0.00	0.00
9	1	0.00	0.00	0.00	0.00	0.00	0.00
10	1	0.00	0.00	0.00	0.00	0.00	0.00
11	1	0.00	0.00	0.00	0.00	0.00	0.00
12	1	0.00	0.00	0.00	0.00	0.00	0.00
13	1	0.00	0.00	0.00	0.00	0.00	0.00
14	1	0.00	0.00	0.00	0.00	0.00	0.00
15	1	0.00	0.00	0.00	0.00	0.00	0.00
16	1	0.00	0.00	0.00	0.00	0.00	0.00
17	1	0.00	0.00	0.00	0.00	0.00	0.00
18	1	0.00	0.00	0.00	0.00	0.00	0.00
19	1	0.00	0.00	0.00	0.00	0.00	0.00
20	1	0.00	0.00	0.00	0.00	0.00	0.00
21	1	0.00	0.00	0.00	0.00	0.00	0.00
22	1	0.00	0.00	0.00	0.00	0.00	0.00
23	1	0.00	0.00	0.00	0.00	0.00	0.00
24	1	0.00	0.00	0.00	0.00	0.00	0.00
25	1	0.00	0.00	0.00	0.00	0.00	0.00
26	1	0.00	0.00	0.00	0.00	0.00	0.00
27	1	0.00	0.00	0.00	0.00	0.00	0.00
28	1	0.00	0.00	0.00	0.00	0.00	0.00
29	1	0.00	0.00	0.00	0.00	0.00	0.00
30	1	0.00	0.00	0.00	0.00	0.00	0.00
31	1	0.00	0.00	0.00	0.00	0.00	0.00
32	1	0.00	0.00	0.00	0.00	0.00	0.00
33	1	0.00	0.00	0.00	0.00	0.00	0.00
34	1	0.00	0.00	0.00	0.00	0.00	0.00
35	1	0.00	0.00	0.00	0.00	0.00	0.00
36	1	0.00	0.00	0.00	0.00	0.00	0.00
37	1	0.00	0.00	0.00	0.00	0.00	0.00
38	1	0.00	0.00	0.00	0.00	0.00	0.00
39	1	0.00	0.00	0.00	0.00	0.00	0.00
40	1	0.00	0.00	0.00	0.00	0.00	0.00
41	1	0.00	0.00	0.00	0.00	0.00	0.00
42	1	0.00	0.00	0.00	0.00	0.00	0.00
43	1	0.00	0.00	0.00	0.00	0.00	0.00
44	1	0.00	0.00	0.00	0.00	0.00	0.00
45	1	0.00	0.00	0.00	0.00	0.00	0.00
46	1	0.00	0.00	0.00	0.00	0.00	0.00
47	1	0.00	0.00	0.00	0.00	0.00	0.00
48	1	0.00	0.00	0.00	0.00	0.00	0.00

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	6	0.36	0.40	0.42	0.38	0.38	0.40
	7	0.38	0.40	0.42	0.38	0.38	0.40
	8	0.38	0.40	0.42	0.38	0.38	0.40
	9	0.38	0.40	0.42	0.38	0.38	0.40
	10	0.38	0.40	0.42	0.38	0.38	0.40
	11	0.38	0.40	0.42	0.38	0.38	0.40
	12	0.38	0.40	0.42	0.38	0.38	0.40
	13	0.38	0.40	0.42	0.38	0.38	0.40
	14	0.38	0.40	0.42	0.38	0.38	0.40
	15	0.38	0.40	0.42	0.38	0.38	0.40
	16	0.38	0.40	0.42	0.38	0.38	0.40
	17	0.38	0.40	0.42	0.38	0.38	0.40
	18	0.38	0.40	0.42	0.38	0.38	0.40
	19	0.38	0.40	0.42	0.38	0.38	0.40
	20	0.38	0.40	0.42	0.38	0.38	0.40
	21	0.38	0.40	0.42	0.38	0.38	0.40
	22	0.38	0.40	0.42	0.38	0.38	0.40
	23	0.38	0.40	0.42	0.38	0.38	0.40
	24	0.38	0.40	0.42	0.38	0.38	0.40
	25	0.38	0.40	0.42	0.38	0.38	0.40
	26	0.38	0.40	0.42	0.38	0.38	0.40
	27	0.38	0.40	0.42	0.38	0.38	0.40
	28	0.38	0.40	0.42	0.38	0.38	0.40
	29	0.38	0.40	0.42	0.38	0.38	0.40
	30	0.38	0.40	0.42	0.38	0.38	0.40
	31	0.38	0.40	0.42	0.38	0.38	0.40
	32	0.38	0.40	0.42	0.38	0.38	0.40
	33	0.38	0.40	0.42	0.38	0.38	0.40
	34	0.38	0.40	0.42	0.38	0.38	0.40
	35	0.38	0.40	0.42	0.38	0.38	0.40
	36	0.38	0.40	0.42	0.38	0.38	0.40
	37	0.38	0.40	0.42	0.38	0.38	0.40
	38	0.38	0.40	0.42	0.38	0.38	0.40
	39	0.38	0.40	0.42	0.38	0.38	0.40
	40	0.38	0.40	0.42	0.38	0.38	0.40
	41	0.38	0.40	0.42	0.38	0.38	0.40
	42	0.38	0.40	0.42	0.38	0.38	0.40
	43	0.38	0.40	0.42	0.38	0.38	0.40
	44	0.38	0.40	0.42	0.38	0.38	0.40
	45	0.38	0.40	0.42	0.38	0.38	0.40
	46	0.38	0.40	0.42	0.38	0.38	0.40
	47	0.38	0.40	0.42	0.38	0.38	0.40
	48	0.38	0.40	0.42	0.38	0.38	0.40
	49	0.38	0.40	0.42	0.38	0.38	0.40
	50	0.38	0.40	0.42	0.38	0.38	0.40
	51	0.38	0.40	0.42	0.38	0.38	0.40
	52	0.38	0.40	0.42	0.38	0.38	0.40
	53	0.38	0.40	0.42	0.38	0.38	0.40
	54	0.38	0.40	0.42	0.38	0.38	0.40
	55	0.38	0.40	0.42	0.38	0.38	0.40
	56	0.38	0.40	0.42	0.38	0.38	0.40
	57	0.38	0.40	0.42	0.38	0.38	0.40
	58	0.38	0.40	0.42	0.38	0.38	0.40
	59	0.38	0.40	0.42	0.38	0.38	0.40
	60	0.38	0.40	0.42	0.38	0.38	0.40
	61	0.38	0.40	0.42	0.38	0.38	0.40
	62	0.38	0.40	0.42	0.38	0.38	0.40
	63	0.38	0.40	0.42	0.38	0.38	0.40
	64	0.38	0.40	0.42	0.38	0.38	0.40
	65	0.38	0.40	0.42	0.38	0.38	0.40
	66	0.38	0.40	0.42	0.38	0.38	0.40
	67	0.38	0.40	0.42	0.38	0.38	0.40
	68	0.38	0.40	0.42	0.38	0.38	0.40
	69	0.38	0.40	0.42	0.38	0.38	0.40
	70	0.38	0.40	0.42	0.38	0.38	0.40
	71	0.38	0.40	0.42	0.38	0.38	0.40
	72	0.38	0.40	0.42	0.38	0.38	0.40
	73	0.38	0.40	0.42	0.38	0.38	0.40
	74	0.38	0.40	0.42	0.38	0.38	0.40
	75	0.38	0.40	0.42	0.38	0.38	0.40
	76	0.38	0.40	0.42	0.38	0.38	0.40
	77	0.38	0.40	0.42	0.38	0.38	0.40
	78	0.38	0.40	0.42	0.38	0.38	0.40
	79	0.38	0.40	0.42	0.38	0.38	0.40
	80	0.38	0.40	0.42	0.38	0.38	0.40
	81	0.38	0.40	0.42	0.38	0.38	0.40
	82	0.38	0.40	0.42	0.38	0.38	0.40
	83	0.38	0.40	0.42	0.38	0.38	0.40
	84	0.38	0.40	0.42	0.38	0.38	0.40
	85	0.38	0.40	0.42	0.38	0.38	0.40
	86	0.38	0.40	0.42	0.38	0.38	0.40
	87	0.38	0.40	0.42	0.38	0.38	0.40
	88	0.38	0.40	0.42	0.38	0.38	0.40
	89	0.38	0.40	0.42	0.38	0.38	0.40
	90	0.38	0.40	0.42	0.38	0.38	0.40
	91	0.38	0.40	0.42	0.38	0.38	0.40
	92	0.38	0.40	0.42	0.38	0.38	0.40
	93	0.38	0.40	0.42	0.38	0.38	0.40
	94	0.38	0.40	0.42	0.38	0.38	0.40
	95	0.38	0.40	0.42	0.38	0.38	0.40
	96	0.38	0.40	0.42	0.38	0.38	0.40
	97	0.38	0.40	0.42	0.38	0.38	0.40
	98	0.38	0.40	0.42	0.38	0.38	0.40
	99	0.38	0.40	0.42	0.38	0.38	0.40
	100	0.38	0.40	0.42	0.38	0.38	0.40

▲Pressioni sul terreno

▲Pressioni verticali

Nel seguito vengono riportate le pressioni trasmesse al terreno nella struttura in corrispondenza dei nodi di fondazione.

Nodo	Caso	p_1 [kg/cm²]	p_2 [kg/cm²]	p_3 [kg/cm²]	p_4 [kg/cm²]
	1	0.38	0.40	0.42	0.38
	2				
	3				
	4				
	5				
	6				
	7				
	8				
	9				
	10				
	11				
	12				
	13				
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	94				
	95				
	96				
	97				
	98				
	99				
	100				

1	10	0,000	0,000	0,000	0,000	0,000
	11	0,000	0,000	0,000	0,000	0,000
	12	0,000	0,000	0,000	0,000	0,000
	13	0,000	0,000	0,000	0,000	0,000
	14	0,000	0,000	0,000	0,000	0,000
	15	0,000	0,000	0,000	0,000	0,000
	16	0,000	0,000	0,000	0,000	0,000
	17	0,000	0,000	0,000	0,000	0,000
	18	0,000	0,000	0,000	0,000	0,000
	19	0,000	0,000	0,000	0,000	0,000
	20	0,000	0,000	0,000	0,000	0,000
	21	0,000	0,000	0,000	0,000	0,000
	22	0,000	0,000	0,000	0,000	0,000
	23	0,000	0,000	0,000	0,000	0,000
	24	0,000	0,000	0,000	0,000	0,000
	25	0,000	0,000	0,000	0,000	0,000
	26	0,000	0,000	0,000	0,000	0,000
	27	0,000	0,000	0,000	0,000	0,000
	28	0,000	0,000	0,000	0,000	0,000
	29	0,000	0,000	0,000	0,000	0,000
	30	0,000	0,000	0,000	0,000	0,000
10	1	0,000	0,000	0,000	0,000	0,000
	2	0,000	0,000	0,000	0,000	0,000
	3	0,000	0,000	0,000	0,000	0,000
	4	0,000	0,000	0,000	0,000	0,000
	5	0,000	0,000	0,000	0,000	0,000
	6	0,000	0,000	0,000	0,000	0,000
	7	0,000	0,000	0,000	0,000	0,000
	8	0,000	0,000	0,000	0,000	0,000
	9	0,000	0,000	0,000	0,000	0,000
	10	0,000	0,000	0,000	0,000	0,000
	11	0,000	0,000	0,000	0,000	0,000
	12	0,000	0,000	0,000	0,000	0,000
	13	0,000	0,000	0,000	0,000	0,000
	14	0,000	0,000	0,000	0,000	0,000
	15	0,000	0,000	0,000	0,000	0,000
	16	0,000	0,000	0,000	0,000	0,000
	17	0,000	0,000	0,000	0,000	0,000
	18	0,000	0,000	0,000	0,000	0,000
	19	0,000	0,000	0,000	0,000	0,000
	20	0,000	0,000	0,000	0,000	0,000
	21	0,000	0,000	0,000	0,000	0,000
	22	0,000	0,000	0,000	0,000	0,000
	23	0,000	0,000	0,000	0,000	0,000
	24	0,000	0,000	0,000	0,000	0,000
	25	0,000	0,000	0,000	0,000	0,000
	26	0,000	0,000	0,000	0,000	0,000
	27	0,000	0,000	0,000	0,000	0,000
	28	0,000	0,000	0,000	0,000	0,000
	29	0,000	0,000	0,000	0,000	0,000
	30	0,000	0,000	0,000	0,000	0,000
11	1	0,000	0,000	0,000	0,000	0,000
	2	0,000	0,000	0,000	0,000	0,000
	3	0,000	0,000	0,000	0,000	0,000
	4	0,000	0,000	0,000	0,000	0,000
	5	0,000	0,000	0,000	0,000	0,000
	6	0,000	0,000	0,000	0,000	0,000
	7	0,000	0,000	0,000	0,000	0,000
	8	0,000	0,000	0,000	0,000	0,000
	9	0,000	0,000	0,000	0,000	0,000
	10	0,000	0,000	0,000	0,000	0,000
	11	0,000	0,000	0,000	0,000	0,000
	12	0,000	0,000	0,000	0,000	0,000
	13	0,000	0,000	0,000	0,000	0,000
	14	0,000	0,000	0,000	0,000	0,000
	15	0,000	0,000	0,000	0,000	0,000
	16	0,000	0,000	0,000	0,000	0,000
	17	0,000	0,000	0,000	0,000	0,000
	18	0,000	0,000	0,000	0,000	0,000
	19	0,000	0,000	0,000	0,000	0,000
	20	0,000	0,000	0,000	0,000	0,000
	21	0,000	0,000	0,000	0,000	0,000
	22	0,000	0,000	0,000	0,000	0,000
	23	0,000	0,000	0,000	0,000	0,000
	24	0,000	0,000	0,000	0,000	0,000
	25	0,000	0,000	0,000	0,000	0,000
	26	0,000	0,000	0,000	0,000	0,000
	27	0,000	0,000	0,000	0,000	0,000
	28	0,000	0,000	0,000	0,000	0,000
	29	0,000	0,000	0,000	0,000	0,000
	30	0,000	0,000	0,000	0,000	0,000
12	1	0,000	0,000	0,000	0,000	0,000
	2	0,000	0,000	0,000	0,000	0,000
	3	0,000	0,000	0,000	0,000	0,000
	4	0,000	0,000	0,000	0,000	0,000
	5	0,000	0,000	0,000	0,000	0,000
	6	0,000	0,000	0,000	0,000	0,000
	7	0,000	0,000	0,000	0,000	0,000
	8	0,000	0,000	0,000	0,000	0,000
	9	0,000	0,000	0,000	0,000	0,000
	10	0,000	0,000	0,000	0,000	0,000
	11	0,000	0,000	0,000	0,000	0,000
	12	0,000	0,000	0,000	0,000	0,000
	13	0,000	0,000	0,000	0,000	0,000
	14	0,000	0,000	0,000	0,000	0,000
	15	0,000	0,000	0,000	0,000	0,000
	16	0,000	0,000	0,000	0,000	0,000
	17	0,000	0,000	0,000	0,000	0,000
	18	0,000	0,000	0,000	0,000	0,000
	19	0,000	0,000	0,000	0,000	0,000
	20	0,000	0,000	0,000	0,000	0,000
	21	0,000	0,000	0,000	0,000	0,000
	22	0,000	0,000	0,000	0,000	0,000
	23	0,000	0,000	0,000	0,000	0,000
	24	0,000	0,000	0,000	0,000	0,000
	25	0,000	0,000	0,000	0,000	0,000
	26	0,000	0,000	0,000	0,000	0,000
	27	0,000	0,000	0,000	0,000	0,000
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	3	0,000	0,000	0,000	0,000	0,000
	4	0,000	0,000	0,000	0,000	0,000
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	8	0,000	0,000	0,000	0,000	0,000
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	7	0,000	0,000	0,000	0,000	0,000
	8	0,000	0,000	0,000	0,000	0,000
	9	0,000	0,000	0,000	0,000	0,000
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	13	0,000	0,000	0,000	0,000	0,000
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	28	0,000	0,000	0,000	0,000	0,000
	29	0,000	0,000	0,000	0,000	0,000
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	4	0,000	0,000	0,000	0,000	0,000
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	9	0,000	0,000	0,000	0,000	0,000
	10	0,000	0,000	0,000	0,000	0,000
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	30	0,000	0,000	0,000	0,000	0,000
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	29	0,000	0,000	0,000	0,000	0,000
	30	0,000	0,000	0,000	0,000	0,000
20	1	0,000	0,000	0,000	0,000	0,000
	2	0,000	0,000	0,000	0,000	0,000
	3	0,000	0,000	0,000	0,000	0,000
	4	0,000	0,000	0,000	0,000	0,000
	5	0,000	0,000	0,000	0,000	0,000
	6	0,000	0,000	0,000	0,000	0,000
	7	0,000	0,000	0,000	0,000	0,000
	8	0,000	0,000	0,000	0,000	0,000
	9	0,000	0,000	0,000	0,000	0,000
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	28	0,000	0,000	0,000	0,000	0,000
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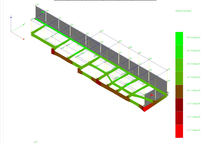
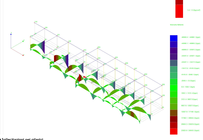
	30	0,000	0,000	0,000	0,000	0,000





Sollecitazioni nel pilastri

Sollecitazioni pilastri

Le sollecitazioni nei pilastri sono da intendersi nel sistema di riferimento locale dell'elemento e in riferimento all'asse.
Contrariamente alle piastre nella spinta è definita in base del dato 0, cui sono, in 20 intervalli, sono indicate le sue dispensa.

Per quanto concerne i segni positivi assunti per le sole componenti di sollecitazione è assunzione come positivi i verso e le sollecitazioni così diretti:

Per ogni pilastro singolo (spicchio, nella serie corrispondente di serie), le componenti di sollecitazione sono elencate dell'asse.

Config.	Nodo	Fx	Fy	Fz	Mx	My	Mz
1	10	0,000	0,000	0,000	0,000	0,000	0,000
1	11	0,000	0,000	0,000	0,000	0,000	0,000
1	12	0,000	0,000	0,000	0,000	0,000	0,000
1	13	0,000	0,000	0,000	0,000	0,000	0,000
1	14	0,000	0,000	0,000	0,000	0,000	0,000
1	15	0,000	0,000	0,000	0,000	0,000	0,000
1	16	0,000	0,000	0,000	0,000	0,000	0,000
1	17	0,000	0,000	0,000	0,000	0,000	0,000
1	18	0,000	0,000	0,000	0,000	0,000	0,000
1	19	0,000	0,000	0,000	0,000	0,000	0,000
1	20	0,000	0,000	0,000	0,000	0,000	0,000
1	21	0,000	0,000	0,000	0,000	0,000	0,000
1	22	0,000	0,000	0,000	0,000	0,000	0,000
1	23	0,000	0,000	0,000	0,000	0,000	0,000
1	24	0,000	0,000	0,000	0,000	0,000	0,000
1	25	0,000	0,000	0,000	0,000	0,000	0,000
1	26	0,000	0,000	0,000	0,000	0,000	0,000
1	27	0,000	0,000	0,000	0,000	0,000	0,000
1	28	0,000	0,000	0,000	0,000	0,000	0,000
1	29	0,000	0,000	0,000	0,000	0,000	0,000
1	30	0,000	0,000	0,000	0,000	0,000	0,000
10	1	0,000	0,000	0,000	0,000	0,000	0,000
10	2	0,000	0,000	0,000	0,000	0,000	0,000
10	3	0,000	0,000	0,000	0,000	0,000	0,000
10	4	0,000	0,000	0,000	0,000	0,000	0,000
10	5	0,000	0,000	0,000	0,000	0,000	0,000
10	6	0,000	0,000	0,000	0,000	0,000	0,000
10	7	0,000	0,000	0,000	0,000	0,000	0,000
10	8	0,000	0,000	0,000	0,000	0,000	0,000
10	9	0,000	0,000	0,000	0,000	0,000	0,000
10	10	0,000	0,000	0,000	0,000	0,000	0,000
10	11	0,000	0,000	0,000	0,000	0,000	0,000
10	12	0,000	0,000	0,000	0,000	0,000	0,000
10	13	0,000	0,000	0,000	0,000	0,000	0,000
10	14	0,000	0,000	0,000	0,000	0,000	0,000
10	15	0,000	0,000	0,000	0,000	0,000	0,000
10	16	0,000	0,000	0,000	0,000	0,000	0,000

1	0	152	0	36	0	5	0	0	152
1	0	37	0	152	0	5	0	0	152
1	0	152	0	36	0	5	0	0	152
1	0	152	0	36	0	5	0	0	152
1	0	152	0	36	0	5	0	0	152
1	0	152	0	36	0	5	0	0	152
1	0	37	0	152	0	5	0	0	152
1	0	152	0	36

1	0	255	255	255	255	255	255	255	255

1	1	1	1	1	1	1	1	1	1

24	1	52	0	1	1	3	0	3	52
24	1	53	0	1	1	3	0	3	53
24	1	54	0	1	1	3	0	3	54
24	1

1	1	0.00	0.00	0.00	0.00	0.00	0.00
2	2	0.00	0.00	0.00	0.00	0.00	0.00
3	3	0.00	0.00	0.00	0.00	0.00	0.00
4	4	0.00	0.00	0.00	0.00	0.00	0.00
5	5	0.00	0.00	0.00	0.00	0.00	0.00
6	6	0.00	0.00	0.00	0.00	0.00	0.00
7	7	0.00	0.00	0.00	0.00	0.00	0.00
8	8	0.00	0.00	0.00	0.00	0.00	0.00
9	9	0.00	0.00	0.00	0.00	0.00	0.00
10	10	0.00	0.00	0.00	0.00	0.00	0.00
11	11	0.00	0.00	0.00	0.00	0.00	0.00
12	12	0.00	0.00	0.00	0.00	0.00	0.00
13	13	0.00	0.00	0.00	0.00	0.00	0.00
14	14	0.00	0.00	0.00	0.00	0.00	0.00
15	15	0.00	0.00	0.00	0.00	0.00	0.00
16	16	0.00	0.00	0.00	0.00	0.00	0.00
17	17	0.00	0.00	0.00	0.00	0.00	0.00
18	18	0.00	0.00	0.00	0.00	0.00	0.00
19	19	0.00	0.00	0.00	0.00	0.00	0.00
20	20	0.00	0.00	0.00	0.00	0.00	0.00
21	21	0.00	0.00	0.00	0.00	0.00	0.00
22	22	0.00	0.00	0.00	0.00	0.00	0.00
23	23	0.00	0.00	0.00	0.00	0.00	0.00
24	24	0.00	0.00	0.00	0.00	0.00	0.00
25	25	0.00	0.00	0.00	0.00	0.00	0.00
26	26	0.00	0.00	0.00	0.00	0.00	0.00
27	27	0.00	0.00	0.00	0.00	0.00	0.00
28	28	0.00	0.00	0.00	0.00	0.00	0.00
29	29	0.00	0.00	0.00	0.00	0.00	0.00
30	30	0.00	0.00	0.00	0.00	0.00	0.00
31	31	0.00	0.00	0.00	0.00	0.00	0.00
32	32	0.00	0.00	0.00	0.00	0.00	0.00
33	33	0.00	0.00	0.00	0.00	0.00	0.00
34	34	0.00	0.00	0.00	0.00	0.00	0.00
35	35	0.00	0.00	0.00	0.00	0.00	0.00
36	36	0.00	0.00	0.00	0.00	0.00	0.00
37	37	0.00	0.00	0.00	0.00	0.00	0.00
38	38	0.00	0.00	0.00	0.00	0.00	0.00
39	39	0.00	0.00	0.00	0.00	0.00	0.00
40	40	0.00	0.00	0.00	0.00	0.00	0.00
41	41	0.00	0.00	0.00	0.00	0.00	0.00
42	42	0.00	0.00	0.00	0.00	0.00	0.00
43	43	0.00	0.00	0.00	0.00	0.00	0.00
44	44	0.00	0.00	0.00	0.00	0.00	0.00
45	45	0.00	0.00	0.00	0.00	0.00	0.00
46	46	0.00	0.00	0.00	0.00	0.00	0.00
47	47	0.00	0.00	0.00	0.00	0.00	0.00
48	48	0.00	0.00	0.00	0.00	0.00	0.00
49	49	0.00	0.00	0.00	0.00	0.00	0.00
50	50	0.00	0.00	0.00	0.00	0.00	0.00
51	51	0.00	0.00	0.00	0.00	0.00	0.00
52	52	0.00	0.00	0.00	0.00	0.00	0.00
53	53	0.00	0.00	0.00	0.00	0.00	0.00
54	54	0.00	0.00	0.00	0.00	0.00	0.00
55	55	0.00	0.00	0.00	0.00	0.00	0.00
56	56	0.00	0.00	0.00	0.00	0.00	0.00
57	57	0.00	0.00	0.00	0.00	0.00	0.00
58	58	0.00	0.00	0.00	0.00	0.00	0.00
59	59	0.00	0.00	0.00	0.00	0.00	0.00
60	60	0.00	0.00	0.00	0.00	0.00	0.00
61	61	0.00	0.00	0.00	0.00	0.00	0.00
62	62	0.00	0.00	0.00	0.00	0.00	0.00
63	63	0.00	0.00	0.00	0.00	0.00	0.00
64	64	0.00	0.00	0.00	0.00	0.00	0.00
65	65	0.00	0.00	0.00	0.00	0.00	0.00
66	66	0.00	0.00	0.00	0.00	0.00	0.00
67	67	0.00	0.00	0.00	0.00	0.00	0.00
68	68	0.00	0.00	0.00	0.00	0.00	0.00
69	69	0.00	0.00	0.00	0.00	0.00	0.00
70	70	0.00	0.00	0.00	0.00	0.00	0.00
71	71	0.00	0.00	0.00	0.00	0.00	0.00
72	72	0.00	0.00	0.00	0.00	0.00	0.00
73	73	0.00	0.00	0.00	0.00	0.00	0.00
74	74	0.00	0.00	0.00	0.00	0.00	0.00
75	75	0.00	0.00	0.00	0.00	0.00	0.00
76	76	0.00	0.00	0.00	0.00	0.00	0.00
77	77	0.00	0.00	0.00	0.00	0.00	0.00
78	78	0.00	0.00	0.00	0.00	0.00	0.00
79	79	0.00	0.00	0.00	0.00	0.00	0.00
80	80	0.00	0.00	0.00	0.00	0.00	0.00
81	81	0.00	0.00	0.00	0.00	0.00	0.00
82	82	0.00	0.00	0.00	0.00	0.00	0.00
83	83	0.00	0.00	0.00	0.00	0.00	0.00
84	84	0.00	0.00	0.00	0.00	0.00	0.00
85	85	0.00	0.00	0.00	0.00	0.00	0.00
86	86	0.00	0.00	0.00	0.00	0.00	0.00
87	87	0.00	0.00	0.00	0.00	0.00	0.00
88	88	0.00	0.00	0.00	0.00	0.00	0.00
89	89	0.00	0.00	0.00	0.00	0.00	0.00
90	90	0.00	0.00	0.00	0.00	0.00	0.00
91	91	0.00	0.00	0.00	0.00	0.00	0.00
92	92	0.00	0.00	0.00	0.00	0.00	0.00
93	93	0.00	0.00	0.00	0.00	0.00	0.00
94	94	0.00	0.00	0.00	0.00	0.00	0.00
95	95	0.00	0.00	0.00	0.00	0.00	0.00
96	96	0.00	0.00	0.00	0.00	0.00	0.00
97	97	0.00	0.00	0.00	0.00	0.00	0.00
98	98	0.00	0.00	0.00	0.00	0.00	0.00
99	99	0.00	0.00	0.00	0.00	0.00	0.00
100	100	0.00	0.00	0.00	0.00	0.00	0.00

▲ Sollecitazioni nelle travi

▶ Inviluppo sforzo assiale

Sforzo assiale/momento nelle travi sono da intendersi nel sistema di riferimento locale dell'elemento, e si riferiscono all'asse. Convenzionalmente della trave nella quarto definita e nasce la terna di riferimento locale dell'asta è così disposta:

Per quanto concerne i legati positivi quali per le sole componenti di sollecitazione e assumono come positivi i nodi e le sollecitazioni se così diretti:

Per ogni trave congeria riportate, nelle varie combinazioni di carico, le sollecitazioni di sollecitazione alla concorrida dell'asta.

Conb.	Sezione	N [kN]	Vy [kN]	Vz [kN]	Mx [kNm]	My [kNm]	Mz [kNm]
1	1	0.00	0.00	0.00	0.00	0.00	0.00
1	2	0.00	0.00	0.00	0.00	0.00	0.00
1	3	0.00	0.00	0.00	0.00	0.00	0.00
1

1	10	10	296.0	0.0	0.0	296.0
2	10	10	296.0	0.0	0.0	296.0
3	10	10	296.0	0.0	0.0	296.0

1	10	10	2010	0	10	0	2010
2	10	10	2010	0	10	0	2010
3	10	10	2010	0	10	0	2010

1	10	1	1	1	1	1
2	10	2	1	1	1	1
3	10	3	1	1	1	1
4	10	4	1	1	1	1
5	10	5	1	1	1	1
6	10	6	1	1	1	1
7	10	7	1	1	1	1
8	10	8	1	1	1	1
9	10	9	1	1	1	1
10	10	10	1	1	1	1
11	10	11	1	1	1	1
12	10	12	1	1	1	1
13	10	13	1	1	1	1
14	10	14	1	1	1	1
15	10	15	1	1	1	1
16	10	16	1	1	1	1
17	10	17	1	1	1	1
18	10	18	1	1	1	1
19	10	19	1	1	1	1
20	10	20	1	1	1	1
21	10	21	1	1	1	1
22	10	22	1	1	1	1
23	10	23	1	1	1	1
24	10	24	1	1	1	1
25	10	25	1	1	1	1
26	10	26	1	1	1	1
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432	10	10	10	10	10	10
433	10	10	10	10	10	10
434	10	10	10	10	10	10
435	10	10	10	10	10	10
436	10	10	10	10	10	10
437	10	10	10	10	10	10
438	10	10	10	10	10	10
439	10	10	10	10	10	10
440	10	10	10	10	10	10
441	10	10	10	10	10	10
442	10	10	10	10	10	10
443	10	10	10	10	10	10
444	10	10	10	10	10	10
445	10	10	10	10	10	10
446	10	10	10	10	10	10
447	10	10	10	10	10	10
448	10	10	10	10	10	10
449	10	10	10	10	10	10
450	10	10	10	10	10	10
451	10	10	10	10	10	10
452	10	10	10	10	10	10
453	10	10	10	10	10	10
454	10	10	10	10	10	10
455	10	10	10	10	10	10
456	10	10	10	10	10	10
457	10	10	10	10	10	10
458	10	10	10	10	10	10
459	10	10	10	10	10	10
460	10	10	10	10	10	10
461	10	10	10	10	10	10
462	10	10	10	10	10	10
463	10	10	10	10	10	10
464	10	10	10	10	10	10
465	10	10	10	10	10	10
466	10	10	10	10	10	10
467	10	10	10	10	10	10
468	10	10	10	10	10	10
469	10	10	10	10	10	10
470	10	10	10	10	10	10
471	10	10	10	10	10	10
472	10	10	10	10	10	10
473	10	10	10	10	10	10
474	10	10	10	10	10	10
475	10	10	10	10	10	10
476	10	10	10	10	10	10
477	10	10	10	10	10	10
478	10	10	10	10	10	10
479	10	10	10	10	10	10
480	10	10	10	10	10	10
481	10	10	10	10	10	10
482	10	10	10	10	10	10
483	10	10	10	10	10	10
484	10	10	10	10	10	10
485	10	10	10	10	10	10
486	10	10	10	10	10	10
487	10	10	10	10	10	10
488	10	10	10	10	10	10
489	10	10	10	10	10	10
490	10	10	10	10	10	10
491	10	10	10	10	10	10
492	10	10	10	10	10	10
493	10	10	10	10	10	10
494	10	10	10	10	10	10
495	10	10	10	10	10	10
496	10	10	10	10	10	10
497	10	10	10	10	10	10
498	10	10	10	10	10	10
499	10	10	10	10	10	10
500	10	10	10	10	10	10

1	10	10	2	2	2	2	2
2	10	10	2	2	2	2	2
3	10	10	2	2	2	2	2

34	1.00	-0.50	0.00	0.00	0.00	0.00
35	1.00	-0.50	0.00	0.00	0.00	0.00
36	1.00	-0.50	0.00	0.00	0.00	0.00

14	0	1.0	1.0	1.0	1.0
15	0	1.0	1.0	1.0	1.0
16	0	1.0	1.0	1.0	1.0

1	1	1.0	802.07	799.18	802.07
1	2	1.0	802.07	799.18	802.07
1	3	1.0	802.07	799.18	802.07
1

1	1	1	0.00	0.00	0.00	0.00
2	1	2	0.00	0.00	0.00	0.00
3	1	3	0.00	0.00	0.00	0.00

| | | |

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| | | |

Verifiche travi

Modalità di verifica

Le travi vengono progettate-verificate a flessione retta e taglio nel piano longitudinale della trave sulla base dell'inviluppo delle sollecitazioni.

Viene comunque sempre predisposta l'armatura minima mentre gli sforzi di taglio vengono integralmente assorbiti dalle staffe.

Le operazioni di progetto-verifica vengono condotte, per ogni asta, in tre diverse sezioni e precisamente in corrispondenza dei fili esterni dei pilastri e della sezione in campata nella quale viene riscontrato il massimo momento positivo (negativo).

I momenti si intendono postivi se tendono le fibre di intradosso (inferiori).

Per quanto concerne il progetto e la verifica delle travi a taglio esse vengono condotte nel modo seguente:

- Si controlla se la trave necessita o meno di armatura aggiuntiva a taglio:
  1. Se non occorre armatura aggiuntiva a taglio si procede a disporre la staffatura minima di regolamento e la progettazione ha termine.
  2. Se occorre armatura aggiuntiva a taglio la staffatuta viene progettata andando a suddividere la trave, a seconda del caso, in uno, tre o cinque conci:
     - due tronchi in prossimità degli appoggi di lunghezza pari all'altezza della sezione;
     - due altri (eventuali) tronchi dall'ascissa precedente a quella in cui il taglio può essere assorbito con la sola staffatura minima da regolamento
     - un restante (eventuale) concio di chiusura centrale.
- In ogni caso l'armatura a taglio si intende simmetrica rispetto alla mezzeria della trave e viene progettata considerando, rispetto alla mezzeria, la zona della trave più sollecitata.

Per quanto concerne le verifiche a taglio esse vengono condotte suddividendo la trave in cinque conci:

due tronchi in prossimità degli appoggi di lunghezza pari all'altezza della sezione; due altri (eventuali) tronchi dall'ascissa precedente a quella in cui il taglio può essere assorbito con la sola staffatura minima da regolamento; il restante (eventuale) concio di chiusura centrale.

L'armatura a taglio si intende simmetrica rispetto alla mezzeria della trave e viene progettata considerando, rispetto alla mezzeria, la zona della trave più sollecitata.

Simbologia utilizzata:

Af Es.
Area di ferro all'estradosso

Af In.
Area di ferro all'intradosso

Sigb.Es.
Tensione del calcestruzzo estradosso

Sigb. In.
Tensione del calcestruzzo intradosso

Sigf. Es.
Tensione dell'acciaio estradosso

Sigf. In.
Tensione dell'acciaio intradosso

Sezioni Impiegate: Trave

Sezioni Nuove

Sez. Num.	Info	Dimensioni	Criterio	Calcestruzzo	γ_M	F.C.	f_{ck} [kg/cm²]	f_{cd} [kg/cm²]	σ_{RARE} [kg/cm²]	σ_{FREQ} [kg/cm²]	σ_{QP} [kg/cm²]	Acciaio
1	Rett.	B 30 H 50 [cm]	Vertrav	C25/30	1.50	1.00	250.0	141.7	150.0	250.0	112.5	B 450 C
2	Rett.	B 75 H 25 [cm]	Vertrav	C25/30	1.50	1.00	250.0	141.7	150.0	250.0	112.5	B 450 C
3	Rett.	B 30 H 45 [cm]	Vertrav	C25/30	1.50	1.00	250.0	141.7	150.0	250.0	112.5	B 450 C

γ_M	F.C.	f_{yk} [kg/cm²]	f_{yd} [kg/cm²]	σ_{yRARE} [kg/cm²]	σ_{yFREQ} [kg/cm²]	σ_{yQP} [kg/cm²]	Cop. Es [cm]	Cop. In [cm]	cotg θ_I	cotg θ
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	3.00	3.00	1.00	1.00
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	3.00	3.00	1.00	1.00
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	3.00	3.00	1.00	1.00

Sezioni Impiegate: Trave di fondazione

Sezioni Nuove

Sez. Num.	Info	Dimensioni	Criterio	Calcestruzzo	γ_M	F.C.	f_{ck} [kg/cm²]	f_{cd} [kg/cm²]	σ_{RARE} [kg/cm²]	σ_{FREQ} [kg/cm²]	σ_{QP} [kg/cm²]	Acciaio
1	Rett.	B 90 H 50 [cm] Terreno numero 1	Verfond	C25/30	1.50	1.00	250.0	141.7	150.0	250.0	112.5	B 450 C

γ_M	F.C.	f_{yk} [kg/cm²]	f_{yd} [kg/cm²]	σ_{yRARE} [kg/cm²]	σ_{yFREQ} [kg/cm²]	σ_{yQP} [kg/cm²]	Cop. Es [cm]	Cop. In [cm]	cotg θ_I	cotg θ
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	4.00	4.00	1.00	1.00

Verifica a fessurazione indiretta

Fattore di sovraresistenza Travi $\gamma_{R,d\ (Nuovo)}$=1.10 $\gamma_{R,d\ (Esistente)}$=0.00
Fattore di sovraresistenza delle azioni sulle Fondazioni $\gamma_{R,d\ (Nuovo)}$=1.10 $\gamma_{R,d\ (Esistente)}$=0.00

Verifiche Travate :

Travata: ***Travata 1 Nodi 1 2 3 4 5 6***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
1	0.30	6.97	9.24			0.0	12302.3	0.10	-10429.8	-15788.8	0.10					
				SLE Rare		0.0			-6804.8			34.0	0.0	169.5	1796.4	
				SLE Freq.		0.0			-5826.3			29.1	0.0	145.1	1538.1	OK
				SLE Q.P.		0.0			-5470.5			27.3	0.0	136.2	1444.1	OK
Camp.	3.27	12.32	9.24			13151.4	20577.0	0.12	0.0	-15830.3	0.11					
				SLE Rare		9713.8			0.0			0.0	42.4	1942.2	317.9	
				SLE Freq.		8522.2			0.0			0.0	37.2	1704.0	278.9	OK

				SLE Q.P.		8063.1			0.0			0.0	35.2	1612.1	263.9	OK
2	6.23	16.23	18.47			0.0	26607.7	0.13	-16176.0	-30052.1	0.14					
				SLE Rare		0.0			-11603.9			41.2	0.0	347.9	1568.4	
				SLE Freq.		0.0			-10289.5			36.5	0.0	308.5	1390.7	OK
				SLE Q.P.		0.0			-9776.1			34.7	0.0	293.1	1321.3	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
2	0.14	16.50	18.47			0.0	27027.0	0.13	-16891.2	-30051.7	0.14					
				SLE Rare		0.0			-12025.7			42.6	0.0	359.4	1625.3	
				SLE Freq.		0.0			-10720.4			38.0	0.0	320.4	1448.9	OK
				SLE Q.P.		0.0			-10217.8			36.2	0.0	305.4	1381.0	OK
Camp.	1.84	9.24	9.24			1774.3	15810.3	0.10	-18.2	-15810.3	0.10					
				SLE Rare		904.3			0.0			0.0	4.4	238.8	28.9	
				SLE Freq.		775.9			0.0			0.0	3.8	204.9	24.8	OK
				SLE Q.P.		726.3			0.0			0.0	3.6	191.8	23.2	OK
3	3.54	16.42	18.47			0.0	26900.5	0.13	-4043.0	-30051.8	0.14					
				SLE Rare		0.0			-2901.2			10.3	0.0	86.8	392.1	
				SLE Freq.		0.0			-2691.4			9.5	0.0	80.5	363.8	OK
				SLE Q.P.		0.0			-2590.2			9.2	0.0	77.5	350.1	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
3	0.18	16.23	18.47			0.0	26607.7	0.13	-5583.4	-30052.1	0.14					
				SLE Rare		0.0			-3602.7			12.8	0.0	108.0	486.9	
				SLE Freq.		0.0			-3386.7			12.0	0.0	101.5	457.7	OK
				SLE Q.P.		0.0			-3292.6			11.7	0.0	98.7	445.0	OK
Camp.	1.69	9.24	9.24			5271.6	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		3498.1			0.0			0.0	17.2	923.9	111.6	
				SLE Freq.		3108.4			0.0			0.0	15.3	821.0	99.2	OK
				SLE Q.P.		2955.7			0.0			0.0	14.5	780.7	94.3	OK
4	3.20	16.48	18.47			3496.1	26998.1	0.13	-5237.0	-30051.8	0.14					
				SLE Rare		0.0			-1623.2			5.8	0.0	48.5	219.4	
				SLE Freq.		0.0			-1354.1			4.8	0.0	40.5	183.0	OK

				SLE Q.P.		0.0			-1244.1			4.4	0.0	37.2	168.1	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
4	0.15	16.42	18.47			0.0	26900.5	0.13	-5827.9	-30051.8	0.14					
				SLE Rare		0.0			-4283.1			15.2	0.0	128.1	578.9	
				SLE Freq.		0.0			-3824.3			13.6	0.0	114.4	516.9	OK
				SLE Q.P.		0.0			-3641.0			12.9	0.0	108.9	492.1	OK
Camp.	1.81	9.24	9.24			2421.2	15810.3	0.10	-900.0	-15810.3	0.10					
				SLE Rare		1068.1			0.0			0.0	5.2	282.1	34.1	
				SLE Freq.		993.7			0.0			0.0	4.9	262.5	31.7	OK
				SLE Q.P.		963.0			0.0			0.0	4.7	254.4	30.7	OK
5	3.46	19.90	21.30			0.0	32180.9	0.14	-12045.3	-34322.6	0.14					
				SLE Rare		0.0			-8398.5			27.7	0.0	241.1	992.4	
				SLE Freq.		0.0			-7452.2			24.6	0.0	213.9	880.6	OK
				SLE Q.P.		0.0			-7070.0			23.3	0.0	202.9	835.4	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
5	0.15	21.32	21.30			0.0	34345.7	0.14	-16111.5	-34319.4	0.14					
				SLE Rare		0.0			-11627.7			37.9	0.0	324.6	1373.8	
				SLE Freq.		0.0			-10430.0			34.0	0.0	291.2	1232.3	OK
				SLE Q.P.		0.0			-9949.0			32.5	0.0	277.8	1175.5	OK
Camp.	3.15	14.07	12.06			16522.0	23248.6	0.12	0.0	-20166.8	0.12					
				SLE Rare		11402.2			0.0			0.0	46.5	2009.7	356.7	
				SLE Freq.		10519.5			0.0			0.0	42.9	1854.1	329.1	OK
				SLE Q.P.		10162.5			0.0			0.0	41.5	1791.2	317.9	OK
6	6.15	14.07	12.06			7361.5	23248.6	0.12	-15999.4	-20166.8	0.12					
				SLE Rare		0.0			-4202.1			18.0	0.0	127.3	859.9	
				SLE Freq.		0.0			-3827.5			16.4	0.0	115.9	783.2	OK
				SLE Q.P.		0.0			-3664.0			15.7	0.0	111.0	749.8	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 1 2 Sez. 1 Rett. 90x50 [cm]											

0.40	6.23	5.83	1.00	19493.4	15154.9	12797 6.3	25264.3	1808.1	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 2 3 Sez. 1 Rett. 90x50 [cm]											
0.14	3.54	3.40	1.00	16930.9	15154.9	12797 6.3	25264.3	778.1	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 3 4 Sez. 1 Rett. 90x50 [cm]											
0.18	3.20	3.02	1.00	11834.4	15154.9	12797 6.3	25264.3	1637.5	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 4 5 Sez. 1 Rett. 90x50 [cm]											
0.15	3.46	3.31	1.00	13661.7	15154.9	12797 6.3	25264.3	2818.9	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 5 6 Sez. 1 Rett. 90x50 [cm]											
0.15	6.05	5.90	1.00	22222.9	16582.4	12797 6.3	25264.3	2512.7	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 11 Nodi 3 10 26***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
3	0.25	9.24	9.24			6772.8	15810.3	0.10	-2855.1	-15810.3	0.10					
				SLE Rare		1404.3			0.0			0.0	6.9	370.9	44.8	
				SLE Freq.		1386.8			0.0			0.0	6.8	366.3	44.3	OK
				SLE Q.P.		1378.3			0.0			0.0	6.8	364.0	44.0	OK
Camp.	1.05	9.24	11.29			7608.6	15828.7	0.11	0.0	-18979.9	0.11					
				SLE Rare		4405.7			0.0			0.0	21.3	1164.3	136.7	
				SLE Freq.		4399.6			0.0			0.0	21.3	1162.7	136.5	OK
				SLE Q.P.		4397.8			0.0			0.0	21.3	1162.2	136.4	OK
10	1.85	16.50	21.30			5744.8	27026.2	0.13	0.0	-34333.3	0.14					
				SLE Rare		3599.3			0.0			0.0	12.9	542.6	102.5	
				SLE Freq.		3906.4			0.0			0.0	14.0	588.8	111.3	OK
				SLE Q.P.		3902.8			0.0			0.0	14.0	588.3	111.2	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
10	0.25	16.10	21.30			15992.7	26412.8	0.13	-3547.8	-34333.5	0.14					
				SLE Rare		5427.3			0.0			0.0	19.6	837.8	154.6	
				SLE Freq.		5838.9			0.0			0.0	21.1	901.3	166.3	OK
				SLE Q.P.		5838.8			0.0			0.0	21.1	901.3	166.3	OK

Camp.	3.01	9.24	12.06			8688.9	15851.8	0.11	-237.6	-20141.1	0.11					
				SLE Rare		5615.9			0.0			0.0	27.1	1484.7	168.7	
				SLE Freq.		4855.4			0.0			0.0	23.4	1283.6	145.9	OK
				SLE Q.P.		4561.8			0.0			0.0	22.0	1206.0	137.1	OK
26	5.78	9.30	24.13			0.0	15988.7	0.12	-36657.9	-38574.1	0.17					
				SLE Rare		0.0			-19545.2			66.7	0.0	470.3	2052.3	
				SLE Freq.		0.0			-18932.1			64.7	0.0	455.6	1987.9	OK
				SLE Q.P.		0.0			-18702.7			63.9	0.0	450.1	1963.8	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 3 10 Sez. 1 Rett. 90x50 [cm]											
0.30	1.80	1.51	1.00	8208.6	15154.9	127976.3	25264.3	966.5	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 10 26 Sez. 1 Rett. 90x50 [cm]											
0.30	5.78	5.48	1.00	19008.5	15154.9	127976.3	25264.3	1081.7	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 12 Nodi 4 11 27***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
4	0.25	9.24	9.24			4748.8	15810.3	0.10	-3579.2	-15810.3	0.10					
				SLE Rare		49.3			-79.0			0.4	0.2	13.0	20.9	
				SLE Freq.		120.0			0.0			0.0	0.6	31.7	3.8	OK
				SLE Q.P.		123.1			0.0			0.0	0.6	32.5	3.9	OK
Camp.	1.05	9.24	9.24			5697.0	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		2936.1			0.0			0.0	14.4	775.5	93.7	
				SLE Freq.		3033.5			0.0			0.0	14.9	801.2	96.8	OK
				SLE Q.P.		3035.1			0.0			0.0	14.9	801.6	96.9	OK
11	1.85	16.50	18.47			4085.4	27027.0	0.13	0.0	-30051.7	0.14					
				SLE Rare		2080.3			0.0			0.0	7.6	313.5	61.0	
				SLE Freq.		2487.9			0.0			0.0	9.1	374.9	72.9	OK
				SLE Q.P.		2487.3			0.0			0.0	9.1	374.8	72.9	OK

Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
11	0.25	16.10	18.47			15714.2	26412.5	0.13	-3434.8	-30052.2	0.14					
				SLE Rare		5310.5			0.0			0.0	19.6	819.5	155.7	
				SLE Freq.		5745.7			0.0			0.0	21.2	886.7	168.5	OK
				SLE Q.P.		5747.0			0.0			0.0	21.2	886.9	168.5	OK
Camp.	3.01	9.24	9.24			11319.7	15810.3	0.10	-132.4	-15810.3	0.10					
				SLE Rare		6306.3			0.0			0.0	31.0	1665.7	201.3	
				SLE Freq.		5499.8			0.0			0.0	27.0	1452.6	175.5	OK
				SLE Q.P.		5188.3			0.0			0.0	25.5	1370.3	165.6	OK
27	5.78	9.30	19.29			0.0	15965.9	0.11	-30619.0	-31272.4	0.14					
				SLE Rare		0.0			-17392.4			64.2	0.0	425.9	2264.0	
				SLE Freq.		0.0			-16874.5			62.3	0.0	413.2	2196.6	OK
				SLE Q.P.		0.0			-16683.4			61.6	0.0	408.5	2171.7	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 4 11 Sez. 1 Rett. 90x50 [cm]											
0.30	1.80	1.51	1.00	7989.5	15154.9	127976.3	25264.3	1042.9	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 11 27 Sez. 1 Rett. 90x50 [cm]											
0.30	5.78	5.48	1.00	21028.5	15154.9	127976.3	25264.3	468.4	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 13 Nodi 5 12 28***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
5	0.25	9.24	9.24			4785.4	15810.3	0.10	-1935.5	-15810.3	0.10					
				SLE Rare		1233.5			0.0			0.0	6.1	325.8	39.4	
				SLE Freq.		980.6			0.0			0.0	4.8	259.0	31.3	OK
				SLE Q.P.		875.0			0.0			0.0	4.3	231.1	27.9	OK
Camp.	1.05	9.24	9.24			5943.7	15810.3	0.10	-4434.9	-15810.3	0.10					
				SLE Rare		894.5			0.0			0.0	4.4	236.3	28.5	
				SLE Freq.		1173.1			0.0			0.0	5.8	309.9	37.4	OK

				SLE Q.P.		1175.6			0.0			0.0	5.8	310.5	37.5	OK
12	1.85	16.36	18.47			4822.2	26802.9	0.13	-8926.2	-30051.9	0.14					
				SLE Rare		0.0			-4055.8			14.4	0.0	121.4	548.2	
				SLE Freq.		0.0			-2707.0			9.6	0.0	81.0	365.9	OK
				SLE Q.P.		0.0			-2166.4			7.7	0.0	64.9	292.8	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
12	0.25	16.10	18.47			11333.3	26412.5	0.13	-5464.2	-30052.2	0.14					
				SLE Rare		2027.9			-13.7			0.0	7.5	313.0	59.5	
				SLE Freq.		2756.5			0.0			0.0	10.1	425.4	80.8	OK
				SLE Q.P.		2758.8			0.0			0.0	10.2	425.7	80.9	OK
Camp.	2.96	9.24	9.24			10085.2	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		7017.9			0.0			0.0	34.5	1853.6	224.0	
				SLE Freq.		6146.7			0.0			0.0	30.2	1623.5	196.2	OK
				SLE Q.P.		5809.8			0.0			0.0	28.5	1534.5	185.4	OK
28	5.68	9.54	15.39			0.0	16305.6	0.11	-22449.7	-25329.5	0.13					
				SLE Rare		0.0			-14458.9			57.8	0.0	428.7	2331.1	
				SLE Freq.		0.0			-14235.2			56.9	0.0	422.0	2295.0	OK
				SLE Q.P.		0.0			-14162.4			56.6	0.0	419.9	2283.3	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 5 12 Sez. 1 Rett. 90x50 [cm]											
0.30	1.80	1.51	1.00	10765.8	15154.9	12797.3	25264.3	2353.3	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 12 28 Sez. 1 Rett. 90x50 [cm]											
0.30	5.63	5.33	1.00	17642.0	15154.9	12797.3	25264.3	865.6	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 14 Nodi 17 10***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
17	0.13	9.30	13.85			0.0	15933.9	0.11	-16278.8	-22955.5	0.12					

				SLE Rare		0.0			-12071.8			50.3	0.0	298.7	2154.3	
				SLE Freq.		0.0			-10805.8			45.1	0.0	267.4	1928.4	OK
				SLE Q.P.		0.0			-10303.1			43.0	0.0	254.9	1838.6	OK
Camp.	2.03	9.24	9.24			4930.4	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		3012.9			0.0			0.0	14.8	795.8	96.2	
				SLE Freq.		2723.4			0.0			0.0	13.4	719.3	86.9	OK
				SLE Q.P.		2608.8			0.0			0.0	12.8	689.0	83.3	OK
10	3.94	9.24	9.24			6582.4	15810.3	0.10	-902.2	-15810.3	0.10					
				SLE Rare		2551.5			0.0			0.0	12.5	673.9	81.4	
				SLE Freq.		2514.4			0.0			0.0	12.3	664.1	80.3	OK
				SLE Q.P.		2495.3			0.0			0.0	12.3	659.1	79.6	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 17 10 Sez. 1 Rett. 90x50 [cm]											
0.13	3.94	3.82	1.00	16383.1	15154.9	127976.3	25264.3	5201.2	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 15 Nodi 12 18***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
12	0.13	8.86	12.32			0.0	15219.7	0.11	-12656.4	-20587.9	0.12					
				SLE Rare		0.0			-9058.1			39.7	0.0	215.4	1811.6	
				SLE Freq.		0.0			-7821.0			34.3	0.0	186.0	1564.1	OK
				SLE Q.P.		0.0			-7329.6			32.2	0.0	174.3	1465.9	OK
Camp.	3.35	12.06	9.24			13311.5	20141.1	0.11	0.0	-15851.8	0.11					
				SLE Rare		9969.3			0.0			0.0	44.1	2038.2	326.8	
				SLE Freq.		9088.9			0.0			0.0	40.2	1858.2	297.9	OK
				SLE Q.P.		8742.4			0.0			0.0	38.7	1787.4	286.6	OK
18	6.57	10.03	13.85			0.0	17021.6	0.11	-16764.8	-22963.0	0.12					
				SLE Rare		0.0			-12342.4			51.3	0.0	303.2	2203.2	

	SLE Freq.	0.0			-11542.9			47.9	0.0	283.6	2060.5	OK
	SLE Q.P.	0.0			-11227.9			46.6	0.0	275.8	2004.3	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 12 18 Sez. 1 Rett. 90x50 [cm]											
0.13	6.57	6.45	1.00	20834.4	15154.9	127976.3	25264.3	1434.2	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 2 Nodi 7 8 9***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
7	0.30	9.24	9.24			83.8	15810.3	0.10	-15102.7	-15810.3	0.10					
				SLE Rare		0.0			-7734.2			38.0	0.0	246.9	2042.8	
				SLE Freq.		0.0			-7238.4			35.5	0.0	231.0	1911.8	OK
				SLE Q.P.		0.0			-7041.4			34.6	0.0	224.7	1859.8	OK
Camp.	2.82	9.24	9.24			11818.5	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		8183.6			0.0			0.0	40.2	2161.5	261.2	
				SLE Freq.		7252.3			0.0			0.0	35.6	1915.5	231.5	OK
				SLE Q.P.		6882.9			0.0			0.0	33.8	1818.0	219.7	OK
8	5.33	16.61	18.47			0.0	27193.3	0.13	-12184.4	-30051.6	0.13					
				SLE Rare		0.0			-8481.0			30.0	0.0	253.2	1146.2	
				SLE Freq.		0.0			-6765.9			24.0	0.0	202.0	914.4	OK
				SLE Q.P.		0.0			-6070.8			21.5	0.0	181.2	820.5	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
8	0.15	16.50	18.47			0.0	27027.0	0.13	-14885.7	-30051.7	0.14					
				SLE Rare		0.0			-10721.3			38.0	0.0	320.4	1449.0	
				SLE Freq.		0.0			-9016.3			32.0	0.0	269.5	1218.6	OK
				SLE Q.P.		0.0			-8319.8			29.5	0.0	248.6	1124.5	OK
Camp.	2.63	9.24	9.24			5094.7	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		3731.6			0.0			0.0	18.3	985.6	119.1	

				SLE Freq.		3131.4			0.0			0.0	15.4	827.1	99.9	OK
				SLE Q.P.		2897.8			0.0			0.0	14.2	765.4	92.5	OK
9	5.11	9.24	9.24			0.0	15810.3	0.10	-10846.6	-15810.3	0.10					
				SLE Rare		0.0			-7940.2			39.0	0.0	253.4	2097.2	
				SLE Freq.		0.0			-6613.0			32.5	0.0	211.1	1746.7	OK
				SLE Q.P.		0.0			-6134.5			30.1	0.0	195.8	1620.3	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 7 8 Sez. 1 Rett. 90x50 [cm]											
0.40	5.33	4.93	1.00	19867.8	15154.9	127976.3	25264.3	4736.6	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 8 9 Sez. 1 Rett. 90x50 [cm]											
0.15	5.11	4.96	1.00	16033.5	15154.9	127976.3	25264.3	6221.9	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 3 Nodi 10 11 12***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
10	0.18	9.24	9.24			688.9	15810.3	0.10	-1578.8	-15810.3	0.10					
				SLE Rare		0.0			-990.9			4.9	0.0	31.6	261.7	
				SLE Freq.		0.0			-918.4			4.5	0.0	29.3	242.6	OK
				SLE Q.P.		0.0			-888.1			4.4	0.0	28.3	234.6	OK
Camp.	1.69	9.24	9.24			4918.4	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		3651.9			0.0			0.0	17.9	964.6	116.6	
				SLE Freq.		3237.8			0.0			0.0	15.9	855.2	103.3	OK
				SLE Q.P.		3073.8			0.0			0.0	15.1	811.9	98.1	OK
11	3.20	16.12	18.47			343.5	26441.4	0.13	-1421.7	-30052.2	0.14					
				SLE Rare		0.0			-1038.5			3.7	0.0	31.2	140.4	
				SLE Freq.		0.0			-898.7			3.2	0.0	27.0	121.5	OK
				SLE Q.P.		0.0			-841.7			3.0	0.0	25.3	113.8	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																

11	0.15	16.63	18.47			13.6	27222.2	0.13	-2530.7	-30051.6	0.13					
				SLE Rare		0.0			-1734.4			6.1	0.0	51.8	234.4	
				SLE Freq.		0.0			-1575.9			5.6	0.0	47.0	213.0	OK
				SLE Q.P.		0.0			-1513.1			5.4	0.0	45.2	204.5	OK
Camp.	1.81	9.24	9.24			1908.1	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		1134.6			0.0			0.0	5.6	299.7	36.2	
				SLE Freq.		1067.5			0.0			0.0	5.2	282.0	34.1	OK
				SLE Q.P.		1040.5			0.0			0.0	5.1	274.8	33.2	OK
12	3.46	6.97	9.24			0.0	12302.2	0.10	-11668.0	-15788.8	0.10					
				SLE Rare		0.0			-8579.2			42.8	0.0	213.7	2264.8	
				SLE Freq.		0.0			-7439.7			37.1	0.0	185.3	1964.0	OK
				SLE Q.P.		0.0			-6984.9			34.9	0.0	174.0	1843.9	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 10 11 Sez. 1 Rett. 90x50 [cm]											
0.18	3.20	3.02	1.00	8408.7	15154.9	127976.3	25264.3	458.3	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 11 12 Sez. 1 Rett. 90x50 [cm]											
0.15	3.46	3.31	1.00	13280.1	15154.9	127976.3	25264.3	959.5	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 4 Nodi 13 14 15***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
13	0.52	9.24	9.24			1788.2	15810.3	0.10	-8316.9	-15810.3	0.10					
				SLE Rare		0.0			-3051.2			15.0	0.0	97.4	805.9	
				SLE Freq.		0.0			-3153.6			15.5	0.0	100.7	832.9	OK
				SLE Q.P.		0.0			-3150.7			15.5	0.0	100.6	832.2	OK
Camp.	2.40	9.24	9.24			7031.0	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		4770.9			0.0			0.0	23.4	1260.1	152.3	
				SLE Freq.		4273.2			0.0			0.0	21.0	1128.7	136.4	OK

				SLE Q.P.		4073.4			0.0			0.0	20.0	1075.9	130.0	OK
14	4.27	16.50	18.47			2895.5	27027.0	0.13	-5146.8	-30051.7	0.14					
				SLE Rare		0.0			-2750.6			9.7	0.0	82.2	371.8	
				SLE Freq.		0.0			-1895.3			6.7	0.0	56.6	256.2	OK
				SLE Q.P.		0.0			-1551.9			5.5	0.0	46.4	209.7	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
14	0.25	16.10	18.47			0.0	26412.5	0.13	-7667.2	-30052.2	0.14					
				SLE Rare		0.0			-5628.8			20.0	0.0	169.0	760.8	
				SLE Freq.		0.0			-4753.8			16.9	0.0	142.7	642.5	OK
				SLE Q.P.		0.0			-4405.8			15.7	0.0	132.3	595.5	OK
Camp.	2.17	9.24	9.24			2671.7	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		1735.5			0.0			0.0	8.5	458.4	55.4	
				SLE Freq.		1442.4			0.0			0.0	7.1	381.0	46.0	OK
				SLE Q.P.		1325.4			0.0			0.0	6.5	350.1	42.3	OK
15	4.08	7.61	9.24			0.0	13288.3	0.10	-8314.9	-15795.6	0.10					
				SLE Rare		0.0			-5196.2			25.8	0.0	139.9	1371.9	
				SLE Freq.		0.0			-4713.6			23.4	0.0	126.9	1244.5	OK
				SLE Q.P.		0.0			-4518.2			22.4	0.0	121.6	1192.9	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 13 14 Sez. 1 Rett. 90x50 [cm]											
0.81	4.22	3.41	1.00	11961.5	15154.9	127976.3	25264.3	7435.8	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 14 15 Sez. 1 Rett. 90x50 [cm]											
0.30	4.08	3.78	1.00	10233.7	15154.9	127976.3	25264.3	2323.2	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 41 Nodi 2 17 25***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
2	0.25	12.06	9.24			14185.9	20141.1	0.11	-1165.1	-15851.8	0.11					

				SLE Rare		5841.7			0.0			0.0	25.8	1194.3	191.5	
				SLE Freq.		5652.6			0.0			0.0	25.0	1155.7	185.3	OK
				SLE Q.P.		5565.6			0.0			0.0	24.6	1137.9	182.4	OK
Camp.	1.93	12.06	9.24			12102.7	20141.1	0.11	0.0	-15851.8	0.11					
				SLE Rare		8567.8			0.0			0.0	37.9	1751.7	280.8	
				SLE Freq.		7991.1			0.0			0.0	35.3	1633.8	261.9	OK
				SLE Q.P.		7767.4			0.0			0.0	34.3	1588.0	254.6	OK
17	3.62	19.44	27.33			3850.0	31467.9	0.13	-10297.6	-43481.6	0.16					
				SLE Rare		0.0			-4372.5			13.2	0.0	122.5	406.8	
				SLE Freq.		0.0			-3689.7			11.2	0.0	103.3	343.2	OK
				SLE Q.P.		0.0			-3401.7			10.3	0.0	95.3	316.5	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
17	0.25	18.25	27.33			12302.9	29655.8	0.13	-3083.5	-43482.2	0.16					
				SLE Rare		3572.1			0.0			0.0	11.9	489.8	95.5	
				SLE Freq.		4256.7			0.0			0.0	14.1	583.7	113.9	OK
				SLE Q.P.		4242.5			0.0			0.0	14.1	581.8	113.5	OK
Camp.	2.08	9.24	18.10			4529.2	15877.9	0.11	-10467.1	-29412.4	0.14					
				SLE Rare		0.0			-988.9			3.7	0.0	32.3	136.8	
				SLE Freq.		0.0			-1310.1			5.0	0.0	42.7	181.2	OK
				SLE Q.P.		0.0			-1321.6			5.0	0.0	43.1	182.8	OK
25	3.91	9.54	28.15			0.0	16358.7	0.12	-41573.3	-44593.6	0.19					
				SLE Rare		0.0			-19900.9			64.4	0.0	565.5	1803.5	
				SLE Freq.		0.0			-19921.8			64.4	0.0	566.0	1805.4	OK
				SLE Q.P.		0.0			-19902.6			64.4	0.0	565.5	1803.7	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 2 17 Sez. 1 Rett. 90x50 [cm]											
0.30	3.57	3.27	1.00	15456.5	15751.9	12797.6.3	25264.3	2074.1	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 17 25 Sez. 1 Rett. 90x50 [cm]											

0.30	3.86	3.56	1.00	19426.0	15154.9	127976.3	25264.3	738.2	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 5 Nodi 16 17***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
16	0.30	6.97	9.24			0.0	12302.2	0.10	-7863.8	-15788.8	0.10					
				SLE Rare		0.0			-5341.4			26.7	0.0	133.0	1410.1	
				SLE Freq.		0.0			-4462.5			22.3	0.0	111.1	1178.0	OK
				SLE Q.P.		0.0			-4139.6			20.7	0.0	103.1	1092.8	OK
Camp.	3.27	9.24	9.24			10314.5	15810.3	0.10	0.0	-15810.3	0.10					
				SLE Rare		7535.5			0.0			0.0	37.0	1990.3	240.5	
				SLE Freq.		6519.6			0.0			0.0	32.0	1722.0	208.1	OK
				SLE Q.P.		6128.8			0.0			0.0	30.1	1618.8	195.6	OK
17	6.23	6.97	12.32			0.0	12333.2	0.10	-14959.8	-20569.8	0.11					
				SLE Rare		0.0			-10820.1			48.1	0.0	275.6	2163.1	
				SLE Freq.		0.0			-9596.8			42.7	0.0	244.4	1918.5	OK
				SLE Q.P.		0.0			-9108.8			40.5	0.0	232.0	1821.0	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 16 17 Sez. 1 Rett. 90x50 [cm]											
0.40	6.23	5.83	1.00	16276.1	15154.9	127976.3	25264.3	320.8	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 6 Nodi 13 20***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
13	0.15	15.27	26.14			22961.5	25111.9	0.13	-2392.2	-41632.9	0.16					
				SLE Rare		9691.4			0.0			0.0	34.8	1579.4	258.0	
				SLE Freq.		9482.9			0.0			0.0	34.1	1545.4	252.5	OK
				SLE Q.P.		9400.3			0.0			0.0	33.8	1531.9	250.3	OK

Camp.	2.60	9.24	26.14			4570.7	15896.9	0.12	-12946.6	-41591.2	0.18					
				SLE Rare		0.0			-1822.9			6.1	0.0	57.7	177.3	
				SLE Freq.		0.0			-2092.8			7.0	0.0	66.2	203.6	OK
				SLE Q.P.		0.0			-2092.3			7.0	0.0	66.2	203.5	OK
20	5.05	9.24	46.24			4625.4	15917.9	0.12	-67386.1	-69906.3	0.32					
				SLE Rare		0.0			-30131.0			83.5	0.0	886.3	1705.1	
				SLE Freq.		0.0			-29025.9			80.4	0.0	853.8	1642.6	OK
				SLE Q.P.		0.0			-28587.8			79.2	0.0	840.9	1617.8	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 13 20 Sez. 1 Rett. 90x50 [cm]											
0.15	5.05	4.90	1.00	24191.8	15154.9	127976.3	25264.3	2142.0	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 7 Nodi 7 15 22***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
7	0.25	12.06	9.24			16009.0	20141.1	0.11	-2367.1	-15851.8	0.11					
				SLE Rare		6441.2			0.0			0.0	28.5	1316.9	211.1	
				SLE Freq.		6259.8			0.0			0.0	27.7	1279.8	205.2	OK
				SLE Q.P.		6189.0			0.0			0.0	27.4	1265.3	202.9	OK
Camp.	0.75	15.22	26.78			15517.9	25003.1	0.13	-2799.7	-42613.3	0.17					
				SLE Rare		5523.9			0.0			0.0	19.8	902.9	148.7	
				SLE Freq.		5544.1			0.0			0.0	19.9	906.2	149.2	OK
				SLE Q.P.		5543.1			0.0			0.0	19.9	906.1	149.2	OK
15	1.25	27.18	35.37			12763.2	43223.4	0.15	-3433.0	-55637.6	0.18					
				SLE Rare		3228.2			0.0			0.0	8.8	300.5	78.9	
				SLE Freq.		3561.7			0.0			0.0	9.7	331.5	87.0	OK
				SLE Q.P.		3561.8			0.0			0.0	9.7	331.6	87.0	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																

15	0.25	31.32	35.37			43125.0	49521.3	0.16	-7495.5	-55660.4	0.17					
				SLE Rare		16132.7			0.0			0.0	42.0	1309.1	390.4	
				SLE Freq.		16286.0			0.0			0.0	42.4	1321.5	394.1	OK
				SLE Q.P.		16283.9			0.0			0.0	42.4	1321.3	394.1	OK
Camp.	2.60	18.10	26.14			6884.2	29389.9	0.13	-7370.6	-41622.7	0.16					
				SLE Rare		2707.3			0.0			0.0	9.1	374.2	72.4	
				SLE Freq.		2112.3			0.0			0.0	7.1	292.0	56.5	OK
				SLE Q.P.		1876.6			0.0			0.0	6.3	259.4	50.2	OK
22	4.95	18.10	48.25			4256.6	29380.5	0.13	-72335.2	-74183.4	0.26					
				SLE Rare		0.0			-32130.4			82.2	0.0	858.8	1736.0	
				SLE Freq.		0.0			-31570.7			80.8	0.0	843.8	1705.8	OK
				SLE Q.P.		0.0			-31354.3			80.2	0.0	838.1	1694.1	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 7 15 Sez. 1 Rett. 90x50 [cm]											
0.30	1.20	0.91	1.00	7941.5	15751.9	127976.3	42107.1	11813.4	27047.9	13156.1	ø 8 4br. 7.5'
Trave di fondazione 15 22 Sez. 1 Rett. 90x50 [cm]											
0.30	4.90	4.60	1.00	30373.5	18031.4	127976.3	31580.4	758.2	27047.9	9867.1	ø 8 4br. 10.0'

Travata: ***Travata 8 Nodi 8 23***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
8	0.25	16.08	16.08			23364.2	26326.7	0.13	-6898.4	-26326.7	0.13					
				SLE Rare		7252.8			0.0			0.0	27.3	1123.7	216.5	
				SLE Freq.		7620.6			0.0			0.0	28.7	1180.7	227.4	OK
				SLE Q.P.		7621.3			0.0			0.0	28.7	1180.8	227.5	OK
Camp.	3.40	14.07	16.08			11570.0	23250.4	0.12	-151.0	-26328.0	0.13					
				SLE Rare		7572.1			0.0			0.0	30.1	1334.9	225.6	
				SLE Freq.		6418.9			0.0			0.0	25.5	1131.6	191.2	OK

				SLE Q.P.		5964.6			0.0			0.0	23.7	1051.5	177.7	OK
23	6.55	14.07	36.19			2018.3	23254.5	0.13	-53535.1	-56548.2	0.22					
				SLE Rare		0.0			-24136.5			69.5	0.0	694.2	1718.4	
				SLE Freq.		0.0			-24064.1			69.3	0.0	692.1	1713.3	OK
				SLE Q.P.		0.0			-24029.2			69.2	0.0	691.1	1710.8	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 8 23 Sez. 1 Rett. 90x50 [cm]											
0.30	6.55	6.25	1.00	21398.9	16582.4	127976.3	25264.3	378.7	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 9 Nodi 1 9 16 24***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
1	0.25	14.07	11.96			19339.0	23240.9	0.12	-2616.5	-20055.7	0.12					
				SLE Rare		7508.8			0.0			0.0	30.6	1322.9	238.5	
				SLE Freq.		7271.3			0.0			0.0	29.7	1281.1	231.0	OK
				SLE Q.P.		7162.7			0.0			0.0	29.2	1262.0	227.5	OK
Camp.	0.79	23.23	18.47			20580.0	37234.4	0.15	0.0	-30039.2	0.13					
				SLE Rare		11494.0			0.0			0.0	37.1	1248.3	332.8	
				SLE Freq.		10493.8			0.0			0.0	33.9	1139.7	303.9	OK
				SLE Q.P.		10107.3			0.0			0.0	32.6	1097.7	292.7	OK
9	1.33	28.15	18.47			20627.4	44699.9	0.17	0.0	-30035.7	0.13					
				SLE Rare		14017.7			0.0			0.0	42.3	1265.8	399.5	
				SLE Freq.		12481.0			0.0			0.0	37.7	1127.1	355.7	OK
				SLE Q.P.		11901.9			0.0			0.0	35.9	1074.8	339.2	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
9	0.00	28.15	18.47			26581.8	44699.9	0.17	0.0	-30035.7	0.13					
				SLE Rare		17877.3			0.0			0.0	54.0	1614.4	509.5	
				SLE Freq.		15855.1			0.0			0.0	47.9	1431.7	451.9	OK

				SLE Q.P.		15077.2			0.0			0.0	45.5	1361.5	429.7	OK
Camp.	1.14	14.07	10.42			12424.1	23240.4	0.12	0.0	-17680.1	0.11					
				SLE Rare		6770.8			0.0			0.0	27.9	1192.9	219.3	
				SLE Freq.		6225.5			0.0			0.0	25.7	1096.8	201.6	OK
				SLE Q.P.		6019.7			0.0			0.0	24.8	1060.6	195.0	OK
16	2.29	20.96	31.35			0.0	33781.5	0.14	-16212.8	-49556.1	0.17					
				SLE Rare		0.0			-11027.2			31.6	0.0	300.7	899.1	
				SLE Freq.		0.0			-9179.0			26.3	0.0	250.3	748.4	OK
				SLE Q.P.		0.0			-8466.8			24.2	0.0	230.9	690.4	OK
Trave di fondazione Sez. 1 Rett. 90x50 [cm]																
16	0.25	19.92	31.35			13197.3	32201.5	0.13	-5398.5	-49554.6	0.18					
				SLE Rare		2114.7			0.0			0.0	6.6	266.4	54.3	
				SLE Freq.		3601.8			0.0			0.0	11.3	453.7	92.5	OK
				SLE Q.P.		3654.5			0.0			0.0	11.5	460.4	93.8	OK
Camp.	2.13	9.24	22.12			5432.0	15888.8	0.11	-13933.7	-35536.2	0.16					
				SLE Rare		0.0			-2061.5			7.3	0.0	66.3	235.3	
				SLE Freq.		0.0			-2416.2			8.5	0.0	77.7	275.7	OK
				SLE Q.P.		0.0			-2429.5			8.6	0.0	78.1	277.3	OK
24	4.01	9.24	32.17			3177.2	15905.6	0.12	-49560.6	-50499.4	0.21					
				SLE Rare		0.0			-20900.4			64.8	0.0	645.4	1668.3	
				SLE Freq.		0.0			-21564.9			66.9	0.0	665.9	1721.3	OK
				SLE Q.P.		0.0			-21592.5			67.0	0.0	666.8	1723.5	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave di fondazione 1 9 Sez. 1 Rett. 90x50 [cm]											
0.30	1.33	1.03	1.00	11686.7	16582.4	127976.3	31580.4	8487.8	27047.9	9867.1	ø 8 4br. 10.0'
Trave di fondazione 9 16 Sez. 1 Rett. 90x50 [cm]											
0.00	2.24	2.24	1.00	24453.5	16582.4	127976.3	25264.3	3143.5	27047.9	7893.6	ø 8 4br. 12.5'
Trave di fondazione 16 24 Sez. 1 Rett. 90x50 [cm]											
0.30	4.01	3.71	1.00	21438.8	15154.9	127976.3	25264.3	4044.1	27047.9	7893.6	ø 8 4br. 12.5'

Travata: ***Travata 102 Nodi 105 106***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
105	0.15	6.03	6.03			4693.6	10066.4	0.12	-4246.5	-10066.4	0.12					
				SLE Rare		138.4			-13.7			0.1	1.4	55.7	13.1	
				SLE Freq.		226.3			0.0			0.0	2.3	91.1	21.4	OK
				SLE Q.P.		230.0			0.0			0.0	2.3	92.6	21.7	OK
Camp.	3.15	6.03	6.03	609.4	1584.5	0.0	10066.4	0.12	-2176.9	-10066.4	0.12					
				SLE Rare		0.0			-1633.9			16.4	0.0	154.3	658.0	
				SLE Freq.		0.0			-1607.9			16.1	0.0	151.9	647.5	OK
				SLE Q.P.		0.0			-1596.5			16.0	0.0	150.8	642.9	OK
106	6.15	6.03	6.03			6200.9	10066.4	0.12	-3937.6	-10066.4	0.12					
				SLE Rare		1192.4			0.0			0.0	12.0	480.2	112.6	
				SLE Freq.		1144.4			0.0			0.0	11.5	460.8	108.1	OK
				SLE Q.P.		1130.4			0.0			0.0	11.3	455.2	106.8	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 105 106 Sez. 1 Rett. 30x50 [cm]											
0.15	0.64	0.49	1.00	5132.4	6073.0	43615.3	16144.2	466.3	5270.6	3296.1	ø 8 2br. 10.0'
0.64	5.56	4.92	1.00	4894.2	6073.0	43615.3	10762.8	466.3	5270.6	2197.4	ø 8 2br. 15.0'
5.56	6.05	0.49	1.00	5109.0	6073.0	43615.3	16144.2	466.3	5270.6	3296.1	ø 8 2br. 10.0'

Travata: ***Travata 102 Nodi 101 102***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 3 Rett. 30x45 [cm]																
101	0.30	3.15	4.36			1146.8	4834.0	0.10	-1721.1	-6552.1	0.12					
				SLE Rare		0.0			-344.2			5.0	0.0	29.6	202.4	
				SLE Freq.		0.0			-291.7			4.3	0.0	25.1	171.5	OK
				SLE Q.P.		0.0			-273.1			4.0	0.0	23.5	160.5	OK

Camp.	3.27	4.62	4.62	484.6	1236.6	0.0	6918.0	0.12	-1437.0	-6918.0	0.12					
				SLE Rare		0.0			-950.9			13.1	0.0	112.4	559.6	
				SLE Freq.		0.0			-966.7			13.3	0.0	114.2	568.9	OK
				SLE Q.P.		0.0			-968.8			13.3	0.0	114.5	570.1	OK
102	6.23	3.15	4.36			4148.1	4834.0	0.10	-410.4	-6552.1	0.12					
				SLE Rare		2079.1			0.0			0.0	33.5	1209.5	235.8	
				SLE Freq.		1976.8			0.0			0.0	31.9	1150.0	224.2	OK
				SLE Q.P.		1942.9			0.0			0.0	31.3	1130.2	220.3	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 101 102 Sez. 3 Rett. 30x45 [cm]
0.40	0.84	0.44	1.00	3228.5	5164.0	38832.9	14374.0	231.9	4565.3	2973.9	ø 8 2br. 10.0'
0.84	5.79	4.95	1.00	3072.8	5264.3	38832.9	11499.2	231.9	4565.3	2379.1	ø 8 2br. 12.5'
5.79	6.23	0.44	1.00	3243.4	5164.0	38832.9	14374.0	231.9	4565.3	2973.9	ø 8 2br. 10.0'

Travata: ***Travata 102 Nodi 102 103 104 105***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 2 Rett. 75x25 [cm]																
102	0.14	6.21	6.21			1829.6	4839.8	0.19	-2386.1	-4839.8	0.19					
				SLE Rare		0.0			-414.2			9.5	0.0	25.4	293.3	
				SLE Freq.		0.0			-308.0			7.1	0.0	18.9	218.1	OK
				SLE Q.P.		0.0			-271.6			6.2	0.0	16.7	192.3	OK
Camp.	1.84	7.70	7.70	609.4	510.2	11.8	5806.0	0.20	-510.0	-5806.0	0.20					
				SLE Rare		0.0			-392.3			8.2	0.0	33.8	281.1	
				SLE Freq.		0.0			-392.3			8.2	0.0	33.8	281.1	OK
				SLE Q.P.		0.0			-392.3			8.2	0.0	33.8	281.1	OK
103	3.54	15.39	15.39			3369.3	10683.4	0.25	-896.2	-10683.4	0.25					
				SLE Rare		1377.6			0.0			0.0	20.5	512.8	127.9	
				SLE Freq.		1268.7			0.0			0.0	18.9	472.2	117.8	OK

				SLE Q.P.		1229.7			0.0			0.0	18.3	457.7	114.1	OK
Trave Sez. 2 Rett. 75x25 [cm]																
103	0.18	15.39	15.39			1808.0	10683.4	0.25	-2760.1	-10683.4	0.25					
				SLE Rare		0.0			-520.6			7.8	0.0	48.3	193.8	
				SLE Freq.		0.0			-487.4			7.3	0.0	45.2	181.4	OK
				SLE Q.P.		0.0			-474.0			7.1	0.0	44.0	176.4	OK
Camp.	1.69	7.70	7.70	609.4	427.4	0.0	5806.0	0.20	-512.6	-5806.0	0.20					
				SLE Rare		0.0			-369.3			7.7	0.0	31.8	264.6	
				SLE Freq.		0.0			-355.1			7.4	0.0	30.6	254.4	OK
				SLE Q.P.		0.0			-349.0			7.3	0.0	30.1	250.0	OK
104	3.20	15.39	15.39			3222.9	10683.4	0.25	-1396.2	-10683.4	0.25					
				SLE Rare		916.7			0.0			0.0	13.7	341.2	85.1	
				SLE Freq.		914.4			0.0			0.0	13.6	340.3	84.9	OK
				SLE Q.P.		913.2			0.0			0.0	13.6	339.9	84.8	OK
Trave Sez. 2 Rett. 75x25 [cm]																
104	0.15	15.39	15.39			1539.4	10683.4	0.25	-2414.9	-10683.4	0.25					
				SLE Rare		0.0			-450.2			6.7	0.0	41.8	167.6	
				SLE Freq.		0.0			-440.3			6.6	0.0	40.9	163.9	OK
				SLE Q.P.		0.0			-437.1			6.5	0.0	40.6	162.7	OK
Camp.	1.81	7.70	7.70	609.4	496.3	229.4	5806.0	0.20	-496.3	-5806.0	0.20					
				SLE Rare		96.5			-381.8			7.9	2.0	69.1	273.5	
				SLE Freq.		81.7			-381.8			7.9	1.7	58.5	273.5	OK
				SLE Q.P.		75.5			-381.8			7.9	1.6	54.1	273.5	OK
105	3.46	6.21	6.21			3748.2	4839.9	0.19	-24.7	-4839.9	0.19					
				SLE Rare		1928.0			0.0			0.0	44.3	1365.0	118.4	
				SLE Freq.		1888.6			0.0			0.0	43.4	1337.1	116.0	OK
				SLE Q.P.		1873.1			0.0			0.0	43.0	1326.1	115.1	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 102 103 Sez. 2 Rett. 75x25 [cm]											

0.14	0.39	0.25	1.00	5784.6	7941.2	49258.5	29172.9	704.3	6450.0	6129.4	ø 8 4br. 5.0'
0.39	3.29	2.90	1.00	5706.6	8532.0	49258.5	9724.3	704.3	6450.0	2689.1	ø 8 4br. 15.0'
3.29	3.54	0.25	1.00	5823.8	10232.8	49258.5	29172.9	704.3	6450.0	8067.3	ø 8 4br. 5.0'
Trave 103 104 Sez. 2 Rett. 75x25 [cm]											
0.18	0.43	0.25	1.00	7199.0	10119.7	49258.5	29172.9	343.5	6450.0	8067.3	ø 8 4br. 5.0'
0.43	2.95	2.52	1.00	8380.3	8532.0	49258.5	9724.3	343.5	6450.0	2689.1	ø 8 4br. 15.0'
2.95	3.20	0.25	1.00	8497.4	10079.8	49258.5	29172.9	343.5	6450.0	8067.3	ø 8 4br. 5.0'
Trave 104 105 Sez. 2 Rett. 75x25 [cm]											
0.15	0.40	0.25	1.00	4706.8	10203.5	49258.5	29172.9	334.8	6450.0	8067.3	ø 8 4br. 5.0'
0.40	3.21	2.81	1.00	5817.4	8532.0	49258.5	9724.3	334.8	6450.0	2689.1	ø 8 4br. 15.0'
3.21	3.46	0.25	1.00	5934.6	7941.2	49258.5	29172.9	334.8	6450.0	6129.5	ø 8 4br. 5.0'

Travata: ***Travata 105 Nodi 113 114 115***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 3 Rett. 30x45 [cm]																
113	0.52	3.92	4.62			2038.9	5925.3	0.11	-3445.4	-6918.5	0.12					
				SLE Rare		19.4			-351.1			4.9	0.3	36.2	206.7	
				SLE Freq.		0.0			-599.3			8.4	0.0	61.8	352.8	OK
				SLE Q.P.		0.0			-597.5			8.4	0.0	61.6	351.8	OK
Camp.	2.39	4.62	4.62	3857.7	4926.0	0.0	6918.0	0.12	-4926.0	-6918.0	0.12					
				SLE Rare		0.0			-3584.9			49.4	0.0	423.6	2109.8	
				SLE Freq.		0.0			-2938.9			40.5	0.0	347.3	1729.6	OK
				SLE Q.P.		0.0			-2685.3			37.0	0.0	317.3	1580.3	OK
114	4.27	6.80	9.24			7583.9	9997.7	0.13	0.0	-13417.9	0.16					
				SLE Rare		5612.1			0.0			0.0	59.9	2167.4	547.3	
				SLE Freq.		4891.0			0.0			0.0	52.2	1888.9	477.0	OK
				SLE Q.P.		4603.9			0.0			0.0	49.2	1778.0	449.0	OK
Trave Sez. 3 Rett. 30x45 [cm]																
114	0.25	6.80	9.24			4019.6	9997.7	0.13	0.0	-13417.9	0.16					
				SLE Rare		2888.0			0.0			0.0	30.8	1116.9	281.7	

				SLE Freq.		2225.4			0.0			0.0	23.8	860.6	217.0	OK
				SLE Q.P.		1958.9			0.0			0.0	20.9	757.6	191.0	OK
Camp.	2.17	4.62	4.62	3857.7	4013.6	0.0	6918.0	0.12	-3988.7	-6918.0	0.12					
				SLE Rare		0.0			-2902.8			40.0	0.0	343.0	1708.3	
				SLE Freq.		0.0			-2365.1			32.6	0.0	279.5	1391.9	OK
				SLE Q.P.		0.0			-2150.1			29.6	0.0	254.0	1265.3	OK
115	4.08	3.44	4.62			4088.4	5249.4	0.11	0.0	-6918.9	0.12					
				SLE Rare		3028.9			0.0			0.0	46.8	1766.5	360.5	
				SLE Freq.		2651.3			0.0			0.0	41.0	1546.3	315.5	OK
				SLE Q.P.		2501.7			0.0			0.0	38.6	1459.0	297.7	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 113 114 Sez. 3 Rett. 30x45 [cm]
0.81	1.22	0.41	1.00	10022.0	5264.3	38832.9	14374.0	283.1	4565.3	2973.9	ø 8 2br. 10.0'
1.22	3.81	2.59	1.00	8978.5	5264.3	38832.9	11499.2	283.1	4565.3	2379.1	ø 8 2br. 12.5'
3.81	4.22	0.41	1.00	9764.9	5683.7	38832.9	14374.0	283.1	4565.3	2973.9	ø 8 2br. 10.0'
											Trave 114 115 Sez. 3 Rett. 30x45 [cm]
0.30	0.74	0.44	1.00	8742.3	5679.3	38832.9	14374.0	1340.0	4565.3	2973.9	ø 8 2br. 10.0'
0.74	3.64	2.89	1.00	8705.0	5264.3	38832.9	11499.2	1340.0	4565.3	2379.1	ø 8 2br. 12.5'
3.64	4.08	0.44	1.00	9667.2	5264.3	38832.9	14374.0	1340.0	4565.3	2973.9	ø 8 2br. 10.0'

Travata: ***Travata 108 Nodi 113 120***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 3 Rett. 30x45 [cm]																
113	0.30	5.67	4.36			7954.0	8402.2	0.13	-451.6	-6550.8	0.11					
				SLE Rare		3900.1			0.0			0.0	50.1	1883.8	432.9	
				SLE Freq.		3820.1			0.0			0.0	49.1	1845.1	424.0	OK
				SLE Q.P.		3788.5			0.0			0.0	48.7	1829.9	420.5	OK
Camp.	2.60	4.62	4.62	484.6	818.9	0.0	6918.0	0.12	-1724.1	-6918.0	0.12					
				SLE Rare		0.0			-847.9			11.7	0.0	100.2	499.0	

				SLE Freq.		0.0			-835.1			11.5	0.0	98.7	491.4	OK
				SLE Q.P.		0.0			-830.0			11.4	0.0	98.1	488.4	OK
120	4.90	3.15	6.07			1592.4	4836.0	0.11	-8011.7	-8970.8	0.14					
				SLE Rare		0.0			-3354.6			43.5	0.0	280.0	1518.6	
				SLE Freq.		0.0			-3246.0			42.0	0.0	270.9	1469.5	OK
				SLE Q.P.		0.0			-3203.1			41.5	0.0	267.3	1450.1	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 113 120 Sez. 3 Rett. 30x45 [cm]
0.40	0.83	0.43	1.00	5049.0	5164.0	38832.9	14374.0	360.7	4565.3	2973.9	ø 8 2br. 10.0'
0.83	4.37	3.55	1.00	4874.0	5264.3	38832.9	11499.2	360.7	4565.3	2379.1	ø 8 2br. 12.5'
4.37	4.80	0.43	1.00	3617.5	5766.9	38832.9	14374.0	360.7	4565.3	2973.9	ø 8 2br. 10.0'

Travata: ***Travata 110 Nodi 136 107 115 122***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
			Trave Sez. 3 Rett. 30x45 [cm]													
136	0.05	1.69	2.34			99.5	2740.1	0.09	-157.2	-3661.0	0.09					
				SLE Rare		0.0			-116.1			2.3	0.0	5.7	66.9	
				SLE Freq.		0.0			-92.1			1.8	0.0	4.5	53.1	OK
				SLE Q.P.		0.0			-82.5			1.6	0.0	4.0	47.5	OK
Camp.	0.97	9.46	5.30	4041.9	911.9	3092.3	13698.1	0.17	-910.4	-7877.3	0.12					
				SLE Rare		1613.7			-662.3			7.7	17.0	477.4	340.6	
				SLE Freq.		1389.4			-538.9			6.3	14.6	411.1	277.2	OK
				SLE Q.P.		1299.5			-489.5			5.7	13.7	384.5	251.8	OK
107	1.90	14.67	9.24			7985.1	20948.9	0.20	0.0	-13418.3	0.13					
				SLE Rare		5852.9			0.0			0.0	48.9	1131.4	526.5	
				SLE Freq.		4912.4			0.0			0.0	41.1	949.6	441.9	OK
				SLE Q.P.		4535.8			0.0			0.0	37.9	876.8	408.0	OK
			Trave Sez. 3 Rett. 30x45 [cm]													
107	0.50	15.74	10.27			14771.6	22432.4	0.20	-261.3	-14869.8	0.14					

				SLE Rare		7844.8			0.0			0.0	62.8	1410.2	679.9	
				SLE Freq.		7407.1			0.0			0.0	59.3	1331.5	642.0	OK
				SLE Q.P.		7232.2			0.0			0.0	57.9	1300.1	626.8	OK
Camp.	1.00	16.03	15.03	4041.8	568.4	6810.7	22889.2	0.17	-547.0	-21507.9	0.16					
				SLE Rare		3268.8			-398.0			2.9	23.6	573.9	250.6	
				SLE Freq.		2882.1			-323.8			2.3	20.8	506.0	221.0	OK
				SLE Q.P.		2727.6			-294.1			2.1	19.7	478.9	209.1	OK
115	1.50	16.29	17.03			4823.4	23252.3	0.17	-6477.2	-24279.3	0.18					
				SLE Rare		0.0			-407.2			2.8	0.0	29.9	67.6	
				SLE Freq.		0.0			-860.7			6.0	0.0	63.1	142.8	OK
				SLE Q.P.		0.0			-860.9			6.0	0.0	63.2	142.9	OK
***Trave Sez. 3 Rett. 30x45 [cm]* Area tirante a taglio insufficiente**																
115	0.50	16.08	16.68			21499.0	22960.0	0.17	0.0	-23791.7	0.17					
				SLE Rare		12777.5			0.0			0.0	89.4	2234.1	942.6	
				SLE Freq.		11871.9			0.0			0.0	83.1	2075.7	875.8	OK
				SLE Q.P.		11511.1			0.0			0.0	80.5	2012.7	849.2	OK
Camp.	2.60	6.03	12.06	4041.8	6830.7	0.0	8882.8	0.12	-8402.1	-17240.6	0.20					
				SLE Rare		0.0			-5968.3			57.3	0.0	602.8	1398.1	
				SLE Freq.		0.0			-5110.3			49.1	0.0	516.2	1197.1	OK
				SLE Q.P.		0.0			-4767.3			45.8	0.0	481.5	1116.8	OK
122	4.70	5.97	16.08			5868.6	8794.1	0.12	-21655.1	-22459.7	0.28					
				SLE Rare		0.0			-7335.9			64.9	0.0	529.4	1307.3	
				SLE Freq.		0.0			-7941.4			70.2	0.0	573.1	1415.2	OK
				SLE Q.P.		0.0			-7938.8			70.2	0.0	572.9	1414.7	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 136 107 Sez. 3 Rett. 30x45 [cm]											
0.05	1.90	1.85	1.00	16728.7	4732.3	38832.9	19165.4	268.4	4565.3	2087.7	ø 8 2br. 7.5'
***Trave 107 115 Sez. 3 Rett. 30x45 [cm]* Vd 52596.3 > VR_{cd}38832.9**											

0.73	1.50	0.77	1.00	52596.3	6871.9	38832.9	28748.0	1032.5	4565.3	5947.9	ø 8 2br. 5.0'
Trave 115 122 Sez. 3 Rett. 30x45 [cm]											
0.76	4.44	3.67	1.00	17190.5	7250.1	38832.9	19165.4	159.9	4565.3	3965.2	ø 8 2br. 7.5'

Travata: ***Travata 111 Nodi 137 108 123***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 3 Rett. 30x45 [cm] **EC2 4.4.2.3. Fessurazione : tensione eccessiva barre di Estradosso**																
137	0.05	3.22	6.68			509.5	4926.6	0.11	-10.9	-9795.7	0.15					
					SLE Rare	42.9			-6.2			0.1	0.7	14.4	2.5	
					SLE Freq.	34.1			-7.4			0.1	0.5	11.5	2.0	OK
					SLE Q.P.	30.7			-7.4			0.1	0.5	10.3	1.8	OK
Camp.	0.97	8.04	12.06	6247.1	1409.5	6487.7	11703.7	0.13	-1404.6	-17290.9	0.18					
					SLE Rare	3524.7			-1019.3			9.3	33.7	1210.9	309.6	
					SLE Freq.	3001.6			-820.7			7.5	28.7	1031.2	263.7	OK
					SLE Q.P.	2793.5			-741.3			6.8	26.7	959.7	245.4	OK
108	1.90	8.04	12.06			14942.8	11703.7	0.13	0.0	-17290.9	0.18					
					SLE Rare	10940.2			0.0			0.0	104.5	3758.5	961.0	
					SLE Freq.	9138.1			0.0			0.0	87.3	3139.4	802.7	
					SLE Q.P.	8419.4			0.0			0.0	80.4	2892.5	739.5	
Trave Sez. 3 Rett. 30x45 [cm] **Sigma cls intr. > Sigma amm.**																
108	0.50	8.04	12.06			28669.0	11703.7	0.13	0.0	-17290.9	0.18					
					SLE Rare	21189.0			0.0			0.0	202.4	7279.5	1861.2	
					SLE Freq.	18429.3			0.0			0.0	176.0	6331.4	1618.8	
					SLE Q.P.	17325.9			0.0			0.0	165.5	5952.3	1521.9	
Camp.	3.45	8.04	12.06	7434.5	20858.6	0.0	11703.7	0.13	-20858.6	-17290.9	0.18					
					SLE Rare	0.0			-15126.5			138.3	0.0	1436.7	3530.2	
					SLE Freq.	0.0			-12141.3			111.0	0.0	1153.2	2833.5	
					SLE Q.P.	0.0			-10947.3			100.1	0.0	1039.8	2554.8	
123	6.40	10.05	16.08			13784.9	14520.6	0.14	-7988.8	-22846.2	0.21					
					SLE Rare	7945.9			0.0			0.0	65.1	2192.6	615.2	
					SLE Freq.	4664.7			0.0			0.0	38.2	1287.2	361.2	OK
					SLE Q.P.	3351.4			0.0			0.0	27.4	924.8	259.5	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 137 108 Sez. 3 Rett. 30x45 [cm]											
0.05	1.90	1.85	1.00	15653.8	5954.3	38832.9	28748.0	827.1	4565.3	5138.2	ø 8 2br. 5.0'
Trave 108 123 Sez. 3 Rett. 30x45 [cm]											
0.78	6.31	5.53	1.00	26122.5	7250.1	38832.9	28748.0	100.6	4565.3	5947.9	ø 8 2br. 5.0'

Travata: ***Travata 112 Nodi 101 109 116 124***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 3 Rett. 30x45 [cm]																
101	0.50	12.06	8.04			14904.9	17290.9	0.18	-999.6	-11703.7	0.13					
				SLE Rare		8220.5			-23.5			0.2	75.2	1918.4	780.8	
				SLE Freq.		7578.6			-18.9			0.2	69.3	1768.7	719.8	OK
				SLE Q.P.		7320.8			-17.1			0.2	66.9	1708.5	695.3	OK
Camp.	0.92	12.06	8.04	6336.5	700.5	10203.0	17290.9	0.18	-2750.6	-11703.7	0.13					
				SLE Rare		2741.4			-484.8			4.6	25.1	639.8	260.4	
				SLE Freq.		2871.0			-390.2			3.7	26.3	670.0	272.7	OK
				SLE Q.P.		2871.0			-352.4			3.4	26.3	670.0	272.7	OK
109	1.33	12.06	8.04			4029.8	17290.9	0.18	-3263.2	-11703.7	0.13					
				SLE Rare		0.0			-1407.5			13.4	0.0	123.6	483.5	
				SLE Freq.		0.0			-740.0			7.1	0.0	65.0	254.2	OK
				SLE Q.P.		0.0			-472.0			4.5	0.0	41.5	162.1	OK
Trave Sez. 3 Rett. 30x45 [cm]																
109	0.00	12.06	8.04			3398.3	17290.9	0.18	-3742.3	-11703.7	0.13					
				SLE Rare		0.0			-1103.3			10.5	0.0	96.9	379.0	
				SLE Freq.		0.0			-388.9			3.7	0.0	34.2	133.6	OK
				SLE Q.P.		0.0			-102.5			1.0	0.0	9.0	35.2	OK
Camp.	1.14	10.05	6.03	8032.9	3239.1	0.0	14489.3	0.17	-5279.4	-8883.8	0.12					
				SLE Rare		0.0			-3809.3			42.1	0.0	362.1	1732.4	
				SLE Freq.		0.0			-3136.1			34.6	0.0	298.1	1426.2	OK

				SLE Q.P.		0.0			-2866.9			31.7	0.0	272.5	1303.8	OK
116	2.29	16.21	13.53			6366.6	23118.8	0.18	-5897.6	-19395.4	0.15					
				SLE Rare		1645.1			0.0			0.0	12.2	287.2	129.7	
				SLE Freq.		640.5			-23.2			0.2	4.8	111.8	50.5	OK
				SLE Q.P.		237.8			-22.7			0.2	1.8	41.5	18.8	OK
Trave Sez. 3 Rett. 30x45 [cm]																
116	0.25	16.21	18.10			18670.4	23153.3	0.16	0.0	-25755.8	0.18					
				SLE Rare		12879.9			0.0			0.0	87.6	2235.9	910.3	
				SLE Freq.		11780.5			0.0			0.0	80.1	2045.0	832.6	OK
				SLE Q.P.		11330.4			0.0			0.0	77.0	1966.9	800.8	OK
Camp.	2.05	6.16	12.06	8036.2	8691.9	0.0	9083.4	0.12	-9477.5	-17270.8	0.20					
				SLE Rare		0.0			-6880.3			65.7	0.0	697.0	1610.2	
				SLE Freq.		0.0			-5837.8			55.8	0.0	591.4	1366.2	OK
				SLE Q.P.		0.0			-5418.7			51.8	0.0	548.9	1268.1	OK
124	3.86	8.22	16.08			4879.8	11967.3	0.13	-17664.8	-22781.5	0.23					
				SLE Rare		0.0			-5450.9			45.6	0.0	495.7	965.7	
				SLE Freq.		0.0			-6448.0			53.9	0.0	586.3	1142.4	OK
				SLE Q.P.		0.0			-6466.6			54.1	0.0	588.0	1145.7	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 101 109 Sez. 3 Rett. 30x45 [cm] **Vd 39960.1 > VR_{cd}38832.9**											
0.72	1.33	0.61	1.00	39960.1	6333.5	38832.9	28748.0	641.3	4565.3	5947.9	ø 8 2br. 5.0'
Trave 109 116 Sez. 3 Rett. 30x45 [cm]											
0.00	2.24	2.24	1.00	23052.8	5754.4	38832.9	28748.0	284.7	4565.3	5947.9	ø 8 2br. 5.0'
Trave 116 124 Sez. 3 Rett. 30x45 [cm]											
0.30	3.76	3.47	1.00	22038.1	7250.1	38832.9	28748.0	277.6	4565.3	5947.9	ø 8 2br. 5.0'

Travata: ***Travata 114 Nodi 103 110 126***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	w mm
Trave Sez. 1 Rett. 30x50 [cm]																

103	0.50	8.04	7.57			9145.3	13279.1	0.13	-6349.0	-12531.1	0.12					
				SLE Rare		1322.9			0.0			0.0	11.6	402.8	116.2	
				SLE Freq.		1398.8			0.0			0.0	12.2	425.9	122.9	OK
				SLE Q.P.		1403.7			0.0			0.0	12.3	427.4	123.3	OK
Camp.	1.30	8.04	6.12	5324.4	1467.5	4762.3	13274.0	0.13	-1818.7	-10210.8	0.11					
				SLE Rare		1875.7			-1050.0			10.0	17.0	572.3	416.0	
				SLE Freq.		1808.4			-860.3			8.2	16.4	551.7	340.9	OK
				SLE Q.P.		1782.8			-784.4			7.5	16.1	543.9	310.8	OK
110	2.10	10.56	13.47			8548.2	17288.1	0.13	0.0	-21897.3	0.16					
				SLE Rare		5970.6			0.0			0.0	42.0	1388.9	425.6	
				SLE Freq.		5114.0			0.0			0.0	36.0	1189.7	364.5	OK
				SLE Q.P.		4777.8			0.0			0.0	33.6	1111.4	340.6	OK
Trave Sez. 1 Rett. 30x50 [cm]																
110	0.50	13.13	14.06			14791.2	21385.7	0.14	0.0	-22863.8	0.15					
				SLE Rare		11015.3			0.0			0.0	71.6	2073.9	754.4	
				SLE Freq.		10118.9			0.0			0.0	65.7	1905.1	693.0	OK
				SLE Q.P.		9763.6			0.0			0.0	63.4	1838.2	668.7	OK
Camp.	3.06	6.03	12.66	3010.5	6616.5	0.0	10065.0	0.11	-7361.6	-20542.8	0.19					
				SLE Rare		0.0			-5421.4			42.4	0.0	462.8	1072.7	
				SLE Freq.		0.0			-4667.3			36.5	0.0	398.5	923.5	OK
				SLE Q.P.		0.0			-4366.2			34.1	0.0	372.8	863.9	OK
126	5.63	7.91	9.50			2791.0	13081.3	0.12	-12429.5	-15599.3	0.14					
				SLE Rare		0.0			-4395.0			36.0	0.0	369.8	1138.7	
				SLE Freq.		0.0			-4859.7			39.8	0.0	408.9	1259.1	OK
				SLE Q.P.		0.0			-4854.3			39.8	0.0	408.5	1257.7	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 103 110 Sez. 1 Rett. 30x50 [cm]											
0.75	2.10	1.35	1.00	25329.5	6073.0	43615.3	32288.4	1280.4	5270.6	6592.1	ø 8 2br. 5.0'
Trave 110 126 Sez. 1 Rett. 30x50 [cm]											

0.78	1.24	0.46	1.00	12669.5	6906.7	43615.3	16144.2	574.2	5270.6	3296.1	ø 8 2br. 10.0'
1.24	2.61	1.37	1.00	11745.4	6684.2	43615.3	12915.4	574.2	5270.6	2636.9	ø 8 2br. 12.5'
2.61	3.70	1.09	1.00	9016.9	7775.7	43615.3	10762.8	574.2	5270.6	2197.4	ø 8 2br. 15.0'
3.70	5.07	1.37	1.00	11520.8	6798.3	43615.3	12915.4	574.2	5270.6	2636.9	ø 8 2br. 12.5'
5.07	5.54	0.46	1.00	12443.2	7064.7	43615.3	16144.2	574.2	5270.6	3296.1	ø 8 2br. 10.0'

Travata: ***Travata 115 Nodi 104 111 127***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
104	0.50	5.97	6.03			6842.3	9967.0	0.12	-5179.7	-10066.5	0.12					
				SLE Rare		771.9			0.0			0.0	7.8	233.0	73.0	
				SLE Freq.		831.7			0.0			0.0	8.4	251.1	78.6	OK
				SLE Q.P.		835.7			0.0			0.0	8.4	252.3	79.0	OK
Camp.	1.30	8.04	6.03	5289.9	1458.0	4031.8	13273.6	0.13	-1431.6	-10065.1	0.11					
				SLE Rare		1969.2			-1043.2			10.0	17.9	600.9	419.4	
				SLE Freq.		1888.6			-854.9			8.2	17.1	576.3	343.7	OK
				SLE Q.P.		1857.6			-779.6			7.5	16.8	566.8	313.4	OK
111	2.10	10.56	13.47			9023.1	17288.1	0.13	0.0	-21897.3	0.16					
				SLE Rare		6676.9			0.0			0.0	47.0	1553.2	476.0	
				SLE Freq.		5817.4			0.0			0.0	40.9	1353.3	414.7	OK
				SLE Q.P.		5479.3			0.0			0.0	38.6	1274.6	390.6	OK
Trave Sez. 1 Rett. 30x50 [cm]																
111	0.50	13.13	14.06			13623.6	21385.7	0.14	0.0	-22863.8	0.15					
				SLE Rare		10215.5			0.0			0.0	66.4	1923.3	699.6	
				SLE Freq.		9355.9			0.0			0.0	60.8	1761.5	640.8	OK
				SLE Q.P.		9015.1			0.0			0.0	58.6	1697.3	617.4	OK
Camp.	3.06	6.03	12.66	2978.4	6545.9	0.0	10065.0	0.11	-7142.4	-20542.8	0.19					
				SLE Rare		0.0			-5263.9			41.1	0.0	449.4	1041.5	
				SLE Freq.		0.0			-4515.6			35.3	0.0	385.5	893.4	OK

				SLE Q.P.		0.0			-4216.7			33.0	0.0	360.0	834.3	OK
127	5.63	6.03	8.04			2386.8	10065.1	0.11	-10218.4	-13273.6	0.13					
				SLE Rare		0.0			-3458.0			31.4	0.0	315.7	1055.1	
				SLE Freq.		0.0			-3929.2			35.6	0.0	358.7	1198.9	OK
				SLE Q.P.		0.0			-3923.9			35.6	0.0	358.2	1197.3	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 104 111 Sez. 1 Rett. 30x50 [cm]											
0.75	2.10	1.35	1.00	21874.8	6073.0	43615.3	32288.4	810.8	5270.6	6424.3	ø 8 2br. 5.0'
Trave 111 127 Sez. 1 Rett. 30x50 [cm]											
0.78	1.24	0.46	1.00	12122.0	6906.7	43615.3	16144.2	209.0	5270.6	3296.1	ø 8 2br. 10.0'
1.24	2.69	1.45	1.00	11207.7	6684.2	43615.3	12915.4	209.0	5270.6	2636.9	ø 8 2br. 12.5'
2.69	3.62	0.93	1.00	8344.2	7775.7	43615.3	10762.8	209.0	5270.6	2197.4	ø 8 2br. 15.0'
3.62	5.07	1.45	1.00	10836.7	6684.2	43615.3	12915.4	209.0	5270.6	2636.9	ø 8 2br. 12.5'
5.07	5.54	0.46	1.00	11750.9	6684.2	43615.3	16144.2	209.0	5270.6	3296.1	ø 8 2br. 10.0'

Travata: ***Travata 116 Nodi 105 112 128***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
105	0.50	5.97	6.03			7368.6	9967.0	0.12	-2784.6	-10066.5	0.12					
				SLE Rare		2553.5			0.0			0.0	25.7	770.9	241.5	
				SLE Freq.		2361.1			0.0			0.0	23.8	712.9	223.3	OK
				SLE Q.P.		2280.6			0.0			0.0	23.0	688.5	215.7	OK
Camp.	1.30	10.06	6.03	7428.9	2047.6	3733.8	16468.0	0.15	-2010.4	-10065.2	0.11					
				SLE Rare		2191.9			-1462.7			13.4	18.4	539.1	587.2	
				SLE Freq.		2011.0			-1190.5			10.9	16.9	494.6	477.9	OK
				SLE Q.P.		1939.5			-1081.6			9.9	16.3	477.0	434.2	OK
112	2.10	13.69	13.64			10394.0	22294.7	0.15	0.0	-22210.0	0.15					
				SLE Rare		6708.3			0.0			0.0	43.3	1215.8	461.6	
				SLE Freq.		5630.8			0.0			0.0	36.4	1020.5	387.4	OK

				SLE Q.P.		5205.2			0.0			0.0	33.6	943.4	358.1	OK
Trave Sez. 1 Rett. 30x50 [cm]																
112	0.50	16.27	14.06			20448.1	26373.5	0.16	0.0	-22885.2	0.14					
				SLE Rare		15103.0			0.0			0.0	92.1	2318.6	1006.8	
				SLE Freq.		13066.6			0.0			0.0	79.6	2006.0	871.1	OK
				SLE Q.P.		12254.7			0.0			0.0	74.7	1881.4	817.0	OK
Camp.	2.96	6.03	12.66	7428.9	16327.3	0.0	10065.0	0.11	-16327.3	-20542.8	0.19					
				SLE Rare		0.0			-11879.1			92.8	0.0	1014.2	2350.4	
				SLE Freq.		0.0			-9668.1			75.6	0.0	825.4	1912.9	OK
				SLE Q.P.		0.0			-8783.8			68.6	0.0	749.9	1738.0	OK
128	5.43	8.64	8.04			10331.9	14244.9	0.13	-3098.8	-13281.2	0.12					
				SLE Rare		7232.6			0.0			0.0	60.9	2049.8	613.8	
				SLE Freq.		4910.1			0.0			0.0	41.4	1391.6	416.7	OK
				SLE Q.P.		3977.7			0.0			0.0	33.5	1127.3	337.6	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 105 112 Sez. 1 Rett. 30x50 [cm]											
0.75	2.10	1.35	1.00	26508.2	6073.0	43615.3	32288.4	909.9	5270.6	6424.3	ø 8 2br. 5.0'
Trave 112 128 Sez. 1 Rett. 30x50 [cm]											
0.77	1.21	0.45	1.00	22371.9	6906.7	43615.3	32288.4	544.1	5270.6	6592.1	ø 8 2br. 5.0'
1.21	4.72	3.50	1.00	18205.4	6684.2	43615.3	21525.6	544.1	5270.6	4394.8	ø 8 2br. 7.5'
4.72	5.16	0.45	1.00	19502.1	6684.2	43615.3	32288.4	544.1	5270.6	6592.1	ø 8 2br. 5.0'

Travata: ***Travata 55 Nodi 102 117 125***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
102	0.50	12.52	9.11			19533.4	20395.4	0.16	-5132.0	-14994.8	0.12					
				SLE Rare		8503.4			0.0			0.0	62.1	1687.3	671.8	
				SLE Freq.		7829.5			0.0			0.0	57.2	1553.6	618.6	OK
				SLE Q.P.		7550.6			0.0			0.0	55.1	1498.3	596.5	OK

Camp.	2.06	8.04	9.11	9008.3	8432.3	0.0	13281.8	0.12	-8432.3	-14990.0	0.13					
				SLE Rare		0.0			-6196.9			51.3	0.0	522.4	1674.5	
				SLE Freq.		0.0			-5256.2			43.5	0.0	443.1	1420.3	OK
				SLE Q.P.		0.0			-4879.9			40.4	0.0	411.3	1318.6	OK
117	3.62	9.82	14.07			12524.7	16120.3	0.12	-8330.4	-22843.3	0.17					
				SLE Rare		3411.8			0.0			0.0	24.3	732.1	241.2	
				SLE Freq.		2470.0			0.0			0.0	17.6	530.0	174.6	OK
				SLE Q.P.		2103.7			0.0			0.0	15.0	451.4	148.7	OK
Trave Sez. 1 Rett. 30x50 [cm]																
117	0.25	15.01	14.07			24072.6	24378.0	0.15	-27.3	-22893.1	0.14					
				SLE Rare		14416.8			0.0			0.0	90.0	2071.5	971.1	
				SLE Freq.		13359.0			0.0			0.0	83.4	1919.5	899.8	OK
				SLE Q.P.		12942.3			0.0			0.0	80.8	1859.6	871.8	OK
Camp.	1.96	6.03	13.23	9008.1	9743.3	0.0	10062.5	0.11	-10402.3	-21404.0	0.20					
				SLE Rare		0.0			-7591.9			58.6	0.0	644.4	1438.3	
				SLE Freq.		0.0			-6650.2			51.3	0.0	564.5	1259.9	OK
				SLE Q.P.		0.0			-6273.7			48.4	0.0	532.5	1188.6	OK
125	3.66	9.11	16.08			7474.1	14994.5	0.12	-19258.1	-25969.7	0.20					
				SLE Rare		0.0			-5251.6			35.6	0.0	399.9	820.0	
				SLE Freq.		0.0			-5953.2			40.4	0.0	453.3	929.5	OK
				SLE Q.P.		0.0			-5944.9			40.3	0.0	452.7	928.2	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 102 117 Sez. 1 Rett. 30x50 [cm]											
0.77	1.22	0.45	1.00	24394.0	6844.3	43615.3	32288.4	299.6	5270.6	6592.1	ø 8 2br. 5.0'
1.22	3.13	1.91	1.00	21461.4	6325.7	43615.3	21525.6	299.6	5270.6	4394.8	ø 8 2br. 7.5'
3.13	3.58	0.45	1.00	20119.7	6585.7	43615.3	32288.4	299.6	5270.6	6592.1	ø 8 2br. 5.0'
Trave 117 125 Sez. 1 Rett. 30x50 [cm]											
0.30	3.39	3.09	1.00	26155.3	6684.2	43615.3	32288.4	713.6	5270.6	6592.1	ø 8 2br. 5.0'

Travata: ***Travata 74 Nodi 107 108 109***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 3 Rett. 30x45 [cm]																
107	0.30	3.15	4.36			832.5	4834.0	0.10	-3114.7	-6552.1	0.12					
				SLE Rare		0.0			-1110.5			16.3	0.0	95.4	652.7	
				SLE Freq.		0.0			-1145.4			16.8	0.0	98.4	673.3	OK
				SLE Q.P.		0.0			-1143.8			16.7	0.0	98.2	672.3	OK
Camp.	2.82	4.62	4.62	484.6	909.5	0.0	6918.0	0.12	-1252.9	-6918.0	0.12					
				SLE Rare		0.0			-888.1			12.2	0.0	104.9	522.6	
				SLE Freq.		0.0			-902.9			12.4	0.0	106.7	531.4	OK
				SLE Q.P.		0.0			-904.3			12.4	0.0	106.8	532.2	OK
108	5.33	5.97	9.24			3552.0	8822.2	0.12	0.0	-13411.7	0.16					
				SLE Rare		1902.6			0.0			0.0	21.3	680.8	187.2	
				SLE Freq.		1904.6			0.0			0.0	21.3	681.5	187.4	OK
				SLE Q.P.		1899.9			0.0			0.0	21.3	679.9	186.9	OK
Trave Sez. 3 Rett. 30x45 [cm]																
108	0.13	5.97	9.24			615.4	8822.2	0.12	0.0	-13411.7	0.16					
				SLE Rare		403.2			0.0			0.0	4.5	139.4	39.7	
				SLE Freq.		354.3			0.0			0.0	4.0	122.5	34.9	OK
				SLE Q.P.		340.8			0.0			0.0	3.8	117.8	33.5	OK
Camp.	2.62	4.62	4.62	0.0	0.0	519.4	6918.0	0.12	0.0	-6918.0	0.12					
				SLE Rare		362.5			0.0			0.0	5.0	213.3	42.8	
				SLE Freq.		381.1			0.0			0.0	5.2	224.3	45.0	OK
				SLE Q.P.		381.3			0.0			0.0	5.2	224.4	45.0	OK
109	5.11	4.62	4.62			872.3	6918.0	0.12	-42.1	-6918.0	0.12					
				SLE Rare		330.8			0.0			0.0	4.6	194.7	39.1	
				SLE Freq.		413.9			0.0			0.0	5.7	243.6	48.9	OK
				SLE Q.P.		421.8			0.0			0.0	5.8	248.2	49.8	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 107 108 Sez. 3 Rett. 30x45 [cm]
0.40	0.84	0.44	1.00	4381.6	5164.0	38832.9	14374.0	1011.6	4565.3	2973.9	ø 8 2br. 10.0'
0.84	4.89	4.05	1.00	4210.5	5264.3	38832.9	11499.2	1011.6	4565.3	2379.1	ø 8 2br. 12.5'
4.89	5.33	0.44	1.00	4327.6	5668.9	38832.9	14374.0	1011.6	4565.3	2973.9	ø 8 2br. 10.0'
											Trave 108 109 Sez. 3 Rett. 30x45 [cm]
0.13	0.57	0.45	1.00	481.4	5756.8	38832.9	14374.0	1160.2	4565.3	2973.9	ø 8 2br. 10.0'
0.57	4.66	4.09	1.00	481.4	5264.3	38832.9	11499.2	1160.2	4565.3	2379.1	ø 8 2br. 12.5'
4.66	5.11	0.45	1.00	481.4	5264.3	38832.9	14374.0	1160.2	4565.3	2973.9	ø 8 2br. 10.0'

Travata: ***Travata 202 Nodi 202 203 204 205 206***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
				Trave Sez. 2 Rett. 75x25 [cm]												
202	0.14	10.18	7.45			5837.7	7394.0	0.22	-1700.1	-5652.1	0.20					
				SLE Rare		2969.5			0.0			0.0	55.5	1629.4	235.2	
				SLE Freq.		2364.9			0.0			0.0	44.2	1297.7	187.3	OK
				SLE Q.P.		2142.8			0.0			0.0	40.0	1175.8	169.7	OK
Camp.	1.84	7.70	9.24	4160.1	3483.0	0.0	5809.7	0.20	-3481.6	-6791.8	0.21					
				SLE Rare		0.0			-2574.8			49.8	0.0	242.8	1550.4	
				SLE Freq.		0.0			-2239.0			43.3	0.0	211.1	1348.2	OK
				SLE Q.P.		0.0			-2104.7			40.7	0.0	198.5	1267.3	OK
203	3.54	15.39	16.93			5179.3	10682.5	0.25	-863.1	-11648.6	0.27					
				SLE Rare		2640.2			0.0			0.0	38.8	983.7	238.7	
				SLE Freq.		2366.3			0.0			0.0	34.8	881.6	213.9	OK
				SLE Q.P.		2252.3			0.0			0.0	33.1	839.2	203.6	OK
				Trave Sez. 2 Rett. 75x25 [cm]												
203	0.18	15.39	16.93			4028.2	10682.5	0.25	-1114.2	-11648.6	0.27					
				SLE Rare		1872.4			0.0			0.0	27.5	697.6	169.3	
				SLE Freq.		1632.5			0.0			0.0	24.0	608.2	147.6	OK
				SLE Q.P.		1533.3			0.0			0.0	22.6	571.3	138.6	OK

Camp.	1.69	7.70	7.70	4162.6	2919.7	0.0	5806.0	0.20	-2918.0	-5806.0	0.20					
				SLE Rare		0.0			-2158.0			44.9	0.0	186.1	1546.1	
				SLE Freq.		0.0			-1876.6			39.0	0.0	161.8	1344.4	OK
				SLE Q.P.		0.0			-1764.0			36.7	0.0	152.1	1263.8	OK
204	3.20	15.39	17.75			4691.9	10674.6	0.25	-626.7	-12119.8	0.27					
				SLE Rare		2580.7			0.0			0.0	37.8	962.6	231.5	
				SLE Freq.		2253.1			0.0			0.0	33.0	840.4	202.1	OK
				SLE Q.P.		2123.3			0.0			0.0	31.1	792.0	190.5	OK
Trave Sez. 2 Rett. 75x25 [cm]																
204	0.15	15.39	17.75			4756.4	10674.6	0.25	-1140.0	-12119.8	0.27					
				SLE Rare		2377.0			0.0			0.0	34.8	886.6	213.3	
				SLE Freq.		2032.7			0.0			0.0	29.8	758.2	182.4	OK
				SLE Q.P.		1895.3			0.0			0.0	27.8	706.9	170.0	OK
Camp.	1.81	7.70	10.05	4162.6	3390.5	0.0	5823.1	0.21	-3390.5	-7274.1	0.22					
				SLE Rare		0.0			-2507.5			47.3	0.0	244.7	1400.0	
				SLE Freq.		0.0			-2180.4			41.2	0.0	212.8	1217.4	OK
				SLE Q.P.		0.0			-2049.6			38.7	0.0	200.0	1144.4	OK
205	3.46	15.39	17.75			5176.4	10674.6	0.25	-1461.0	-12119.8	0.27					
				SLE Rare		2252.0			0.0			0.0	33.0	840.0	202.0	
				SLE Freq.		2039.0			0.0			0.0	29.9	760.6	182.9	OK
				SLE Q.P.		1954.2			0.0			0.0	28.6	728.9	175.3	OK
Trave Sez. 2 Rett. 75x25 [cm]																
205	0.15	15.39	17.75			4861.8	10674.6	0.25	-746.0	-12119.8	0.27					
				SLE Rare		2163.9			0.0			0.0	31.7	807.1	194.1	
				SLE Freq.		2100.2			0.0			0.0	30.8	783.4	188.4	OK
				SLE Q.P.		2074.4			0.0			0.0	30.4	773.8	186.1	OK
Camp.	3.15	7.70	7.70	609.4	1584.5	0.0	5806.0	0.20	-1583.7	-5806.0	0.20					
				SLE Rare		0.0			-1218.2			25.3	0.0	105.1	872.8	
				SLE Freq.		0.0			-1218.2			25.3	0.0	105.1	872.8	OK

				SLE Q.P.		0.0			-1218.2			25.3	0.0	105.1	872.8	OK
206	6.15	6.21	6.21			3803.8	4839.8	0.19	-2416.0	-4839.8	0.19					
				SLE Rare		696.2			0.0			0.0	16.0	492.9	42.8	
				SLE Freq.		703.3			0.0			0.0	16.2	497.9	43.2	OK
				SLE Q.P.		703.2			0.0			0.0	16.2	497.9	43.2	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 202 203 Sez. 2 Rett. 75x25 [cm]
0.14	0.40	0.26	1.00	10454.3	8438.8	49258.5	29172.9	870.5	6450.0	8067.3	ø 8 4br. 5.0'
0.40	3.28	2.89	1.00	9802.4	9066.6	49258.5	11669.2	870.5	6450.0	3226.9	ø 8 4br. 12.5'
3.28	3.54	0.26	1.00	9629.0	11096.7	49258.5	29172.9	870.5	6450.0	8067.3	ø 8 4br. 5.0'
											Trave 203 204 Sez. 2 Rett. 75x25 [cm]
0.18	0.43	0.25	1.00	12103.5	11096.7	49258.5	29172.9	541.4	6450.0	8067.3	ø 8 4br. 5.0'
0.43	2.95	2.52	1.00	11468.4	8532.0	49258.5	11669.2	541.4	6450.0	3226.9	ø 8 4br. 12.5'
2.95	3.20	0.25	1.00	12005.2	11272.3	49258.5	29172.9	541.4	6450.0	8067.3	ø 8 4br. 5.0'
											Trave 204 205 Sez. 2 Rett. 75x25 [cm]
0.15	0.40	0.25	1.00	11779.7	11259.3	49258.5	29172.9	1071.8	6450.0	8067.3	ø 8 4br. 5.0'
0.40	3.21	2.81	1.00	11144.6	9326.4	49258.5	11669.2	1071.8	6450.0	3226.9	ø 8 4br. 12.5'
3.21	3.46	0.25	1.00	11779.7	11224.3	49258.5	29172.9	1071.8	6450.0	8067.3	ø 8 4br. 5.0'
											Trave 205 206 Sez. 2 Rett. 75x25 [cm]
0.15	0.40	0.25	1.00	4285.7	11272.3	49258.5	29172.9	431.1	6450.0	8067.3	ø 8 4br. 5.0'
0.40	5.81	5.41	1.00	4408.1	8532.0	49258.5	9724.3	431.1	6450.0	2689.1	ø 8 4br. 15.0'
5.81	6.05	0.25	1.00	4527.2	7941.2	49258.5	29172.9	431.1	6450.0	6129.4	ø 8 4br. 5.0'

Travata: ***Travata 204 Nodi 225 226 227 228 229***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
225	0.13	6.03	6.03			8963.8	10066.4	0.12	-2588.7	-10066.4	0.12					
				SLE Rare		4771.6			0.0			0.0	47.9	1921.5	450.7	
				SLE Freq.		3706.2			0.0			0.0	37.2	1492.5	350.1	OK

				SLE Q.P.		3371.5			0.0			0.0	33.8	1357.7	318.5	OK
Camp.	1.83	6.03	6.03	4510.8	3755.9	759.2	10066.4	0.12	-3755.3	-10066.4	0.12					
				SLE Rare		0.0			-2767.9			27.8	0.0	261.5	1114.6	
				SLE Freq.		0.0			-2367.0			23.8	0.0	223.6	953.2	OK
				SLE Q.P.		0.0			-2233.3			22.4	0.0	211.0	899.3	OK
226	3.53	6.91	12.06			4592.5	11460.8	0.11	-1266.6	-19627.6	0.17					
				SLE Rare		2095.5			0.0			0.0	17.5	507.9	161.6	
				SLE Freq.		1877.4			0.0			0.0	15.7	455.0	144.8	OK
				SLE Q.P.		1801.2			0.0			0.0	15.1	436.5	138.9	OK
Trave Sez. 1 Rett. 30x50 [cm]																
226	0.18	6.91	12.06			2860.4	11460.8	0.11	-14.8	-19627.6	0.17					
				SLE Rare		2028.5			0.0			0.0	17.0	490.9	156.4	
				SLE Freq.		1814.3			0.0			0.0	15.2	439.1	139.9	OK
				SLE Q.P.		1739.3			0.0			0.0	14.5	420.9	134.1	OK
Camp.	1.69	6.03	6.03	4510.8	3163.9	0.0	10066.4	0.12	-3162.1	-10066.4	0.12					
				SLE Rare		0.0			-2330.7			23.4	0.0	220.2	938.5	
				SLE Freq.		0.0			-1993.1			20.0	0.0	188.3	802.6	OK
				SLE Q.P.		0.0			-1880.5			18.9	0.0	177.6	757.3	OK
227	3.20	6.98	12.06			3715.1	11581.7	0.11	-260.2	-19629.6	0.17					
				SLE Rare		2551.7			0.0			0.0	21.3	614.4	196.6	
				SLE Freq.		2152.4			0.0			0.0	17.9	518.3	165.8	OK
				SLE Q.P.		2014.8			0.0			0.0	16.8	485.2	155.2	OK
Trave Sez. 1 Rett. 30x50 [cm]																
227	0.15	6.98	12.06			4317.3	11581.7	0.11	-503.7	-19629.6	0.17					
				SLE Rare		2764.6			0.0			0.0	23.0	671.3	213.0	
				SLE Freq.		2338.9			0.0			0.0	19.5	567.9	180.2	OK
				SLE Q.P.		2191.4			0.0			0.0	18.3	532.1	168.9	OK
Camp.	1.81	6.03	6.03	4510.8	3674.1	0.0	10066.4	0.12	-3674.1	-10066.4	0.12					
				SLE Rare		0.0			-2708.0			27.2	0.0	255.8	1090.5	

				SLE Freq.		0.0			-2315.8			23.2	0.0	218.8	932.6	OK
				SLE Q.P.		0.0			-2185.0			21.9	0.0	206.4	879.9	OK
228	3.46	6.88	9.79			4247.8	11414.5	0.12	-1277.8	-16046.6	0.15					
				SLE Rare		2030.2			0.0			0.0	17.8	495.5	167.6	
				SLE Freq.		1804.0			0.0			0.0	15.8	440.3	148.9	OK
				SLE Q.P.		1752.1			0.0			0.0	15.4	427.6	144.7	OK
Trave Sez. 1 Rett. 30x50 [cm]																
228	0.15	6.88	11.73			6481.3	11413.6	0.11	-2085.9	-19105.9	0.17					
				SLE Rare		2511.8			0.0			0.0	21.2	605.4	195.7	
				SLE Freq.		2241.7			0.0			0.0	18.9	540.3	174.6	OK
				SLE Q.P.		2179.8			0.0			0.0	18.4	525.3	169.8	OK
Camp.	3.05	6.03	6.03	767.5	1995.6	787.0	10066.4	0.12	-2828.8	-10066.4	0.12					
				SLE Rare		0.0			-1494.3			15.0	0.0	141.2	601.8	
				SLE Freq.		0.0			-1364.4			13.7	0.0	128.9	549.4	OK
				SLE Q.P.		0.0			-1312.4			13.2	0.0	124.0	528.5	OK
229	5.95	6.03	6.03			7685.2	10066.4	0.12	-6533.4	-10066.4	0.12					
				SLE Rare		643.8			0.0			0.0	6.5	259.2	60.8	
				SLE Freq.		610.8			0.0			0.0	6.1	246.0	57.7	OK
				SLE Q.P.		574.8			0.0			0.0	5.8	231.5	54.3	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 225 226 Sez. 1 Rett. 30x50 [cm]
0.13	0.63	0.50	1.00	14205.0	6073.0	43615.3	16144.2	481.0	5270.6	3296.1	ø 8 2br. 10.0'
0.63	3.03	2.40	1.00	12848.6	6073.0	43615.3	12915.4	481.0	5270.6	2636.9	ø 8 2br. 12.5'
3.03	3.53	0.50	1.00	11589.9	6379.5	43615.3	16144.2	481.0	5270.6	3296.1	ø 8 2br. 10.0'
											Trave 226 227 Sez. 1 Rett. 30x50 [cm]
0.18	3.20	3.02	1.00	15504.6	6073.0	43615.3	21525.6	379.1	5270.6	4394.8	ø 8 2br. 7.5'
											Trave 227 228 Sez. 1 Rett. 30x50 [cm]
0.15	3.46	3.31	1.00	14806.4	6073.0	43615.3	21525.6	916.1	5270.6	4394.8	ø 8 2br. 7.5'
											Trave 228 229 Sez. 1 Rett. 30x50 [cm]

0.15	0.63	0.48	1.00	5635.9	6426.1	43615.3	16144.2	274.0	5270.6	3296.1	ø 8 2br. 10.0'
0.63	5.19	4.56	1.00	6802.2	6073.0	43615.3	10762.8	274.0	5270.6	2197.4	ø 8 2br. 15.0'
5.19	5.66	0.48	1.00	7069.4	6073.0	43615.3	16144.2	274.0	5270.6	3296.1	ø 8 2br. 10.0'

Travata: ***Travata 207 Nodi 205 212 228***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
205	0.50	4.48	6.03			4882.1	7576.5	0.10	-6369.1	-10067.3	0.12					
				SLE Rare		0.0			-675.6			7.0	0.0	50.0	272.5	
				SLE Freq.		0.0			-751.0			7.8	0.0	55.6	302.9	OK
				SLE Q.P.		0.0			-749.2			7.8	0.0	55.5	302.2	OK
Camp.	1.30	6.03	6.03	3341.6	921.0	2088.7	10066.4	0.12	-1578.3	-10066.4	0.12					
				SLE Rare		750.2			-668.8			6.7	7.5	302.1	269.3	
				SLE Freq.		745.8			-581.5			5.8	7.5	300.3	234.2	OK
				SLE Q.P.		744.8			-546.6			5.5	7.5	299.9	220.1	OK
212	2.10	7.86	11.74			8204.4	12983.6	0.12	-56.7	-19139.3	0.16					
				SLE Rare		4343.4			0.0			0.0	34.9	1180.5	334.4	
				SLE Freq.		4139.9			0.0			0.0	33.3	1125.2	318.7	OK
				SLE Q.P.		4061.5			0.0			0.0	32.7	1103.9	312.7	OK
Trave Sez. 1 Rett. 30x50 [cm]																
212	0.50	7.86	12.05			11907.3	12983.5	0.12	0.0	-19629.1	0.16					
				SLE Rare		7865.9			0.0			0.0	62.9	2080.7	600.2	
				SLE Freq.		7200.2			0.0			0.0	57.5	1904.6	549.4	OK
				SLE Q.P.		6936.9			0.0			0.0	55.4	1834.9	529.3	OK
Camp.	2.97	6.03	6.03	3341.6	7344.2	968.7	10066.4	0.12	-8020.4	-10066.4	0.12					
				SLE Rare		0.0			-5431.3			54.5	0.0	513.1	2187.2	
				SLE Freq.		0.0			-4722.5			47.4	0.0	446.1	1901.7	OK
				SLE Q.P.		0.0			-4439.0			44.5	0.0	419.3	1787.6	OK
228	5.43	6.03	6.03			9527.5	10066.4	0.12	-6488.1	-10066.4	0.12					

	SLE Rare	2702.9			0.0			0.0	27.1	1088.5	255.3	
	SLE Freq.	2076.8			0.0			0.0	20.8	836.3	196.2	OK
	SLE Q.P.	1824.3			0.0			0.0	18.3	734.6	172.3	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 205 212 Sez. 1 Rett. 30x50 [cm]
0.75	1.17	0.42	1.00	16565.0	6073.0	43615.3	32288.4	1202.8	5270.6	5625.5	ø 8 2br. 5.0'
1.17	1.68	0.51	1.00	16777.9	6073.0	43615.3	21525.6	1202.8	5270.6	4394.8	ø 8 2br. 7.5'
1.68	2.10	0.42	1.00	17988.6	6403.1	43615.3	32288.4	1202.8	5270.6	6592.1	ø 8 2br. 5.0'
											Trave 212 228 Sez. 1 Rett. 30x50 [cm]
0.77	1.21	0.45	1.00	10781.1	6242.1	43615.3	16144.2	718.5	5270.6	3296.1	ø 8 2br. 10.0'
1.21	2.17	0.96	1.00	9637.5	6073.0	43615.3	12915.4	718.5	5270.6	2636.9	ø 8 2br. 12.5'
2.17	3.76	1.59	1.00	8666.7	6073.0	43615.3	10762.8	718.5	5270.6	2197.4	ø 8 2br. 15.0'
3.76	4.72	0.96	1.00	11120.3	6073.0	43615.3	12915.4	718.5	5270.6	2636.9	ø 8 2br. 12.5'
4.72	5.16	0.45	1.00	12263.9	6073.0	43615.3	16144.2	718.5	5270.6	3296.1	ø 8 2br. 10.0'

Travata: ***Travata 208 Nodi 206 218 229***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
206	0.50	4.48	6.03			5975.8	7576.5	0.10	-3220.4	-10067.3	0.12					
				SLE Rare		1660.2			0.0			0.0	18.6	662.4	160.7	
				SLE Freq.		1511.9			0.0			0.0	17.0	603.2	146.4	OK
				SLE Q.P.		1453.3			0.0			0.0	16.3	579.9	140.7	OK
Camp.	2.20	6.03	6.03	3341.6	3176.6	0.0	10066.4	0.12	-3157.8	-10066.4	0.12					
				SLE Rare		0.0			-2335.3			23.4	0.0	220.6	940.4	
				SLE Freq.		0.0			-2030.6			20.4	0.0	191.8	817.7	OK
				SLE Q.P.		0.0			-1908.7			19.2	0.0	180.3	768.6	OK
218	3.90	7.90	11.83			7087.0	13049.6	0.12	-1899.1	-19284.3	0.16					
				SLE Rare		3423.6			0.0			0.0	27.4	925.7	262.7	
				SLE Freq.		2922.6			0.0			0.0	23.4	790.2	224.3	OK

				SLE Q.P.		2721.7			0.0			0.0	21.8	735.9	208.9	OK
Trave Sez. 1 Rett. 30x50 [cm]																
218	0.50	7.90	9.79			6084.6	13050.0	0.12	-613.9	-16053.3	0.14					
				SLE Rare		3604.7			0.0			0.0	30.2	958.0	293.5	
				SLE Freq.		3177.2			0.0			0.0	26.6	844.4	258.7	OK
				SLE Q.P.		3007.4			0.0			0.0	25.2	799.3	244.9	OK
Camp.	2.16	6.03	6.03	3341.6	3562.4	0.0	10066.4	0.12	-3748.3	-10066.4	0.12					
				SLE Rare		0.0			-2770.4			27.8	0.0	261.7	1115.6	
				SLE Freq.		0.0			-2403.7			24.1	0.0	227.1	968.0	OK
				SLE Q.P.		0.0			-2256.9			22.6	0.0	213.2	908.8	OK
229	3.83	6.03	6.03			2800.3	10066.4	0.12	-3116.6	-10066.4	0.12					
				SLE Rare		44.6			-101.2			1.0	0.4	18.0	40.7	
				SLE Freq.		12.0			-113.5			1.1	0.1	10.7	45.7	OK
				SLE Q.P.		0.0			-111.8			1.1	0.0	10.6	45.0	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
Trave 206 218 Sez. 1 Rett. 30x50 [cm]											
0.78	1.24	0.46	1.00	12258.7	6073.0	43615.3	16144.2	648.0	5270.6	3296.1	ø 8 2br. 10.0'
1.24	3.44	2.21	1.00	11149.2	6073.0	43615.3	12915.4	648.0	5270.6	2636.9	ø 8 2br. 12.5'
3.44	3.90	0.46	1.00	11455.3	6430.6	43615.3	16144.2	648.0	5270.6	3296.1	ø 8 2br. 10.0'
Trave 218 229 Sez. 1 Rett. 30x50 [cm]											
0.77	1.21	0.45	1.00	11439.0	6242.1	43615.3	16144.2	646.9	5270.6	3296.1	ø 8 2br. 10.0'
1.21	3.29	2.08	1.00	11289.0	6073.0	43615.3	12915.4	646.9	5270.6	2636.9	ø 8 2br. 12.5'
3.29	3.74	0.45	1.00	12431.1	6073.0	43615.3	16144.2	646.9	5270.6	3296.1	ø 8 2br. 10.0'

Travata: ***Travata 46 Nodi 202 217 225***

Nodo	x [m]	A_{fe} [cm²]	A_{fi} [cm²]	q_T [kg/m]	M_{rif} [kgm]	M_{de} [kgm]	M_{re} [kgm]	x/d	M_{di} [kgm]	M_{ri} [kgm]	x/d	σ_{be} [kg/cm²]	σ_{bi} [kg/cm²]	σ_{fe} [kg/cm²]	σ_{fi} [kg/cm²]	wmm
Trave Sez. 1 Rett. 30x50 [cm]																
202	0.50	8.04	7.57			12747.6	13279.1	0.13	-9249.3	-12531.1	0.12					
				SLE Rare		1807.5			0.0			0.0	15.8	550.3	158.8	

				SLE Freq.		1770.3			0.0			0.0	15.5	539.0	155.5	OK
				SLE Q.P.		1747.3			0.0			0.0	15.3	532.0	153.5	OK
Camp.	2.06	6.03	6.03	487.5	456.3	2719.6	10066.4	0.12	-2329.8	-10066.4	0.12					
				SLE Rare		38.2			-351.0			3.5	0.4	33.2	141.4	
				SLE Freq.		48.8			-351.0			3.5	0.5	33.2	141.4	OK
				SLE Q.P.		47.8			-351.0			3.5	0.5	33.2	141.4	OK
217	3.62	8.09	12.06			7776.8	13357.0	0.12	-8826.9	-19652.0	0.16					
				SLE Rare		0.0			-623.6			4.7	0.0	43.5	128.5	
				SLE Freq.		0.0			-557.6			4.2	0.0	38.9	114.9	OK
				SLE Q.P.		0.0			-521.5			3.9	0.0	36.4	107.4	OK
Trave Sez. 1 Rett. 30x50 [cm]																
217	0.25	8.09	12.06			11067.4	13357.0	0.12	-5879.2	-19652.0	0.16					
				SLE Rare		2540.6			0.0			0.0	20.1	665.0	193.3	
				SLE Freq.		2610.9			0.0			0.0	20.6	683.4	198.6	OK
				SLE Q.P.		2599.8			0.0			0.0	20.6	680.5	197.8	OK
Camp.	1.96	6.03	6.03	493.8	534.1	2201.7	10066.4	0.12	-2300.7	-10066.4	0.12					
				SLE Rare		165.1			-410.6			4.1	1.7	66.5	165.4	
				SLE Freq.		146.6			-409.9			4.1	1.5	59.0	165.0	OK
				SLE Q.P.		140.8			-409.5			4.1	1.4	56.7	164.9	OK
225	3.66	6.03	10.05			9835.5	10063.9	0.11	-11778.1	-16456.2	0.15					
				SLE Rare		0.0			-881.0			7.4	0.0	78.0	217.0	
				SLE Freq.		0.0			-986.5			8.3	0.0	87.3	243.0	OK
				SLE Q.P.		0.0			-979.4			8.2	0.0	86.7	241.2	OK

Da [m]	A [m]	Dx [m]	cotg (θ)	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	V_{Rcd} [kg]	V_{Rd} [kg]	T_{Ed} [kgm]	T_{Rcd} [kgm]	T_{Rsd} [kgm]	Staffe
											Trave 202 217 Sez. 1 Rett. 30x50 [cm]
0.77	1.22	0.45	1.00	12261.0	6549.3	43615.3	16144.2	1485.4	5270.6	3296.1	ø 8 2br. 10.0'
1.22	3.13	1.91	1.00	12052.4	6073.0	43615.3	12915.4	1485.4	5270.6	2636.9	ø 8 2br. 12.5'
3.13	3.58	0.45	1.00	11168.2	6465.1	43615.3	16144.2	1485.4	5270.6	3296.1	ø 8 2br. 10.0'
											Trave 217 225 Sez. 1 Rett. 30x50 [cm]

0.30	0.75	0.45	1.00	10328.4	6434.2	43615.3	16144.2	1434.3	5270.6	3296.1	ø 8 2br. 10.0'
0.75	2.93	2.19	1.00	10120.2	6073.0	43615.3	12915.4	1434.3	5270.6	2636.9	ø 8 2br. 12.5'
2.93	3.39	0.45	1.00	10298.4	7200.3	43615.3	16144.2	1434.3	5270.6	3296.1	ø 8 2br. 10.0'

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Verifiche setti in c.a.

Modalità di verifica

Le pareti in c.a. vengono verificate come setti/diaframmi o nuclei.

La verifica dei setti/diaframmi viene condotta a pressoflessione retta e a taglio. Viene calcolato lo sforzo normale medio agente sul setto e il momento ad esso associato. Quando previsto, sono introdotti ferri verticali aggiuntivi da disporsi sulle estremità del setto stesso.

La verifica dei nuclei viene condotta a pressoflessione deviata sulla sezione complessiva e a taglio sulle singole pareti costituenti il nucleo.

Sezioni Impiegate:

Sez. Num.	Info	Dimensioni	Criterio	Calcestruzzo	γ_M	F.C.	f_{ck} [kg/cm²]	f_{cd} [kg/cm²]	σ_{RARE} [kg/cm²]	σ_{FREQ} [kg/cm²]	σ_{QP} [kg/cm²]	Acciaio
1	Muro fondazione	B 130 H 50 s 30 [cm] Terreno numero 1	Verset	C25/30	1.50	1.00	250.0	141.7	150.0	250.0	112.5	B 450 C

γ_M	F.C.	f_{yk} [kg/cm²]	f_{yd} [kg/cm²]	σ_{yRARE} [kg/cm²]	σ_{yFREQ} [kg/cm²]	σ_{yQP} [kg/cm²]	Coprif erro [cm]	cotg θ
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	4.00	1.00

Taglio di progetto pari al taglio di calcolo
Verifica a taglio-compressione del calcestruzzo dell'anima nelle zone dissipative: fattore riduttivo 0.40
V_{Rdc}=0.90 lw bw α_cv f_{cd} (cotg(α)+cotg(θ))/(1+cotg(θ)²)
Il rapporto di taglio α_s=M_{Ed}/(V_{Ed} lw) è limitato a 0.5 (α_s≥0.5).

Verifiche Setti:

Setto : 6 106 118 18 / Sezione 1

B = 390.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	18	-63126.5	0.0	-49890.2	0.06
Sommità	13	-24500.0	0.0	35637.7	0.03

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-52246.5	0.0	-10928.7	-5.5
$\sigma_{Cls,Med}$	23	-52246.5	0.0	-10928.7	-4.2
$\sigma_{s,t}$	20	-55179.2	0.0	-11149.4	-46.8
$\sigma_{s,c}$	19	-57378.1	0.0	-11550.8	-88.9
Sommita					

$\sigma_{Cls,Max}$	23	-34940.2	0.0	5963.0	-3.5
$\sigma_{Cls,Med}$	23	-34940.2	0.0	5963.0	-2.8
$\sigma_{s,t}$	20	-37872.9	0.0	5909.3	-35.1
$\sigma_{s,c}$	19	-40071.8	0.0	5759.0	-58.1

Verifiche a Taglio

			compressione					taglio - trazione								
Parete	**B [m]**	**H [m]**	**Comb**	**ε**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**S/R**	**Comb**	**ε**	**V_{Ed} [kg]**	**α_s**	**V_{Rcd} [kg]**	**V_{Rsd} [kg]**	**V_{Rd} [kg]**	**ρ_h ρ_v+ ρ_N**	**S/R**
6 118	3.90	3.75	18	1.00	19339.5	373025.2	0.05	18	1.00	19339.5	2.00	0.0	0.0	86297.2		0.22

scorrimento									
Comb	**ε**	**V_{Ed} [kg]**	**V_{dd} [kg]**	**V_{id} [kg]**	**V_{fd} [kg]**	**$V_{Rd,s}$ [kg]**	**V_{id} V_{Ed}/2**	**S/R**	**S/R**
									0.22

Setto : 18 118 129 29 / Sezione 1

B = 413.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	**Comb.**	**N_{Ed} [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**Sd/Sr**
Base	18	-32912.7	0.0	-90156.3	0.10
Sommità	18	-14585.8	0.0	-66271.7	0.10

S.L.E.	**Combinazione**	**N [kg]**	**M_{12} [kgm]**	**M_{13} [kgm]**	**σ [kg/cm²]**
Base					
$\sigma_{Cls,Max}$	23	-36703.8	0.0	-36053.1	-6.8
$\sigma_{Cls,Med}$	23	-36703.8	0.0	-36053.1	-3.4
$\sigma_{s,t}$	20	-39198.5	0.0	-37509.7	19.5
$\sigma_{s,c}$	19	-40857.9	0.0	-38514.8	-108.2
Sommita					
$\sigma_{Cls,Max}$	23	-18376.9	0.0	-20929.1	-3.9

$\sigma_{Cls,Med}$	23	-18376.9	0.0	-20929.1	-1.9
$\sigma_{s,t}$	22	-18428.2	0.0	-21001.1	21.1
$\sigma_{s,c}$	19	-22531.1	0.0	-21110.6	-59.4

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v+ ρ_N	S/R
18 129	4.13	3.75	18	1.00	41686.7	395024.1	0.11	18	1.00	41686.7	2.00	0.0	0.0	91386.5		0.46

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed}/2	S/R	S/R
									0.46

Setto : 19 119 120 20 / Sezione 1

B = 368.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	17	-19310.7	0.0	15079.1	0.02
Sommità	11	2156.2	0.0	3086.1	0.02

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-18029.3	0.0	6572.2	-2.4
$\sigma_{Cls,Med}$	23	-18029.3	0.0	6572.2	-1.5
$\sigma_{s,t}$	20	-18671.4	0.0	6216.7	-11.6
$\sigma_{s,c}$	19	-19145.4	0.0	5941.2	-35.7
Sommita					
$\sigma_{Cls,Max}$	19	-2815.4	0.0	-4816.3	-1.2
$\sigma_{Cls,Med}$	19	-2815.4	0.0	-4816.3	-0.6
$\sigma_{s,t}$	19	-2815.4	0.0	-4816.3	21.5

$\sigma_{s,c}$	19	-2815.4	0.0	-4816.3	-17.3

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v+ ρ_N	S/R
19 120	3.68	3.75	12	1.00	4344.0	351982.8	0.01	12	1.00	4344.0	2.00	0.0	0.0	81429.2		0.05

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed}/2	S/R	S/R
									0.05

Setto : 20 120 121 21 / Sezione 1

B = 452.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	16	-28256.4	0.0	-35874.3	0.03
Sommità	11	-3581.2	0.0	26493.4	0.04

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-25825.5	0.0	-8878.7	-2.6
$\sigma_{Cls,Med}$	23	-25825.5	0.0	-8878.7	-1.8
$\sigma_{s,t}$	23	-25825.5	0.0	-8878.7	-15.2
$\sigma_{s,c}$	19	-28661.2	0.0	-13994.3	-48.2
Sommita					
$\sigma_{Cls,Max}$	19	-8603.7	0.0	-3158.2	-0.9
$\sigma_{Cls,Med}$	19	-8603.7	0.0	-3158.2	-0.6
$\sigma_{s,t}$	19	-8603.7	0.0	-3158.2	-4.8
$\sigma_{s,c}$	19	-8603.7	0.0	-3158.2	-13.1

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v+ ρ_N	S/R
20 121	4.52	3.75	16	1.00	15814.7	432326.6	0.04	16	1.00	15814.7	2.00	0.0	0.0	100016.3		0.16

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed} /2	S/R	S/R
									0.16

Setto : 21 121 122 22 / Sezione 1

B = 408.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	11	-23303.6	0.0	49395.3	0.05
Sommità	11	-5198.6	0.0	40905.8	0.08

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-24141.1	0.0	14515.2	-3.4
$\sigma_{Cls,Med}$	23	-24141.1	0.0	14515.2	-1.8
$\sigma_{s,t}$	20	-25827.4	0.0	13500.6	-8.1
$\sigma_{s,c}$	19	-27041.6	0.0	12958.2	-51.6
Sommita					
$\sigma_{Cls,Max}$	23	-6036.1	0.0	7241.1	-1.4
$\sigma_{Cls,Med}$	23	-6036.1	0.0	7241.1	-0.7
$\sigma_{s,t}$	23	-6036.1	0.0	7241.1	9.1
$\sigma_{s,c}$	19	-8936.6	0.0	5258.7	-18.6

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_b $\rho_v+\rho_N$	S/R
21 122	4.08	3.75	11	1.00	24052.1	390241.8	0.06	11	1.00	24052.1	2.00	0.0	0.0	902802		0.27

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed} /2	S/R	S/R
									0.27

Setto : 22 122 123 23 / Sezione 1

B = 548.00 H = 375.00 [cm]

Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	16	-36434.1	0.0	-55859.5	0.03
Sommità	16	-12116.6	0.0	-57783.8	0.05

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-35325.0	0.0	117.5	-2.0
$\sigma_{Cls,Med}$	23	-35325.0	0.0	117.5	-2.0
$\sigma_{s,t}$	20	-37641.3	0.0	-1770.6	-30.6
$\sigma_{s,c}$	19	-39273.0	0.0	-2139.7	-35.5
Sommita					
$\sigma_{Cls,Max}$	19	-14955.5	0.0	-7070.1	-1.3
$\sigma_{Cls,Med}$	19	-14955.5	0.0	-7070.1	-0.9
$\sigma_{s,t}$	20	-13323.8	0.0	-5782.1	-6.2
$\sigma_{s,c}$	19	-14955.5	0.0	-7070.1	-19.1

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v+ ρ_N	S/R
22 123	5.48	3.75	16	1.00	30286.5	524148.3	0.06	16	1.00	30286.5	2.00	0.0	0.0	121258.7		0.25

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed} /2	S/R	S/R
									0.25

Setto : 23 123 124 24 / Sezione 1

B = 516.00 H = 375.00 [cm]

Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	16	-36192.7	0.0	-75457.4	0.04
Sommità	16	-13295.2	0.0	-68432.2	0.06

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-35931.3	0.0	-15739.6	-3.2
$\sigma_{Cls,Med}$	23	-35931.3	0.0	-15739.6	-2.2
$\sigma_{s,t}$	20	-38825.8	0.0	-17606.1	-17.6
$\sigma_{s,c}$	19	-40594.3	0.0	-18024.7	-54.6
Sommita					
$\sigma_{Cls,Max}$	23	-13033.8	0.0	-10994.4	-1.5
$\sigma_{Cls,Med}$	19	-17696.8	0.0	-11827.8	-1.1
$\sigma_{s,t}$	20	-15928.3	0.0	-12428.8	-2.0
$\sigma_{s,c}$	19	-17696.8	0.0	-11827.8	-27.8

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v+ ρ_N	S/R
23 124	5.16	3.75	16	1.00	38365.3	493541.1	0.08	16	1.00	38365.3	2.00	0.0	0.0	114177.9		0.34

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed} /2	S/R	S/R
									0.34

Setto : 24 124 125 25 / Sezione 1

B = 640.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	16	-40829.5	0.0	-99333.5	0.04
Sommità	16	-12429.5	0.0	-110844.1	0.09

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-41372.1	0.0	-29070.6	-3.3
$\sigma_{Cls,Med}$	23	-41372.1	0.0	-29070.6	-2.0
$\sigma_{s,t}$	20	-44416.9	0.0	-29033.7	-13.5
$\sigma_{s,c}$	19	-46071.9	0.0	-28552.5	-52.7
Sommita					
$\sigma_{Cls,Max}$	23	-12972.1	0.0	-41593.5	-3.7
$\sigma_{Cls,Med}$	23	-12972.1	0.0	-41593.5	-1.8
$\sigma_{s,t}$	23	-12972.1	0.0	-41593.5	81.1
$\sigma_{s,c}$	20	-16016.9	0.0	-42897.9	-53.1

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v+ ρ_N	S/R
24 125	6.40	3.75	16	1.00	55947.4	612143.9	0.09	16	1.00	55947.4	2.00	0.0	0.0	141616.0		0.40

scorrimento								
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed} /2	S/R	S/R
									0.40

Setto : 25 125 126 26 / Sezione 1

B = 365.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	16	-30047.1	0.0	-55063.4	0.06
Sommità	16	-13850.2	0.0	-58748.3	0.11

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-33397.7	0.0	-18178.5	-5.3
$\sigma_{Cls,Med}$	23	-33397.7	0.0	-18178.5	-2.8
$\sigma_{s,t}$	20	-36124.2	0.0	-17663.1	-11.4
$\sigma_{s,c}$	19	-37632.6	0.0	-17647.0	-82.6
Sommita					
$\sigma_{Cls,Max}$	23	-17200.9	0.0	-21604.8	-5.1
$\sigma_{Cls,Med}$	23	-17200.9	0.0	-21604.8	-2.5
$\sigma_{s,t}$	23	-17200.9	0.0	-21604.8	50.7
$\sigma_{s,c}$	19	-21435.8	0.0	-21343.2	-73.5

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v+ ρ_N	S/R
25 126	3.65	3.75	16	1.00	30338.9	349113.5	0.09	16	1.00	30338.9	2.00	0.0	0.0	80765.4		0.38

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed} /2	S/R	S/R
									0.38

Setto : 26 126 127 27 / Sezione 1

B = 335.00 H = 375.00 [cm]

Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	16	-30788.2	0.0	-43299.8	0.06
Sommità	16	-15922.6	0.0	-42981.4	0.09

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-33767.7	0.0	-12515.8	-5.2
$\sigma_{Cls,Med}$	23	-33767.7	0.0	-12515.8	-3.2
$\sigma_{s,t}$	20	-36577.5	0.0	-11179.3	-24.8
$\sigma_{s,c}$	19	-38278.4	0.0	-10789.8	-79.6
Sommita					
$\sigma_{Cls,Max}$	23	-18902.1	0.0	-12474.0	-3.8
$\sigma_{Cls,Med}$	23	-18902.1	0.0	-12474.0	-1.9
$\sigma_{s,t}$	20	-21711.9	0.0	-11279.7	-3.7
$\sigma_{s,c}$	19	-23412.8	0.0	-10911.8	-58.9

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione									scorrimento								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_h ρ_v + ρ_N	S/R	Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed}/2	S/R	S/R
26 127	3.35	3.75	16	1.00	23008.0	320418.9	0.07	16	1.00	23008.0	2.00	0.0	0.0	74127.1		0.31										0.31

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed}/2	S/R	S/R
									0.31

Setto : 27 127 128 28 / Sezione 1

B = 361.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	15	-34893.4	0.0	-34215.3	0.04
Sommità	15	-18874.0	0.0	-36588.0	0.05

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-36287.2	0.0	-3228.6	-3.6
$\sigma_{Cls,Med}$	23	-36287.2	0.0	-3228.6	-3.1
$\sigma_{s,t}$	19	-41183.8	0.0	1333.0	-50.4
$\sigma_{s,c}$	19	-41183.8	0.0	1333.0	-55.7
Sommita					
$\sigma_{Cls,Max}$	23	-20267.8	0.0	-4754.1	-2.4
$\sigma_{Cls,Med}$	23	-20267.8	0.0	-4754.1	-1.7
$\sigma_{s,t}$	20	-23359.0	0.0	-1991.3	-26.1
$\sigma_{s,c}$	20	-23359.0	0.0	-1991.3	-34.1

Verifiche a Taglio

Parete	B [m]	H [m]	compressione					taglio - trazione								
			Comb	ε	V_{Ed} [kg]	$V_{Rd,c}$ [kg]	S/R	Comb	ε	V_{Ed} [kg]	α_s	V_{Rcd} [kg]	V_{Rsd} [kg]	V_{Rd} [kg]	ρ_b $\rho_v+\rho_N$	S/R
27 128	3.61	3.75	15	1.00	18853.7	345287.5	0.05	15	1.00	18853.7	2.00	0.0	0.0	798803.3		0.24

scorrimento									
Comb	ε	V_{Ed} [kg]	V_{dd} [kg]	V_{id} [kg]	V_{fd} [kg]	$V_{Rd,s}$ [kg]	V_{id} V_{Ed}/2	S/R	S/R
									0.24

Setto : 28 128 129 29 / Sezione 1

B = 645.00 H = 375.00 [cm]
Armature su ogni faccia: Verticali : ø 10 25' [cm], Orizzontali : ø 10 25' [cm], Integrative Sx: ø 18 30' [cm], Dx: ø 18 30' [cm]

Sezione	Comb.	N_{Ed} [kg]	M_{12} [kgm]	M_{13} [kgm]	Sd/Sr
Base	12	-50564.5	0.0	59924.0	0.03
Sommità	16	-13148.6	0.0	94706.8	0.07

S.L.E.	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Base					
$\sigma_{Cls,Max}$	23	-48023.5	0.0	1093.1	-2.4
$\sigma_{Cls,Med}$	23	-48023.5	0.0	1093.1	-2.3
$\sigma_{s,t}$	20	-50989.1	0.0	3715.5	-34.8
$\sigma_{s,c}$	19	-52744.1	0.0	4711.0	-41.6
Sommita					
$\sigma_{Cls,Max}$	23	-19401.7	0.0	29013.9	-2.3
$\sigma_{Cls,Med}$	23	-19401.7	0.0	29013.9	-1.1
$\sigma_{s,t}$	19	-24122.2	0.0	39068.3	12.5
$\sigma_{s,c}$	19	-24122.2	0.0	39068.3	-45.0

Verifiche a Taglio

			compressione					taglio - trazione								
Parete	**B [m]**	**H [m]**	**Comb**	**ε**	**V_{Ed} [kg]**	**$V_{Rd,c}$ [kg]**	**S/R**	**Comb**	**ε**	**V_{Ed} [kg]**	**α_s**	**V_{Rcd} [kg]**	**V_{Rsd} [kg]**	**V_{Rd} [kg]**	**ρ_h ρ_v+ ρ_N**	**S/R**
28129	6.45	3.75	16	1.00	41160.5	616926.4	0.07	16	1.00	41160.5	2.00	0.0	0.0	142722.4		0.29

scorrimento									
Comb	**ε**	**V_{Ed} [kg]**	**V_{dd} [kg]**	**V_{id} [kg]**	**V_{fd} [kg]**	**$V_{Rd,s}$ [kg]**	**V_{id} V_{Ed} /2**	**S/R**	**S/R**
									0.29

Verifiche pilastri

Modalità di verifica

I pilastri vengono verificati (a discrezione dell'utente) secondo una delle seguenti modalità:

- Presso-tenso flessione deviata.
- Presso-tenso flessione retta. In tale caso viene svolta prima la verifica a presso-tenso flessione considerando come azioni agenti lo sforzo normale ed il momento M_x agente sulla sezione poi, disgiuntamente, considerando come azioni agenti lo sforzo normale e l'altro momento M_y. A discrezione dell'operatore tali momenti (a favore della sicurezza) possono essere incrementati di un fattore di amplificazione anch'esso a discrezione dell'utente.

Le verifiche vengono effettuate nella sezione di sommità e in quella di base in tutte le combinazioni di carico.

Nelle stampe si riportano (per le due sezioni di verifica succitate) le sollecitazioni relative alla combinazione di carico critica. Le sollecitazioni di verifica alle estremità sono valutate ad una ascissa di spunto definita dall'utente.

Sezioni Impiegate:

Sez. Num.	Info	Dimensioni	Criterio	Calcestruzzo	γ_M	F.C.	f_{ck} [kg/cm²]	f_{cd} [kg/cm²]	σ_{RARE} [kg/cm²]	σ_{FREQ} [kg/cm²]	σ_{QP} [kg/cm²]	Acciaio	cotg θ
1	Rett.	B 30 H 50 [cm]	Verpil	C28/35	1.50	1.00	280.0	158.7	168.0	280.0	126.0	B 450 C	1.00
2	Rett.	B 50 H 30 [cm]	Verpil	C28/35	1.50	1.00	280.0	158.7	168.0	280.0	126.0	B 450 C	1.00
3	Rett.	B 30 H 30 [cm]	Verpil	C28/35	1.50	1.00	280.0	158.7	168.0	280.0	126.0	B 450 C	1.00

γ_M	F.C.	f_{yk} [kg/cm²]	f_{yd} [kg/cm²]	σ_{yRARE} [kg/cm²]	σ_{yFREQ} [kg/cm²]	σ_{yQP} [kg/cm²]	Copr. [cm]	Verifica	cotg θ
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	3.00	Deviata	1.00
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	3.00	Deviata	1.00
1.15	1.00	4500.0	3913.0	3600.0	4500.0	4500.0	3.00	Deviata	1.00

Verifiche Pilastri:

L'area complessiva dei bracci di staffa A_{st} è l'area totale delle staffe in entrambe le direzioni.

Le staffe disposte rispattano il rapporto meccanico volumetrico della staffatura di confinamento all'interno della zone critiche. La quantità di staffe per unità di lunghezza per duttilità viene disposta nelle sole zone critiche.

L'azione tagliante plastica è calcolata in accordo con EC8 5.4.2.3. Formula 5.9 Ai fini della valutazione dei momenti resistenti del pilastro nei due piani si assume lo sforzo assiale N pari al valore medio dello sforzo assiale nelle combinazioni di carico sismiche. I momenti resistenti sono valutati indipendentemente nei due piani.

Fattore di sovraresistenza $\gamma_{R,d\ (Nuovi)}$=1.10 $\gamma_{R,d\ (Esistenti)}$=0.00

Pilastro: 1/101 / L 3.05[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >

Staffe: ø 8 2br.x4br./10.0 x 305.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
1	15	-16994.5	18778.4	-7887.1	10.27	6.59	0.96
101	15	-15588.3	-18778.4	7887.1	4.82	97.61	0.97

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.30	1.00	15768.2	16144.2	0.98	1.00	5914.6	18126.8	0.33	ø 8 2br.x4br./10.0	0.222

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
1	Ft. 19	-23523.5	6871.0	-3176.1	1335.4
	$\sigma_{s,c}$19	-23523.5	6871.0	-3176.1	-1208.7
	$\sigma_{cls,Max}$19	-23523.5	6871.0	-3176.1	-107.5
	$\sigma_{cls,Med}$19	-23523.5	6871.0	-3176.1	-36.3
101	Ft. 19	-22117.3	-8586.9	1872.8	1461.9
	$\sigma_{s,c}$19	-22117.3	-8586.9	1872.8	-1184.5
	$\sigma_{cls,Max}$19	-22117.3	-8586.9	1872.8	-103.8
	$\sigma_{cls,Med}$19	-22117.3	-8586.9	1872.8	-39.5
Combinazioni Frequenti					
1	Ft. 21	-19956.9	6789.3	-2850.1	1359.1
	$\sigma_{s,c}$21	-19956.9	6789.3	-2850.1	-1143.6
	$\sigma_{cls,Max}$21	-19956.9	6789.3	-2850.1	-102.2
	$\sigma_{cls,Med}$21	-19956.9	6789.3	-2850.1	-34.8
101	Ft. 21	-18550.7	-7876.5	1633.9	1381.3
	$\sigma_{s,c}$21	-18550.7	-7876.5	1633.9	-1066.6
	$\sigma_{cls,Max}$21	-18550.7	-7876.5	1633.9	-93.9
	$\sigma_{cls,Med}$21	-18550.7	-7876.5	1633.9	-35.9
Combinazioni Quasi Permanenti					
1	Ft. 23	-18630.0	6736.7	-2728.5	1364.5
	$\sigma_{s,c}$23	-18630.0	6736.7	-2728.5	-1116.8
	$\sigma_{cls,Max}$23	-18630.0	6736.7	-2728.5	-100.1
	$\sigma_{cls,Med}$23	-18630.0	6736.7	-2728.5	-34.1
101	Ft. 23	-17223.8	-7576.5	1548.0	1344.5
	$\sigma_{s,c}$23	-17223.8	-7576.5	1548.0	-1019.7
	$\sigma_{cls,Max}$23	-17223.8	-7576.5	1548.0	-89.9
	$\sigma_{cls,Med}$23	-17223.8	-7576.5	1548.0	-34.4

Pilastro: 2/102 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./10.0 x 300.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
2	14	-23285.6	-16255.7	7336.6	7.31	17.15	0.84
102	14	-21879.4	-16255.7	7336.6	13.23	18.73	0.84

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.25	1.00	13903.8	16144.2	0.86	1.00	4362.7	18126.8	0.24	ø 8 2br.x4br./10.0	0.222

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
2	Ft. 20	-34881.8	4407.0	-1182.9	228.9
	$\sigma_{s,c}$19	-37165.7	4471.8	-1175.6	-740.2
	$\sigma_{cls,Max}$19	-37165.7	4471.8	-1175.6	-58.6
	$\sigma_{cls,Med}$19	-37165.7	4471.8	-1175.6	-23.6
102	Ft. 20	-33475.5	-5651.3	1390.5	476.3
	$\sigma_{s,c}$19	-35759.4	-5878.2	1398.6	-899.0
	$\sigma_{cls,Max}$19	-35759.4	-5878.2	1398.6	-73.1
	$\sigma_{cls,Med}$19	-35759.4	-5878.2	1398.6	-28.9
	Combinazioni Frequenti				
2	Ft. 22	-31544.7	4389.3	-1174.9	278.9
	$\sigma_{s,c}$21	-33067.3	4432.5	-1170.0	-716.7
	$\sigma_{cls,Max}$21	-33067.3	4432.5	-1170.0	-57.3
	$\sigma_{cls,Med}$21	-33067.3	4432.5	-1170.0	-22.8
102	Ft. 22	-30138.5	-5400.2	1373.8	503.8
	$\sigma_{s,c}$21	-31661.1	-5551.4	1379.3	-849.4
	$\sigma_{cls,Max}$21	-31661.1	-5551.4	1379.3	-69.7
	$\sigma_{cls,Med}$21	-31661.1	-5551.4	1379.3	-27.2
	Combinazioni Quasi Permanenti				
2	Ft. 23	-31479.9	4404.6	-1171.0	281.6
	$\sigma_{s,c}$23	-31479.9	4404.6	-1171.0	-707.4
	$\sigma_{cls,Max}$23	-31479.9	4404.6	-1171.0	-56.8
	$\sigma_{cls,Med}$23	-31479.9	4404.6	-1171.0	-22.4
102	Ft. 23	-30073.6	-5411.6	1372.5	507.0
	$\sigma_{s,c}$23	-30073.6	-5411.6	1372.5	-829.1
	$\sigma_{cls,Max}$23	-30073.6	-5411.6	1372.5	-68.2
	$\sigma_{cls,Med}$23	-30073.6	-5411.6	1372.5	-26.5

Pilastro: 102/202 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./15.0 x 195.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
102	16	-13076.7	11684.9	7919.2	5.67	2.87	0.74
202	17	-11897.3	-13248.5	4265.8	1.00	1.00	0.62

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.50	1.00	8593.1	12915.4	0.67	1.00	4741.9	14501.5	0.33	ø 8 2br.x4br./12.5	0.177
0.50	2.45	1.00	8593.1	10762.8	0.80	1.00	4741.9	12084.6	0.39	ø 8 2br.x4br./15.0	0.148
2.45	2.95	1.00	8593.1	12915.4	0.67	1.00	4741.9	14501.5	0.33	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
102	Ft. 19	-12088.1	1639.1	-520.4	112.4
	$\sigma_{s,c}$19	-12088.1	1639.1	-520.4	-275.6
	$\sigma_{cls,Max}$19	-12088.1	1639.1	-520.4	-22.3
	$\sigma_{cls,Med}$19	-12088.1	1639.1	-520.4	-8.6
202	Ft. 19	-10794.4	-2023.9	1020.0	301.9
	$\sigma_{s,c}$19	-10794.4	-2023.9	1020.0	-378.3
	$\sigma_{cls,Max}$19	-10794.4	-2023.9	1020.0	-32.5
	$\sigma_{cls,Med}$19	-10794.4	-2023.9	1020.0	-11.1
Combinazioni Frequenti					
102	Ft. 21	-10669.7	1303.5	-348.2	62.2
	$\sigma_{s,c}$21	-10669.7	1303.5	-348.2	-215.6
	$\sigma_{cls,Max}$21	-10669.7	1303.5	-348.2	-17.1
	$\sigma_{cls,Med}$21	-10669.7	1303.5	-348.2	-6.9
202	Ft. 21	-9375.9	-1841.8	622.6	222.0
	$\sigma_{s,c}$21	-9375.9	-1841.8	622.6	-300.6
	$\sigma_{cls,Max}$21	-9375.9	-1841.8	622.6	-25.3
	$\sigma_{cls,Med}$21	-9375.9	-1841.8	622.6	-9.2
Combinazioni Quasi Permanenti					
102	Ft. 23	-10155.9	1164.8	-294.3	44.7
	$\sigma_{s,c}$23	-10155.9	1164.8	-294.3	-193.8
	$\sigma_{cls,Max}$23	-10155.9	1164.8	-294.3	-15.2
	$\sigma_{cls,Med}$23	-10155.9	1164.8	-294.3	-6.2
202	Ft. 23	-8862.1	-1763.5	497.0	196.6
	$\sigma_{s,c}$23	-8862.1	-1763.5	497.0	-273.9
	$\sigma_{cls,Max}$23	-8862.1	-1763.5	497.0	-22.9
	$\sigma_{cls,Med}$23	-8862.1	-1763.5	497.0	-8.6

Pilastro: 3/103 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./20.0 x 200.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
3	15	-19598.6	-6605.0	-14381.8	5.18	13.58	0.97
103	15	-18192.3	6605.0	14381.8	6.14	7.48	0.98

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	7740.7	12915.4	0.60	1.00	5607.3	14501.5	0.39	ø 8 2br.x4br./12.5	0.177
0.75	2.75	1.00	7740.7	8072.1	0.96	1.00	5607.3	9063.4	0.62	ø 8 2br.x4br./20.0	0.111
2.75	3.25	1.00	7740.7	12915.4	0.60	1.00	5607.3	14501.5	0.39	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
3	Ft. 20	-23970.7	961.8	-2083.8	141.6
	$\sigma_{s,c}$19	-25231.4	939.2	-2130.3	-484.6
	$\sigma_{cls,Max}$19	-25231.4	939.2	-2130.3	-40.5
	$\sigma_{cls,Med}$19	-25231.4	939.2	-2130.3	-17.2
103	Ft. 20	-22564.4	-579.3	1645.3	44.3
	$\sigma_{s,c}$19	-23825.2	-574.5	1669.5	-389.8
	$\sigma_{cls,Max}$19	-23825.2	-574.5	1669.5	-31.7
	$\sigma_{cls,Med}$19	-23825.2	-574.5	1669.5	-14.1
Combinazioni Frequenti					
3	Ft. 22	-22354.7	1023.9	-1995.4	156.0
	$\sigma_{s,c}$21	-23195.2	1008.9	-2026.4	-466.9
	$\sigma_{cls,Max}$21	-23195.2	1008.9	-2026.4	-39.2
	$\sigma_{cls,Med}$21	-23195.2	1008.9	-2026.4	-16.3
103	Ft. 22	-20948.4	-611.3	1587.8	57.8
	$\sigma_{s,c}$21	-21788.9	-608.1	1604.0	-372.3
	$\sigma_{cls,Max}$21	-21788.9	-608.1	1604.0	-30.5
	$\sigma_{cls,Med}$21	-21788.9	-608.1	1604.0	-13.4
Combinazioni Quasi Permanenti					
3	Ft. 23	-22369.1	1031.1	-1989.5	155.3
	$\sigma_{s,c}$23	-22369.1	1031.1	-1989.5	-460.0
	$\sigma_{cls,Max}$23	-22369.1	1031.1	-1989.5	-38.7
	$\sigma_{cls,Med}$23	-22369.1	1031.1	-1989.5	-16.0
103	Ft. 23	-20962.9	-617.0	1582.2	57.2
	$\sigma_{s,c}$23	-20962.9	-617.0	1582.2	-365.5
	$\sigma_{cls,Max}$23	-20962.9	-617.0	1582.2	-30.1
	$\sigma_{cls,Med}$23	-20962.9	-617.0	1582.2	-13.1

Pilastro: 103/203 / L 3.20[m] / Sezione 1 B 30 H 50 [cm]

Af: 8 ø 18 + 6 ø 16 =32.42 [cm²] < 2ϕ18 x 4 V + 1ϕ16 x 2 B + 2ϕ16 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 53.3 - ø 8 2br.x4br./15.0 x 213.3 - ø 8 2br.x4br./12.5 x 53.3

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
103	16	-9772.8	7607.8	13797.7	5.42	3.86	0.98
203	12	-8914.9	-584.4	6478.4	1.00	1.00	0.40

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.53	1.00	8785.4	12915.4	0.68	1.00	8714.5	14501.5	0.60	ø 8 2br.x4br./12.5	0.177
0.53	2.67	1.00	8785.4	10762.8	0.82	1.00	8714.5	12084.6	0.72	ø 8 2br.x4br./15.0	0.148
2.67	3.20	1.00	8785.4	12915.4	0.68	1.00	8714.5	14501.5	0.60	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
103	Ft. 20	-10968.3	-2339.5	-94.5	161.6
	$\sigma_{s,c}19$	-11766.9	-2375.9	-75.8	-273.7
	$\sigma_{cls,Max}19$	-11766.9	-2375.9	-75.8	-21.7
	$\sigma_{cls,Med}19$	-11766.9	-2375.9	-75.8	-10.3
203	Ft. 20	-9674.5	4.5	555.0	-17.9
	$\sigma_{s,c}19$	-10473.1	2.8	559.1	-134.4
	$\sigma_{cls,Max}19$	-10473.1	2.8	559.1	-10.6
	$\sigma_{cls,Med}19$	-10473.1	2.8	559.1	-5.3
Combinazioni Frequenti					
103	Ft. 22	-9951.6	-2288.1	-116.2	178.6
	$\sigma_{s,c}21$	-10484.0	-2312.3	-103.7	-265.6
	$\sigma_{cls,Max}21$	-10484.0	-2312.3	-103.7	-21.3
	$\sigma_{cls,Med}21$	-10484.0	-2312.3	-103.7	-10.0
203	Ft. 22	-8657.9	4.3	560.1	-8.1
	$\sigma_{s,c}21$	-9190.3	3.1	562.8	-125.4
	$\sigma_{cls,Max}21$	-9190.3	3.1	562.8	-10.0
	$\sigma_{cls,Med}21$	-9190.3	3.1	562.8	-5.0
Combinazioni Quasi Permanenti					
103	Ft. 23	-9962.3	-2287.4	-115.5	178.2
	$\sigma_{s,c}23$	-9962.3	-2287.4	-115.5	-262.6
	$\sigma_{cls,Max}23$	-9962.3	-2287.4	-115.5	-21.1
	$\sigma_{cls,Med}23$	-9962.3	-2287.4	-115.5	-9.8
203	Ft. 23	-8668.6	3.7	562.4	-7.9
	$\sigma_{s,c}23$	-8668.6	3.7	562.4	-121.7
	$\sigma_{cls,Max}23$	-8668.6	3.7	562.4	-9.8
	$\sigma_{cls,Med}23$	-8668.6	3.7	562.4	-4.9

Pilastro: 4/104 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./20.0 x 200.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
4	15	-21080.7	-5305.9	-14318.8	24.73	14.52	0.94
104	14	-15674.5	5305.9	13940.8	2.23	18.10	0.95

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	5073.5	12915.4	0.39	1.00	5493.1	14501.5	0.38	ø 8 2br.x4br./12.5	0.177
0.75	2.75	1.00	5073.5	8072.1	0.63	1.00	5493.1	9063.4	0.61	ø 8 2br.x4br./20.0	0.111
2.75	3.25	1.00	5073.5	12915.4	0.39	1.00	5493.1	14501.5	0.38	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
4	Ft. 20	-22912.0	-21.5	-1921.6	38.8
	$\sigma_{s,c}$19	-24220.9	-38.6	-1963.0	-382.8
	$\sigma_{cls,Max}$19	-24220.9	-38.6	-1963.0	-31.8
	$\sigma_{cls,Med}$19	-24220.9	-38.6	-1963.0	-15.7
104	Ft. 20	-21505.7	481.7	1917.1	99.3
	$\sigma_{s,c}$19	-22814.7	499.7	1973.3	-414.0
	$\sigma_{cls,Max}$19	-22814.7	499.7	1973.3	-34.7
	$\sigma_{cls,Med}$19	-22814.7	499.7	1973.3	-15.7
Combinazioni Frequenti					
4	Ft. 22	-21184.4	25.0	-1855.2	50.9
	$\sigma_{s,c}$21	-22057.1	13.6	-1882.8	-357.5
	$\sigma_{cls,Max}$21	-22057.1	13.6	-1882.8	-29.9
	$\sigma_{cls,Med}$21	-22057.1	13.6	-1882.8	-14.9
104	Ft. 22	-19778.2	436.7	1833.1	105.1
	$\sigma_{s,c}$21	-20650.8	448.7	1870.5	-384.7
	$\sigma_{cls,Max}$21	-20650.8	448.7	1870.5	-32.4
	$\sigma_{cls,Med}$21	-20650.8	448.7	1870.5	-14.7
Combinazioni Quasi Permanenti					
4	Ft. 23	-21188.4	30.2	-1852.7	50.8
	$\sigma_{s,c}$23	-21188.4	30.2	-1852.7	-349.9
	$\sigma_{cls,Max}$23	-21188.4	30.2	-1852.7	-29.4
	$\sigma_{cls,Med}$23	-21188.4	30.2	-1852.7	-14.6
104	Ft. 23	-19782.1	432.0	1831.0	104.1
	$\sigma_{s,c}$23	-19782.1	432.0	1831.0	-373.5
	$\sigma_{cls,Max}$23	-19782.1	432.0	1831.0	-31.6
	$\sigma_{cls,Med}$23	-19782.1	432.0	1831.0	-14.3

Pilastro: 104/204 / L 3.20[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 53.3 - ø 8 2br.x4br./20.0 x 213.3 - ø 8 2br.x4br./12.5 x 53.3

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
104	16	-10464.6	5710.3	13870.3	4.67	4.00	0.99
204	12	-8864.3	168.4	6117.5	1.00	1.00	0.40

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.53	1.00	7238.2	12915.4	0.56	1.00	8390.0	14501.5	0.58	ø 8 2br.x4br./12.5	0.177
0.53	2.67	1.00	7238.2	8072.1	0.90	1.00	8390.0	9063.4	0.93	ø 8 2br.x4br./20.0	0.111
2.67	3.20	1.00	7238.2	12915.4	0.56	1.00	8390.0	14501.5	0.58	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
104	Ft. 20	-11363.4	-2232.1	-296.7	188.7
	$\sigma_{s,c}$19	-12234.6	-2271.0	-303.5	-310.5
	$\sigma_{cls,Max}$19	-12234.6	-2271.0	-303.5	-25.1
	$\sigma_{cls,Med}$19	-12234.6	-2271.0	-303.5	-10.7
204	Ft. 20	-10069.6	70.0	189.5	-54.1
	$\sigma_{s,c}$19	-10940.9	63.6	169.2	-104.5
	$\sigma_{cls,Max}$19	-10940.9	63.6	169.2	-7.5
	$\sigma_{cls,Med}$19	-10940.9	63.6	169.2	-5.6
	Combinazioni Frequenti				
104	Ft. 22	-10193.7	-2177.6	-285.0	205.1
	$\sigma_{s,c}$21	-10774.5	-2203.6	-289.5	-296.4
	$\sigma_{cls,Max}$21	-10774.5	-2203.6	-289.5	-24.1
	$\sigma_{cls,Med}$21	-10774.5	-2203.6	-289.5	-10.3
204	Ft. 22	-8900.0	77.3	209.3	-42.7
	$\sigma_{s,c}$21	-9480.8	73.0	195.8	-96.5
	$\sigma_{cls,Max}$21	-9480.8	73.0	195.8	-7.1
	$\sigma_{cls,Med}$21	-9480.8	73.0	195.8	-4.8
	Combinazioni Quasi Permanenti				
104	Ft. 23	-10191.9	-2177.1	-284.4	204.9
	$\sigma_{s,c}$23	-10191.9	-2177.1	-284.4	-290.9
	$\sigma_{cls,Max}$23	-10191.9	-2177.1	-284.4	-23.8
	$\sigma_{cls,Med}$23	-10191.9	-2177.1	-284.4	-10.1
204	Ft. 23	-8898.2	77.0	207.7	-42.8
	$\sigma_{s,c}$23	-8898.2	77.0	207.7	-93.5
	$\sigma_{cls,Max}$23	-8898.2	77.0	207.7	-6.9
	$\sigma_{cls,Med}$23	-8898.2	77.0	207.7	-4.5

Pilastro: 5/105 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 8 ø 18 =20.36 [cm²] < 1ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./20.0 x 200.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
5	13	-15608.8	-5305.9	-10162.7	2.46	58.74	0.98
105	13	-14202.6	5305.9	-10162.7	1.94	20.80	0.99

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	3716.5	12915.4	0.29	1.00	4795.0	14501.5	0.33	ø 8 2br.x4br./12.5	0.177
0.75	2.75	1.00	3716.5	8072.1	0.46	1.00	4795.0	9063.4	0.53	ø 8 2br.x4br./20.0	0.111
2.75	3.25	1.00	3716.5	12915.4	0.29	1.00	4795.0	14501.5	0.33	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
5	Ft. 19	-29614.4	213.3	-2055.7	7.2
	$\sigma_{s,c}$19	-29614.4	213.3	-2055.7	-488.4
	$\sigma_{cls,Max}$19	-29614.4	213.3	-2055.7	-39.8
	$\sigma_{cls,Med}$19	-29614.4	213.3	-2055.7	-19.1
105	Ft. 20	-26821.1	788.4	810.5	-73.6
	$\sigma_{s,c}$19	-28208.2	731.5	856.3	-383.9
	$\sigma_{cls,Max}$19	-28208.2	731.5	856.3	-29.3
	$\sigma_{cls,Med}$19	-28208.2	731.5	856.3	-15.6
Combinazioni Frequenti					
5	Ft. 21	-27348.8	83.2	-1901.0	-3.5
	$\sigma_{s,c}$21	-27348.8	83.2	-1901.0	-441.1
	$\sigma_{cls,Max}$21	-27348.8	83.2	-1901.0	-36.0
	$\sigma_{cls,Med}$21	-27348.8	83.2	-1901.0	-17.7
105	Ft. 22	-25017.9	845.4	735.2	-62.1
	$\sigma_{s,c}$21	-25942.6	807.5	765.7	-361.5
	$\sigma_{cls,Max}$21	-25942.6	807.5	765.7	-27.6
	$\sigma_{cls,Med}$21	-25942.6	807.5	765.7	-14.4
Combinazioni Quasi Permanenti					
5	Ft. 23	-26434.4	27.1	-1841.5	-7.5
	$\sigma_{s,c}$23	-26434.4	27.1	-1841.5	-422.1
	$\sigma_{cls,Max}$23	-26434.4	27.1	-1841.5	-34.4
	$\sigma_{cls,Med}$23	-26434.4	27.1	-1841.5	-17.1
105	Ft. 23	-25028.2	841.2	732.1	-62.9
	$\sigma_{s,c}$23	-25028.2	841.2	732.1	-353.0
	$\sigma_{cls,Max}$23	-25028.2	841.2	732.1	-26.9
	$\sigma_{cls,Med}$23	-25028.2	841.2	732.1	-13.9

Pilastro: 105/205 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./20.0 x 195.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
105	13	-3142.9	-8567.3	-8820.1	1.00	2.02	0.73
205	13	-1849.2	6517.7	4820.3	1.00	1.00	0.45

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.50	1.00	5859.7	12915.4	0.45	1.00	8169.4	14501.5	0.56	ø 8 2br.x4br./12.5	0.177
0.50	2.45	1.00	5859.7	8072.1	0.73	1.00	8169.4	9063.4	0.90	ø 8 2br.x4br./20.0	0.111
2.45	2.95	1.00	5859.7	12915.4	0.45	1.00	8169.4	14501.5	0.56	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
105	Ft. 20	-8172.0	-2041.1	856.9	341.4
	$\sigma_{s,c}$20	-8172.0	-2041.1	856.9	-350.3
	$\sigma_{cls,Max}$20	-8172.0	-2041.1	856.9	-30.6
	$\sigma_{cls,Med}$20	-8172.0	-2041.1	856.9	-10.5
205	Ft. 19	-7493.1	471.8	455.7	27.2
	$\sigma_{s,c}$19	-7493.1	471.8	455.7	-138.1
	$\sigma_{cls,Max}$19	-7493.1	471.8	455.7	-11.2
	$\sigma_{cls,Med}$19	-7493.1	471.8	455.7	-4.5
Combinazioni Frequenti					
105	Ft. 22	-7365.7	-2088.7	913.3	387.5
	$\sigma_{s,c}$22	-7365.7	-2088.7	913.3	-360.7
	$\sigma_{cls,Max}$22	-7365.7	-2088.7	913.3	-31.9
	$\sigma_{cls,Med}$22	-7365.7	-2088.7	913.3	-10.9
205	Ft. 22	-6071.9	677.8	185.7	26.0
	$\sigma_{s,c}$21	-6481.8	616.4	262.0	-121.3
	$\sigma_{cls,Max}$21	-6481.8	616.4	262.0	-9.6
	$\sigma_{cls,Med}$21	-6481.8	616.4	262.0	-3.8
Combinazioni Quasi Permanenti					
105	Ft. 23	-7368.6	-2087.4	914.4	387.4
	$\sigma_{s,c}$23	-7368.6	-2087.4	914.4	-360.8
	$\sigma_{cls,Max}$23	-7368.6	-2087.4	914.4	-31.9
	$\sigma_{cls,Med}$23	-7368.6	-2087.4	914.4	-10.9
205	Ft. 23	-6074.9	675.8	185.1	25.6
	$\sigma_{s,c}$23	-6074.9	675.8	185.1	-115.1
	$\sigma_{cls,Max}$23	-6074.9	675.8	185.1	-9.1
	$\sigma_{cls,Med}$23	-6074.9	675.8	185.1	-3.7

Pilastro: 6/106 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 8 ø 16 =16.08 [cm²] < 1ϕ16 x 4 V + 0ϕ16 x 2 B + 2ϕ16 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./15.0 x 200.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
6	15	-8976.3	-81.0	7284.5	1.98	6.79	0.86
106	15	-7570.1	81.0	7284.5	1.00	6.60	0.88

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	327.6	12915.4	0.03	1.00	98.6	14501.5	0.01	ø 8 2br.x4br./12.5	0.177
0.75	2.75	1.00	327.6	10762.8	0.03	1.00	98.6	12084.6	0.01	ø 8 2br.x4br./15.0	0.148
2.75	3.25	1.00	327.6	12915.4	0.03	1.00	98.6	14501.5	0.01	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
6	Ft. 19	-8952.2	-50.1	763.2	36.2
	$\sigma_{s,c}$19	-8952.2	-50.1	763.2	-173.6
	$\sigma_{cls,Max}$19	-8952.2	-50.1	763.2	-14.6
	$\sigma_{cls,Med}$19	-8952.2	-50.1	763.2	-7.1
106	Ft. 19	-7545.9	195.9	813.6	108.1
	$\sigma_{s,c}$19	-7545.9	195.9	813.6	-191.1
	$\sigma_{cls,Max}$19	-7545.9	195.9	813.6	-16.8
	$\sigma_{cls,Med}$19	-7545.9	195.9	813.6	-7.5
Combinazioni Frequenti					
6	Ft. 21	-8418.8	-53.6	717.6	34.7
	$\sigma_{s,c}$21	-8418.8	-53.6	717.6	-163.9
	$\sigma_{cls,Max}$21	-8418.8	-53.6	717.6	-13.8
	$\sigma_{cls,Med}$21	-8418.8	-53.6	717.6	-6.7
106	Ft. 21	-7012.5	192.0	769.7	107.3
	$\sigma_{s,c}$21	-7012.5	192.0	769.7	-181.1
	$\sigma_{cls,Max}$21	-7012.5	192.0	769.7	-16.0
	$\sigma_{cls,Med}$21	-7012.5	192.0	769.7	-7.1
Combinazioni Quasi Permanenti					
6	Ft. 23	-8202.6	-55.1	698.7	34.0
	$\sigma_{s,c}$23	-8202.6	-55.1	698.7	-159.9
	$\sigma_{cls,Max}$23	-8202.6	-55.1	698.7	-13.4
	$\sigma_{cls,Med}$23	-8202.6	-55.1	698.7	-6.5
106	Ft. 23	-6796.4	190.6	751.6	106.9
	$\sigma_{s,c}$23	-6796.4	190.6	751.6	-177.0
	$\sigma_{cls,Max}$23	-6796.4	190.6	751.6	-15.6
	$\sigma_{cls,Med}$23	-6796.4	190.6	751.6	-6.9

Pilastro: 106/206 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 8 ø 16 =16.08 [cm²] < 1ϕ16 x 4 V + 0ϕ16 x 2 B + 2ϕ16 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./15.0 x 195.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
106	17	-6916.4	9503.7	-5767.2	1.00	1.22	0.94
206	12	-6674.1	-6434.0	3005.7	1.00	1.00	0.55

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.50	1.00	9154.3	12915.4	0.71	1.00	3686.7	14501.5	0.25	ø 8 2br.x4br./12.5	0.177
0.50	2.45	1.00	9154.3	10762.8	0.85	1.00	3686.7	12084.6	0.31	ø 8 2br.x4br./15.0	0.148
2.45	2.95	1.00	9154.3	12915.4	0.71	1.00	3686.7	14501.5	0.25	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
106	Ft. 19	-8085.2	1361.9	-910.5	372.8
	$\sigma_{s,c}19$	-8085.2	1361.9	-910.5	-369.2
	$\sigma_{cls,Max}19$	-8085.2	1361.9	-910.5	-32.7
	$\sigma_{cls,Med}19$	-8085.2	1361.9	-910.5	-10.9
206	Ft. 19	-6791.4	-1881.4	991.9	651.3
	$\sigma_{s,c}19$	-6791.4	-1881.4	991.9	-466.2
	$\sigma_{cls,Max}19$	-6791.4	-1881.4	991.9	-42.7
	$\sigma_{cls,Med}19$	-6791.4	-1881.4	991.9	-14.2
Combinazioni Frequenti					
106	Ft. 21	-7465.4	1254.2	-879.5	359.9
	$\sigma_{s,c}21$	-7465.4	1254.2	-879.5	-348.0
	$\sigma_{cls,Max}21$	-7465.4	1254.2	-879.5	-31.0
	$\sigma_{cls,Med}21$	-7465.4	1254.2	-879.5	-10.3
206	Ft. 21	-6171.7	-1676.5	991.2	617.4
	$\sigma_{s,c}21$	-6171.7	-1676.5	991.2	-435.9
	$\sigma_{cls,Max}21$	-6171.7	-1676.5	991.2	-40.2
	$\sigma_{cls,Med}21$	-6171.7	-1676.5	991.2	-13.4
Combinazioni Quasi Permanenti					
106	Ft. 23	-7217.3	1212.4	-865.6	354.5
	$\sigma_{s,c}23$	-7217.3	1212.4	-865.6	-339.4
	$\sigma_{cls,Max}23$	-7217.3	1212.4	-865.6	-30.3
	$\sigma_{cls,Med}23$	-7217.3	1212.4	-865.6	-10.1
206	Ft. 23	-5923.6	-1595.3	991.3	605.2
	$\sigma_{s,c}23$	-5923.6	-1595.3	991.3	-423.8
	$\sigma_{cls,Max}23$	-5923.6	-1595.3	991.3	-39.3
	$\sigma_{cls,Med}23$	-5923.6	-1595.3	991.3	-13.1

Pilastro: 7/107 / L 3.05[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./7.5 x 305.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
7	17	-23868.3	19132.4	-5575.2	1.00	1.00	0.85
107	17	-22462.1	-14611.9	3941.9	1.00	1.00	0.63

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.30	1.00	20456.7	21525.6	0.95	1.00	7613.6	24169.1	0.32	ø 8 2br.x4br./7.5	0.295

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
7	Ft. 20	-15543.3	7124.5	-2839.1	1571.6
	$\sigma_{s,c}$19	-16390.3	7042.9	-2925.6	-1167.2
	$\sigma_{cls,Max}$19	-16390.3	7042.9	-2925.6	-105.9
	$\sigma_{cls,Med}$19	-16390.3	7042.9	-2925.6	-35.8
107	Ft. 20	-14137.1	-4580.2	1783.2	864.5
	$\sigma_{s,c}$20	-14137.1	-4580.2	1783.2	-753.9
	$\sigma_{cls,Max}$20	-14137.1	-4580.2	1783.2	-66.9
	$\sigma_{cls,Med}$20	-14137.1	-4580.2	1783.2	-23.0
Combinazioni Frequenti					
7	Ft. 22	-14420.6	7230.3	-2714.0	1604.1
	$\sigma_{s,c}$21	-14985.2	7175.9	-2771.7	-1152.7
	$\sigma_{cls,Max}$21	-14985.2	7175.9	-2771.7	-104.8
	$\sigma_{cls,Med}$21	-14985.2	7175.9	-2771.7	-35.7
107	Ft. 22	-13014.3	-4831.1	1702.2	934.6
	$\sigma_{s,c}$22	-13014.3	-4831.1	1702.2	-763.2
	$\sigma_{cls,Max}$22	-13014.3	-4831.1	1702.2	-68.0
	$\sigma_{cls,Med}$22	-13014.3	-4831.1	1702.2	-23.7
Combinazioni Quasi Permanenti					
7	Ft. 23	-14422.0	7229.6	-2711.8	1603.5
	$\sigma_{s,c}$23	-14422.0	7229.6	-2711.8	-1147.1
	$\sigma_{cls,Max}$23	-14422.0	7229.6	-2711.8	-104.4
	$\sigma_{cls,Med}$23	-14422.0	7229.6	-2711.8	-35.6
107	Ft. 23	-13015.8	-4830.2	1700.1	933.9
	$\sigma_{s,c}$23	-13015.8	-4830.2	1700.1	-762.8
	$\sigma_{cls,Max}$23	-13015.8	-4830.2	1700.1	-68.0
	$\sigma_{cls,Med}$23	-13015.8	-4830.2	1700.1	-23.7

Pilastro: 8/108 / L 3.05[m] / Sezione 1 B 30 H 50 [cm]

Af: 18 ø 18 =45.80 [cm²] < 3ϕ18 x 4 V + 1ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./5.0 x 305.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
8	17	-30517.2	23508.3	-4547.3	1.00	1.06	0.67
108	17	-29110.9	-21556.8	4547.3	1.00	1.00	0.63

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.30	1.00	27605.2	32288.4	0.85	1.00	5378.4	36253.7	0.15	ø 8 2br.x4br./5.0	0.443

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
8	Ft. 20	-31152.1	9852.6	-1983.4	968.4
	$\sigma_{s,c}$19	-34457.6	9981.7	-1994.5	-1119.1
	$\sigma_{cls,Max}$19	-34457.6	9981.7	-1994.5	-94.2
	$\sigma_{cls,Med}$19	-34457.6	9981.7	-1994.5	-36.2
108	Ft. 19	-33051.3	-13685.1	2181.7	1457.8
	$\sigma_{s,c}$19	-33051.3	-13685.1	2181.7	-1396.3
	$\sigma_{cls,Max}$19	-33051.3	-13685.1	2181.7	-119.5
	$\sigma_{cls,Med}$19	-33051.3	-13685.1	2181.7	-47.0
	Combinazioni Frequenti				
8	Ft. 22	-26717.7	9704.1	-1981.6	1035.8
	$\sigma_{s,c}$21	-28921.4	9790.2	-1989.0	-1079.2
	$\sigma_{cls,Max}$21	-28921.4	9790.2	-1989.0	-91.9
	$\sigma_{cls,Med}$21	-28921.4	9790.2	-1989.0	-34.9
108	Ft. 21	-27515.1	-12235.9	2197.3	1383.3
	$\sigma_{s,c}$21	-27515.1	-12235.9	2197.3	-1270.0
	$\sigma_{cls,Max}$21	-27515.1	-12235.9	2197.3	-109.6
	$\sigma_{cls,Med}$21	-27515.1	-12235.9	2197.3	-42.0
	Combinazioni Quasi Permanenti				
8	Ft. 23	-26711.7	9709.3	-1984.5	1037.1
	$\sigma_{s,c}$23	-26711.7	9709.3	-1984.5	-1062.6
	$\sigma_{cls,Max}$23	-26711.7	9709.3	-1984.5	-91.0
	$\sigma_{cls,Med}$23	-26711.7	9709.3	-1984.5	-34.4
108	Ft. 23	-25305.5	-11654.1	2200.6	1353.2
	$\sigma_{s,c}$23	-25305.5	-11654.1	2200.6	-1219.1
	$\sigma_{cls,Max}$23	-25305.5	-11654.1	2200.6	-105.6
	$\sigma_{cls,Med}$23	-25305.5	-11654.1	2200.6	-40.1

Pilastro: 10/110 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 4 ø 18 + 4 ø 16 =18.22 [cm²] < 1ϕ18 x 4 V + 0ϕ16 x 2 B + 2ϕ16 x 2 H >
Staffe: ø 8 2br.x4br./10.0 x 300.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
10	17	-13273.3	15727.6	-2302.5	1.00	1.00	0.98
110	17	-11867.0	-15701.4	416.8	1.00	1.00	0.93

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.25	1.00	15480.8	16144.2	0.96	1.00	2161.0	18126.8	0.12	ø 8 2br.x4br./10.0	0.222

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
10	Ft. 20	-19811.5	5809.8	-846.2	1175.2
	$\sigma_{s,c}$20	-19811.5	5809.8	-846.2	-931.4
	$\sigma_{cls,Max}$20	-19811.5	5809.8	-846.2	-80.8
	$\sigma_{cls,Med}$19	-21757.0	5837.3	-803.5	-33.1
110	Ft. 20	-18405.2	-6691.1	-540.9	1484.7
	$\sigma_{s,c}$19	-20350.7	-6855.6	-700.1	-1033.5
	$\sigma_{cls,Max}$19	-20350.7	-6855.6	-700.1	-90.4
	$\sigma_{cls,Med}$19	-20350.7	-6855.6	-700.1	-38.7
	Combinazioni Frequenti				
10	Ft. 22	-17181.0	5798.1	-891.2	1320.4
	$\sigma_{s,c}$22	-17181.0	5798.1	-891.2	-932.4
	$\sigma_{cls,Max}$22	-17181.0	5798.1	-891.2	-82.3
	$\sigma_{cls,Med}$21	-18478.0	5816.5	-862.7	-33.2
110	Ft. 22	-15774.7	-6487.4	-337.2	1509.9
	$\sigma_{s,c}$21	-17071.7	-6597.1	-443.3	-939.1
	$\sigma_{cls,Max}$21	-17071.7	-6597.1	-443.3	-82.8
	$\sigma_{cls,Med}$21	-17071.7	-6597.1	-443.3	-37.1
	Combinazioni Quasi Permanenti				
10	Ft. 23	-17172.9	5803.7	-888.5	1322.1
	$\sigma_{s,c}$23	-17172.9	5803.7	-888.5	-932.5
	$\sigma_{cls,Max}$23	-17172.9	5803.7	-888.5	-82.3
	$\sigma_{cls,Med}$23	-17172.9	5803.7	-888.5	-33.2
110	Ft. 23	-15766.6	-6490.9	-339.1	1512.1
	$\sigma_{s,c}$23	-15766.6	-6490.9	-339.1	-899.5
	$\sigma_{cls,Max}$23	-15766.6	-6490.9	-339.1	-79.6
	$\sigma_{cls,Med}$23	-15766.6	-6490.9	-339.1	-36.5

Pilastro: 11/111 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 8 ø 16 =16.08 [cm²] < 1ϕ16 x 4 V + 0ϕ16 x 2 B + 2ϕ16 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 300.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
11	17	-16422.0	12195.0	-2883.2	1.15	1.00	0.84
111	17	-15015.8	-12195.0	2825.4	1.00	1.00	0.85

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.25	1.00	12693.8	12915.4	0.98	1.00	4566.5	14501.5	0.31	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
11	Ft. 20	-21120.9	3793.7	-1579.6	747.9
	$\sigma_{s,c}$19	-23092.6	3784.2	-1660.2	-853.9
	$\sigma_{cls,Max}$19	-23092.6	3784.2	-1660.2	-72.6
	$\sigma_{cls,Med}$19	-23092.6	3784.2	-1660.2	-25.3
111	Ft. 20	-19714.7	-5157.6	2002.7	1449.8
	$\sigma_{s,c}$19	-21686.4	-5301.0	2168.9	-1185.5
	$\sigma_{cls,Max}$19	-21686.4	-5301.0	2168.9	-105.3
	$\sigma_{cls,Med}$19	-21686.4	-5301.0	2168.9	-36.1
Combinazioni Frequenti					
11	Ft. 22	-18457.5	3829.8	-1463.9	853.0
	$\sigma_{s,c}$21	-19772.0	3823.5	-1517.7	-837.9
	$\sigma_{cls,Max}$21	-19772.0	3823.5	-1517.7	-72.3
	$\sigma_{cls,Med}$21	-19772.0	3823.5	-1517.7	-25.3
111	Ft. 22	-17051.3	-4979.8	1774.9	1468.1
	$\sigma_{s,c}$21	-18365.7	-5075.4	1885.8	-1100.8
	$\sigma_{cls,Max}$21	-18365.7	-5075.4	1885.8	-98.5
	$\sigma_{cls,Med}$21	-18365.7	-5075.4	1885.8	-34.0
Combinazioni Quasi Permanenti					
11	Ft. 23	-18449.8	3835.0	-1462.1	854.7
	$\sigma_{s,c}$23	-18449.8	3835.0	-1462.1	-831.3
	$\sigma_{cls,Max}$23	-18449.8	3835.0	-1462.1	-72.1
	$\sigma_{cls,Med}$23	-18449.8	3835.0	-1462.1	-25.3
111	Ft. 23	-17043.6	-4982.8	1773.6	1469.2
	$\sigma_{s,c}$23	-17043.6	-4982.8	1773.6	-1066.3
	$\sigma_{cls,Max}$23	-17043.6	-4982.8	1773.6	-95.7
	$\sigma_{cls,Med}$23	-17043.6	-4982.8	1773.6	-33.2

Pilastro: 12/112 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 300.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
12	13	-39897.7	-27786.5	-490.8	18.54	1.88	0.99
112	13	-38491.5	-27786.5	-490.8	15.56	1.00	1.00

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.25	1.00	11910.6	12915.4	0.92	1.00	3209.6	14501.5	0.22	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
12	Ft. 20	-37605.1	2961.1	-1362.1	64.6
	$\sigma_{s,c}$19	-40957.6	3064.4	-1409.2	-669.6
	$\sigma_{cls,Max}$19	-40957.6	3064.4	-1409.2	-52.2
	$\sigma_{cls,Med}$19	-40957.6	3064.4	-1409.2	-22.3
112	Ft. 19	-39551.3	-5611.2	711.7	251.5
	$\sigma_{s,c}$19	-39551.3	-5611.2	711.7	-802.4
	$\sigma_{cls,Max}$19	-39551.3	-5611.2	711.7	-62.9
	$\sigma_{cls,Med}$19	-39551.3	-5611.2	711.7	-27.6
Combinazioni Frequenti					
12	Ft. 22	-33082.9	2850.7	-1289.5	91.9
	$\sigma_{s,c}$21	-35317.9	2919.5	-1320.8	-611.5
	$\sigma_{cls,Max}$21	-35317.9	2919.5	-1320.8	-48.1
	$\sigma_{cls,Med}$21	-35317.9	2919.5	-1320.8	-19.9
112	Ft. 22	-31676.7	-4734.8	684.4	252.8
	$\sigma_{s,c}$21	-33911.6	-4990.1	689.9	-714.6
	$\sigma_{cls,Max}$21	-33911.6	-4990.1	689.9	-56.3
	$\sigma_{cls,Med}$21	-33911.6	-4990.1	689.9	-24.4
Combinazioni Quasi Permanenti					
12	Ft. 23	-33071.3	2856.7	-1287.3	92.4
	$\sigma_{s,c}$23	-33071.3	2856.7	-1287.3	-588.6
	$\sigma_{cls,Max}$23	-33071.3	2856.7	-1287.3	-46.5
	$\sigma_{cls,Med}$23	-33071.3	2856.7	-1287.3	-18.9
112	Ft. 23	-31665.1	-4738.6	682.6	253.3
	$\sigma_{s,c}$23	-31665.1	-4738.6	682.6	-679.5
	$\sigma_{cls,Max}$23	-31665.1	-4738.6	682.6	-53.7
	$\sigma_{cls,Med}$23	-31665.1	-4738.6	682.6	-23.1

Pilastro: 112/212 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 18 ø 18 =45.80 [cm²] < 3ϕ18 x 4 V + 1ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./5.0 x 295.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
112	16	-10417.7	27834.3	3804.3	2.54	1.00	0.81
212	18	-8214.5	-13587.2	-1356.1	1.00	1.00	0.37

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	2.95	1.00	22443.2	32288.4	0.70	1.00	4795.0	36253.7	0.13	ø 8 2br.x4br./5.0	0.443

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
112	Ft. 19	-14512.0	6062.1	591.1	591.9
	$\sigma_{s,c}$19	-14512.0	6062.1	591.1	-569.0
	$\sigma_{cls,Max}$19	-14512.0	6062.1	591.1	-48.1
	$\sigma_{cls,Med}$19	-14512.0	6062.1	591.1	-20.4
212	Ft. 19	-13218.3	-5111.2	168.0	433.3
	$\sigma_{s,c}$19	-13218.3	-5111.2	168.0	-441.9
	$\sigma_{cls,Max}$19	-13218.3	-5111.2	168.0	-36.6
	$\sigma_{cls,Med}$19	-13218.3	-5111.2	168.0	-17.2
Combinazioni Frequenti					
112	Ft. 21	-13185.7	5177.0	555.1	497.3
	$\sigma_{s,c}$21	-13185.7	5177.0	555.1	-496.8
	$\sigma_{cls,Max}$21	-13185.7	5177.0	555.1	-41.9
	$\sigma_{cls,Med}$21	-13185.7	5177.0	555.1	-17.6
212	Ft. 21	-11891.9	-4464.6	117.7	368.0
	$\sigma_{s,c}$21	-11891.9	-4464.6	117.7	-384.2
	$\sigma_{cls,Max}$21	-11891.9	-4464.6	117.7	-31.7
	$\sigma_{cls,Med}$21	-11891.9	-4464.6	117.7	-15.1
Combinazioni Quasi Permanenti					
112	Ft. 23	-12658.4	4823.6	541.4	459.6
	$\sigma_{s,c}$23	-12658.4	4823.6	541.4	-468.0
	$\sigma_{cls,Max}$23	-12658.4	4823.6	541.4	-39.4
	$\sigma_{cls,Med}$23	-12658.4	4823.6	541.4	-16.5
212	Ft. 23	-11364.7	-4206.2	96.8	341.7
	$\sigma_{s,c}$23	-11364.7	-4206.2	96.8	-361.1
	$\sigma_{cls,Max}$23	-11364.7	-4206.2	96.8	-29.7
	$\sigma_{cls,Med}$23	-11364.7	-4206.2	96.8	-14.2

Pilastro: 13/113 / L 3.05[m] / Sezione 2 B 50 H 30 [cm]

Af: 16 ø 18 =40.72 [cm²] < 3ϕ18 x 4 V + 2ϕ18 x 2 B + 0ϕ18 x 2 H >
Staffe: ø 8 4br.x2br./12.5 x 305.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
13	17	-7992.3	15060.3	-7886.4	1.00	1.00	0.87
113	17	-6586.1	-9084.6	3013.6	1.00	1.00	0.51

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.30	1.00	14201.9	14501.5	0.98	1.00	8719.7	12915.4	0.68	ø 8 4br.x2br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
13	Ft. 20	-8179.9	6726.9	-3245.7	1779.4
	$\sigma_{s,c}$19	-8859.3	6786.1	-3178.2	-1030.5
	$\sigma_{cls,Max}$19	-8859.3	6786.1	-3178.2	-106.5
	$\sigma_{cls,Med}$19	-8859.3	6786.1	-3178.2	-41.6
113	Ft. 19	-7453.1	-4492.4	-628.5	978.7
	$\sigma_{s,c}$19	-7453.1	-4492.4	-628.5	-552.7
	$\sigma_{cls,Max}$19	-7453.1	-4492.4	-628.5	-59.2
	$\sigma_{cls,Med}$19	-7453.1	-4492.4	-628.5	-27.1
	Combinazioni Frequenti				
13	Ft. 22	-7276.7	6642.4	-3322.9	1789.7
	$\sigma_{s,c}$21	-7729.6	6681.8	-3277.9	-1021.6
	$\sigma_{cls,Max}$21	-7729.6	6681.8	-3277.9	-105.8
	$\sigma_{cls,Med}$21	-7729.6	6681.8	-3277.9	-41.0
113	Ft. 22	-5870.4	-4364.6	134.6	935.4
	$\sigma_{s,c}$21	-6323.4	-4400.1	-86.2	-481.7
	$\sigma_{cls,Max}$21	-6323.4	-4400.1	-86.2	-53.4
	$\sigma_{cls,Med}$21	-6323.4	-4400.1	-86.2	-26.4
	Combinazioni Quasi Permanenti				
13	Ft. 23	-7277.3	6641.1	-3320.0	1789.1
	$\sigma_{s,c}$23	-7277.3	6641.1	-3320.0	-1018.4
	$\sigma_{cls,Max}$23	-7277.3	6641.1	-3320.0	-105.6
	$\sigma_{cls,Med}$23	-7277.3	6641.1	-3320.0	-40.7
113	Ft. 23	-5871.0	-4363.8	132.4	935.0
	$\sigma_{s,c}$23	-5871.0	-4363.8	132.4	-479.1
	$\sigma_{cls,Max}$23	-5871.0	-4363.8	132.4	-53.3
	$\sigma_{cls,Med}$23	-5871.0	-4363.8	132.4	-26.1

Pilastro: 14/114 / L 3.05[m] / Sezione 2 B 50 H 30 [cm]

Af: 8 ø 18 =20.36 [cm²] < 1ϕ18 x 4 V + 2ϕ18 x 2 B + 0ϕ18 x 2 H >
Staffe: ø 8 4br.x2br./12.5 x 50.8 - ø 8 4br.x2br./15.0 x 203.3 - ø 8 4br.x2br./12.5 x 50.8

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
14	17	-15007.3	9841.3	-6500.9	1.00	1.00	0.97
114	17	-13601.1	-6388.6	6311.5	1.00	1.00	0.67

Verifiche a Taglio

Da [m]	A [m]	cotg(θ)$_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	cotg(θ)$_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.76	1.00	9390.6	14501.5	0.65	1.00	8608.3	12915.4	0.67	ø 8 4br.x2br./12.5	0.177
0.76	2.79	1.00	9390.6	12084.6	0.78	1.00	8608.3	10762.8	0.80	ø 8 4br.x2br./15.0	0.148
2.79	3.30	1.00	9390.6	14501.5	0.65	1.00	8608.3	12915.4	0.67	ø 8 4br.x2br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
14	Ft. 20	-14988.3	4311.3	-2907.4	1767.1
	$\sigma_{s,c}$19	-16463.8	4341.1	-2902.3	-1097.9
	$\sigma_{cls,Max}$19	-16463.8	4341.1	-2902.3	-109.0
	$\sigma_{cls,Med}$19	-16463.8	4341.1	-2902.3	-38.9
114	Ft. 20	-13582.0	-3086.0	3045.8	1336.4
	$\sigma_{s,c}$19	-15057.6	-3123.6	3079.6	-943.9
	$\sigma_{cls,Max}$19	-15057.6	-3123.6	3079.6	-89.8
	$\sigma_{cls,Med}$19	-15057.6	-3123.6	3079.6	-30.4
Combinazioni Frequenti					
14	Ft. 22	-13020.4	4268.9	-2893.2	1841.5
	$\sigma_{s,c}$21	-14004.1	4288.7	-2889.8	-1076.5
	$\sigma_{cls,Max}$21	-14004.1	4288.7	-2889.8	-108.4
	$\sigma_{cls,Med}$21	-14004.1	4288.7	-2889.8	-38.4
114	Ft. 22	-11614.1	-3034.0	2983.7	1397.0
	$\sigma_{s,c}$21	-12597.8	-3059.1	3006.2	-916.9
	$\sigma_{cls,Max}$21	-12597.8	-3059.1	3006.2	-88.6
	$\sigma_{cls,Med}$21	-12597.8	-3059.1	3006.2	-29.8
Combinazioni Quasi Permanenti					
14	Ft. 23	-13020.3	4268.3	-2888.5	1840.2
	$\sigma_{s,c}$23	-13020.3	4268.3	-2888.5	-1068.3
	$\sigma_{cls,Max}$23	-13020.3	4268.3	-2888.5	-108.3
	$\sigma_{cls,Med}$23	-13020.3	4268.3	-2888.5	-38.2
114	Ft. 23	-11614.0	-3033.6	2979.9	1396.0
	$\sigma_{s,c}$23	-11614.0	-3033.6	2979.9	-906.2
	$\sigma_{cls,Max}$23	-11614.0	-3033.6	2979.9	-88.1
	$\sigma_{cls,Med}$23	-11614.0	-3033.6	2979.9	-29.6

Pilastro: 15/115 / L 3.05[m] / Sezione 1 B 30 H 50 [cm]

Af: 18 ø 18 =45.80 [cm²] < 3ϕ18 x 4 V + 1ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./5.0 x 305.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
15	17	-5872.8	31390.6	-3250.5	1.00	1.00	0.90
115	17	-4466.6	-29526.0	3039.8	1.00	1.00	0.85

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.30	1.00	26502.5	32288.4	0.82	1.00	5032.1	36253.7	0.14	ø 8 2br.x4br./5.0	0.443

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
15	Ft. 20	-12751.4	13729.2	-1857.6	1839.7
	$\sigma_{s,c}$19	-14454.2	13883.9	-1934.4	-1274.4
	$\sigma_{cls,Max}$19	-14454.2	13883.9	-1934.4	-113.2
	$\sigma_{cls,Med}$19	-14454.2	13883.9	-1934.4	-44.3
115	Ft. 19	-13048.0	-14465.3	2156.1	1979.0
	$\sigma_{s,c}$19	-13048.0	-14465.3	2156.1	-1335.1
	$\sigma_{cls,Max}$19	-13048.0	-14465.3	2156.1	-119.3
	$\sigma_{cls,Med}$19	-13048.0	-14465.3	2156.1	-46.0
	Combinazioni Frequenti				
15	Ft. 22	-10472.8	13516.3	-1747.0	1843.5
	$\sigma_{s,c}$21	-11608.1	13619.5	-1798.2	-1220.8
	$\sigma_{cls,Max}$21	-11608.1	13619.5	-1798.2	-109.0
	$\sigma_{cls,Med}$21	-11608.1	13619.5	-1798.2	-42.9
115	Ft. 21	-10201.8	-13887.8	1923.0	1927.2
	$\sigma_{s,c}$21	-10201.8	-13887.8	1923.0	-1247.3
	$\sigma_{cls,Max}$21	-10201.8	-13887.8	1923.0	-111.9
	$\sigma_{cls,Med}$21	-10201.8	-13887.8	1923.0	-43.6
	Combinazioni Quasi Permanenti				
15	Ft. 23	-10471.0	13514.9	-1745.2	1843.1
	$\sigma_{s,c}$23	-10471.0	13514.9	-1745.2	-1199.5
	$\sigma_{cls,Max}$23	-10471.0	13514.9	-1745.2	-107.3
	$\sigma_{cls,Med}$23	-10471.0	13514.9	-1745.2	-42.4
115	Ft. 23	-9064.8	-13658.2	1831.1	1906.9
	$\sigma_{s,c}$23	-9064.8	-13658.2	1831.1	-1212.2
	$\sigma_{cls,Max}$23	-9064.8	-13658.2	1831.1	-109.0
	$\sigma_{cls,Med}$23	-9064.8	-13658.2	1831.1	-42.7

Pilastro: 16/116 / L 3.05[m] / Sezione 1 B 30 H 50 [cm]

Af: 8 ø 18 =20.36 [cm²] < 1ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./10.0 x 305.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
16	13	-25217.2	-53079.1	-914.5	71.30	1.00	3.04
116	13	-23811.0	53079.1	347.1	70.79	1.00	3.04

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.30	1.00	16059.9	16144.2	0.99	1.00	1245.6	18126.8	0.07	ø 8 2br.x4br./10.0	0.222

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
16	Ft. 20	-30702.7	15222.8	-1984.8	4012.3
	$\sigma_{s,c}$19	-33968.9	15390.0	-2159.1	-2369.7
	$\sigma_{cls,Max}$19	-33968.9	15390.0	-2159.1	-213.3
	$\sigma_{cls,Med}$19	-33968.9	15390.0	-2159.1	-87.0
116	Ft. 20	-29296.4	-12638.0	1070.4	2999.2
	$\sigma_{s,c}$19	-32562.6	-12743.6	1244.6	-1873.4
	$\sigma_{cls,Max}$19	-32562.6	-12743.6	1244.6	-165.5
	$\sigma_{cls,Med}$19	-32562.6	-12743.6	1244.6	-71.4
	Combinazioni Frequenti				
16	Ft. 22	-25638.5	15066.2	-1725.4	4169.3
	$\sigma_{s,c}$21	-27816.0	15177.6	-1841.6	-2257.4
	$\sigma_{cls,Max}$21	-27816.0	15177.6	-1841.6	-205.5
	$\sigma_{cls,Med}$21	-27816.0	15177.6	-1841.6	-85.4
116	Ft. 22	-24232.3	-12568.4	828.6	3186.3
	$\sigma_{s,c}$21	-26409.8	-12638.8	944.7	-1776.6
	$\sigma_{cls,Max}$21	-26409.8	-12638.8	944.7	-159.2
	$\sigma_{cls,Med}$21	-26409.8	-12638.8	944.7	-70.6
	Combinazioni Quasi Permanenti				
16	Ft. 23	-25480.9	15080.9	-1719.4	4181.4
	$\sigma_{s,c}$23	-25480.9	15080.9	-1719.4	-2211.0
	$\sigma_{cls,Max}$23	-25480.9	15080.9	-1719.4	-202.2
	$\sigma_{cls,Med}$23	-25480.9	15080.9	-1719.4	-84.6
116	Ft. 23	-24074.7	-12584.3	826.4	3199.6
	$\sigma_{s,c}$23	-24074.7	-12584.3	826.4	-1735.3
	$\sigma_{cls,Max}$23	-24074.7	-12584.3	826.4	-156.4
	$\sigma_{cls,Med}$23	-24074.7	-12584.3	826.4	-70.1

Pilastro: 17/117 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 18 ø 18 =45.80 [cm²] < 3ϕ18 x 4 V + 1ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./5.0 x 300.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
17	14	-34028.6	-32786.4	898.8	194.01	5.77	0.82
117	14	-32622.4	-32786.4	-898.8	20.63	4.65	0.82

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	3.25	1.00	23495.9	32288.4	0.73	1.00	2454.9	36253.7	0.07	ø 8 2br.x4br./5.0	0.443

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
17	Ft. 20	-37739.1	11667.5	-411.0	852.6
	$\sigma_{s,c}$19	-40974.3	11806.1	-348.2	-1074.7
	$\sigma_{cls,Max}$19	-40974.3	11806.1	-348.2	-86.8
	$\sigma_{cls,Med}$19	-40974.3	11806.1	-348.2	-41.3
117	Ft. 20	-36332.8	-9670.8	46.7	581.0
	$\sigma_{s,c}$19	-39568.0	-9784.4	-78.3	-895.8
	$\sigma_{cls,Max}$19	-39568.0	-9784.4	-78.3	-71.0
	$\sigma_{cls,Med}$19	-39568.0	-9784.4	-78.3	-35.0
Combinazioni Frequenti					
17	Ft. 22	-33319.7	11510.0	-488.5	923.8
	$\sigma_{s,c}$21	-35476.5	11602.4	-446.7	-1042.8
	$\sigma_{cls,Max}$21	-35476.5	11602.4	-446.7	-85.3
	$\sigma_{cls,Med}$21	-35476.5	11602.4	-446.7	-39.9
117	Ft. 22	-31913.5	-9542.2	215.5	662.8
	$\sigma_{s,c}$21	-34070.3	-9617.9	132.2	-860.4
	$\sigma_{cls,Max}$21	-34070.3	-9617.9	132.2	-69.1
	$\sigma_{cls,Med}$21	-34070.3	-9617.9	132.2	-33.7
Combinazioni Quasi Permanenti					
17	Ft. 23	-33296.2	11516.1	-487.2	924.9
	$\sigma_{s,c}$23	-33296.2	11516.1	-487.2	-1030.0
	$\sigma_{cls,Max}$23	-33296.2	11516.1	-487.2	-84.7
	$\sigma_{cls,Med}$23	-33296.2	11516.1	-487.2	-39.3
117	Ft. 23	-31890.0	-9547.3	216.0	663.9
	$\sigma_{s,c}$23	-31890.0	-9547.3	216.0	-853.9
	$\sigma_{cls,Max}$23	-31890.0	-9547.3	216.0	-69.1
	$\sigma_{cls,Med}$23	-31890.0	-9547.3	216.0	-33.2

Pilastro: 117/217 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 18 ø 18 =45.80 [cm²] < 3ϕ18 x 4 V + 1ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./7.5 x 295.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
117	11	-6904.3	27053.8	-3788.8	19.42	1.00	0.80
217	17	-4911.8	-22341.5	2655.4	1.00	1.00	0.65

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	2.95	1.00	20790.5	21525.6	0.97	1.00	7335.3	24169.1	0.30	ø 8 2br.x4br./7.5	0.295

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
117	Ft. 19	-8682.1	2696.9	-1438.7	422.5
	$\sigma_{s,c}$19	-8682.1	2696.9	-1438.7	-410.1
	$\sigma_{cls,Max}$19	-8682.1	2696.9	-1438.7	-36.7
	$\sigma_{cls,Med}$19	-8682.1	2696.9	-1438.7	-12.2
217	Ft. 19	-7388.4	-3396.4	4570.6	1232.6
	$\sigma_{s,c}$19	-7388.4	-3396.4	4570.6	-798.8
	$\sigma_{cls,Max}$19	-7388.4	-3396.4	4570.6	-79.6
	$\sigma_{cls,Med}$19	-7388.4	-3396.4	4570.6	-29.2
	Combinazioni Frequenti				
117	Ft. 21	-7352.5	2728.1	-1063.3	381.3
	$\sigma_{s,c}$21	-7352.5	2728.1	-1063.3	-361.2
	$\sigma_{cls,Max}$21	-7352.5	2728.1	-1063.3	-32.0
	$\sigma_{cls,Med}$21	-7352.5	2728.1	-1063.3	-10.8
217	Ft. 21	-6058.7	-3437.8	3383.6	993.1
	$\sigma_{s,c}$21	-6058.7	-3437.8	3383.6	-670.8
	$\sigma_{cls,Max}$21	-6058.7	-3437.8	3383.6	-65.4
	$\sigma_{cls,Med}$21	-6058.7	-3437.8	3383.6	-22.7
	Combinazioni Quasi Permanenti				
117	Ft. 23	-6829.7	2740.0	-916.0	367.1
	$\sigma_{s,c}$23	-6829.7	2740.0	-916.0	-341.5
	$\sigma_{cls,Max}$23	-6829.7	2740.0	-916.0	-30.1
	$\sigma_{cls,Med}$23	-6829.7	2740.0	-916.0	-10.4
217	Ft. 23	-5535.9	-3453.3	2918.5	900.9
	$\sigma_{s,c}$23	-5535.9	-3453.3	2918.5	-619.8
	$\sigma_{cls,Max}$23	-5535.9	-3453.3	2918.5	-59.8
	$\sigma_{cls,Med}$23	-5535.9	-3453.3	2918.5	-20.3

Pilastro: 18/118 / L 3.25[m] / Sezione 1 B 30 H 50 [cm]

Af: 6 ø 18 =15.27 [cm²] < 1ϕ18 x 4 V + 0ϕ18 x 2 B + 1ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 54.2 - ø 8 2br.x4br./20.0 x 216.7 - ø 8 2br.x4br./12.5 x 54.2

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
18	16	-5529.3	315.0	867.4	1.00	1.00	0.07
118	16	-4123.1	-261.4	817.7	1.00	1.00	0.07

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.79	1.00	497.5	12915.4	0.04	1.00	53.1	14501.5	0.00	ø 8 2br.x4br./12.5	0.177
0.79	2.96	1.00	497.5	8072.1	0.06	1.00	53.1	9063.4	0.01	ø 8 2br.x4br./20.0	0.111
2.96	3.50	1.00	497.5	12915.4	0.04	1.00	53.1	14501.5	0.00	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
18	Ft. 19	-5696.6	135.1	597.4	75.0
	$\sigma_{s,c}$19	-5696.6	135.1	597.4	-140.4
	$\sigma_{cls,Max}$19	-5696.6	135.1	597.4	-12.4
	$\sigma_{cls,Med}$19	-5696.6	135.1	597.4	-5.6
118	Ft. 20	-4004.5	-113.5	527.6	103.7
	$\sigma_{s,c}$19	-4290.3	-114.0	549.7	-123.5
	$\sigma_{cls,Max}$19	-4290.3	-114.0	549.7	-11.4
	$\sigma_{cls,Med}$19	-4290.3	-114.0	549.7	-5.1
Combinazioni Frequenti					
18	Ft. 22	-5018.0	133.3	543.9	75.3
	$\sigma_{s,c}$21	-5208.5	133.8	559.1	-131.7
	$\sigma_{cls,Max}$21	-5208.5	133.8	559.1	-11.7
	$\sigma_{cls,Med}$21	-5208.5	133.8	559.1	-5.2
118	Ft. 22	-3611.7	-112.9	497.8	106.1
	$\sigma_{s,c}$21	-3802.3	-113.2	512.5	-115.1
	$\sigma_{cls,Max}$21	-3802.3	-113.2	512.5	-10.8
	$\sigma_{cls,Med}$21	-3802.3	-113.2	512.5	-4.8
Combinazioni Quasi Permanenti					
18	Ft. 23	-5015.4	133.3	543.9	75.3
	$\sigma_{s,c}$23	-5015.4	133.3	543.9	-128.3
	$\sigma_{cls,Max}$23	-5015.4	133.3	543.9	-11.4
	$\sigma_{cls,Med}$23	-5015.4	133.3	543.9	-5.1
118	Ft. 23	-3609.1	-112.9	497.7	106.1
	$\sigma_{s,c}$23	-3609.1	-112.9	497.7	-111.7
	$\sigma_{cls,Max}$23	-3609.1	-112.9	497.7	-10.5
	$\sigma_{cls,Med}$23	-3609.1	-112.9	497.7	-4.7

Pilastro: 118/218 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 6 ø 18 =15.27 [cm²] < 1ϕ18 x 4 V + 0ϕ18 x 2 B + 1ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 295.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
118	17	-9634.1	10434.0	-3333.8	1.00	1.00	0.82
218	17	-8340.4	-8948.1	-4.9	1.00	1.00	0.58

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	2.95	1.00	10811.3	12915.4	0.84	1.00	4689.9	14501.5	0.32	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
118	Ft. 20	-11532.5	1318.0	-488.2	100.4
	$\sigma_{s,c}$19	-12410.0	1342.9	-505.6	-289.9
	$\sigma_{cls,Max}$19	-12410.0	1342.9	-505.6	-23.3
	$\sigma_{cls,Med}$19	-12410.0	1342.9	-505.6	-9.0
218	Ft. 20	-10238.7	-1303.7	259.9	76.3
	$\sigma_{s,c}$19	-11116.3	-1342.3	255.8	-245.4
	$\sigma_{cls,Max}$19	-11116.3	-1342.3	255.8	-19.3
	$\sigma_{cls,Med}$19	-11116.3	-1342.3	255.8	-8.1
Combinazioni Frequenti					
118	Ft. 22	-10361.1	1275.1	-463.5	112.6
	$\sigma_{s,c}$21	-10946.2	1291.7	-475.1	-273.3
	$\sigma_{cls,Max}$21	-10946.2	1291.7	-475.1	-22.1
	$\sigma_{cls,Med}$21	-10946.2	1291.7	-475.1	-8.4
218	Ft. 22	-9067.4	-1242.6	252.9	89.4
	$\sigma_{s,c}$21	-9652.4	-1268.4	250.1	-229.7
	$\sigma_{cls,Max}$21	-9652.4	-1268.4	250.1	-18.2
	$\sigma_{cls,Med}$21	-9652.4	-1268.4	250.1	-7.5
Combinazioni Quasi Permanenti					
118	Ft. 23	-10360.8	1273.0	-463.2	112.1
	$\sigma_{s,c}$23	-10360.8	1273.0	-463.2	-267.2
	$\sigma_{cls,Max}$23	-10360.8	1273.0	-463.2	-21.7
	$\sigma_{cls,Med}$23	-10360.8	1273.0	-463.2	-8.2
218	Ft. 23	-9067.1	-1240.5	250.1	88.4
	$\sigma_{s,c}$23	-9067.1	-1240.5	250.1	-224.3
	$\sigma_{cls,Max}$23	-9067.1	-1240.5	250.1	-17.9
	$\sigma_{cls,Med}$23	-9067.1	-1240.5	250.1	-7.3

Pilastro: 22/122 / L 3.05[m] / Sezione 1 B 30 H 50 [cm]

Af: 6 ø 18 =15.27 [cm²] < 1ϕ18 x 4 V + 0ϕ18 x 2 B + 1ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.8 - ø 8 2br.x4br./20.0 x 203.3 - ø 8 2br.x4br./12.5 x 50.8

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
22	17	-2634.5	5759.3	10.3	1.00	4.02	0.42
122	17	-1228.3	5135.1	10.3	1.00	1.00	0.39

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.76	1.00	499.4	12915.4	0.04	1.00	66.1	14501.5	0.00	ø 8 2br.x4br./12.5	0.177
0.76	2.79	1.00	499.4	8072.1	0.06	1.00	66.1	9063.4	0.01	ø 8 2br.x4br./20.0	0.111
2.79	3.30	1.00	499.4	12915.4	0.04	1.00	66.1	14501.5	0.00	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
22	Ft. 19	-2881.3	3391.1	-0.1	1177.6
	$\sigma_{s,c}$19	-2881.3	3391.1	-0.1	-402.3
	$\sigma_{cls,Max}$19	-2881.3	3391.1	-0.1	-39.0
	$\sigma_{cls,Med}$19	-2881.3	3391.1	-0.1	-19.5
122	Ft. 19	-1475.1	3080.9	17.0	1154.1
	$\sigma_{s,c}$19	-1475.1	3080.9	17.0	-359.2
	$\sigma_{cls,Max}$19	-1475.1	3080.9	17.0	-35.7
	$\sigma_{cls,Med}$19	-1475.1	3080.9	17.0	-17.6
Combinazioni Frequenti					
22	Ft. 21	-2644.9	3193.8	-1.5	1114.2
	$\sigma_{s,c}$21	-2644.9	3193.8	-1.5	-378.6
	$\sigma_{cls,Max}$21	-2644.9	3193.8	-1.5	-36.8
	$\sigma_{cls,Med}$21	-2644.9	3193.8	-1.5	-18.4
122	Ft. 21	-1238.6	2892.3	15.6	1093.7
	$\sigma_{s,c}$21	-1238.6	2892.3	15.6	-335.6
	$\sigma_{cls,Max}$21	-1238.6	2892.3	15.6	-33.5
	$\sigma_{cls,Med}$21	-1238.6	2892.3	15.6	-16.5
Combinazioni Quasi Permanenti					
22	Ft. 23	-2551.5	3115.6	-1.9	1089.1
	$\sigma_{s,c}$23	-2551.5	3115.6	-1.9	-369.2
	$\sigma_{cls,Max}$23	-2551.5	3115.6	-1.9	-35.9
	$\sigma_{cls,Med}$23	-2551.5	3115.6	-1.9	-17.9
122	Ft. 23	-1145.2	2817.4	15.0	1069.6
	$\sigma_{s,c}$23	-1145.2	2817.4	15.0	-326.3
	$\sigma_{cls,Max}$23	-1145.2	2817.4	15.0	-32.6
	$\sigma_{cls,Med}$23	-1145.2	2817.4	15.0	-16.1

Pilastro: 25/125 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 6 ø 18 =15.27 [cm²] < 1ϕ18 x 4 V + 0ϕ18 x 2 B + 1ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./20.0 x 200.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
25	18	-2262.0	11015.6	46.9	3.50	1.23	0.84
125	18	-855.7	11015.6	-46.9	3.80	1.00	0.86

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	244.0	12915.4	0.02	1.00	97.5	14501.5	0.01	ø 8 2br.x4br./12.5	0.177
0.75	2.75	1.00	244.0	8072.1	0.03	1.00	97.5	9063.4	0.01	ø 8 2br.x4br./20.0	0.111
2.75	3.25	1.00	244.0	12915.4	0.02	1.00	97.5	14501.5	0.01	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
25	Ft. 19	-3796.2	1953.7	20.6	539.8
	$\sigma_{s,c}$19	-3796.2	1953.7	20.6	-254.0
	$\sigma_{cls,Max}$19	-3796.2	1953.7	20.6	-23.1
	$\sigma_{cls,Med}$19	-3796.2	1953.7	20.6	-11.3
125	Ft. 19	-2390.0	1775.7	-35.0	565.4
	$\sigma_{s,c}$19	-2390.0	1775.7	-35.0	-227.2
	$\sigma_{cls,Max}$19	-2390.0	1775.7	-35.0	-21.4
	$\sigma_{cls,Med}$19	-2390.0	1775.7	-35.0	-10.3
Combinazioni Frequenti					
25	Ft. 21	-3400.6	1824.6	20.0	513.8
	$\sigma_{s,c}$21	-3400.6	1824.6	20.0	-236.4
	$\sigma_{cls,Max}$21	-3400.6	1824.6	20.0	-21.6
	$\sigma_{cls,Med}$21	-3400.6	1824.6	20.0	-10.6
125	Ft. 21	-1994.3	1644.0	-32.3	538.3
	$\sigma_{s,c}$21	-1994.3	1644.0	-32.3	-208.6
	$\sigma_{cls,Max}$21	-1994.3	1644.0	-32.3	-19.8
	$\sigma_{cls,Med}$21	-1994.3	1644.0	-32.3	-9.5
Combinazioni Quasi Permanenti					
25	Ft. 23	-3259.4	1774.4	19.7	502.9
	$\sigma_{s,c}$23	-3259.4	1774.4	19.7	-229.6
	$\sigma_{cls,Max}$23	-3259.4	1774.4	19.7	-21.0
	$\sigma_{cls,Med}$23	-3259.4	1774.4	19.7	-10.3
125	Ft. 23	-1853.2	1592.7	-31.3	526.9
	$\sigma_{s,c}$23	-1853.2	1592.7	-31.3	-201.4
	$\sigma_{cls,Max}$23	-1853.2	1592.7	-31.3	-19.2
	$\sigma_{cls,Med}$23	-1853.2	1592.7	-31.3	-9.2

Pilastro: 125/225 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 12 ø 18 =30.54 [cm²] < 2ϕ18 x 4 V + 0ϕ18 x 2 B + 2ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 295.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
125	16	-9620.2	15881.0	6476.6	24.56	1.00	0.82
225	18	-3816.2	-10952.8	-3970.7	1.00	1.00	0.55

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	2.95	1.00	12498.9	12915.4	0.97	1.00	9036.5	14501.5	0.62	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
125	Ft. 19	-12287.5	-5926.2	77.6	890.9
	$\sigma_{s,c}19$	-12287.5	-5926.2	77.6	-616.4
	$\sigma_{cls,Max}19$	-12287.5	-5926.2	77.6	-52.9
	$\sigma_{cls,Med}19$	-12287.5	-5926.2	77.6	-25.9
225	Ft. 20	-10310.8	-909.8	225.3	8.4
	$\sigma_{s,c}19$	-10993.8	-806.6	272.7	-167.3
	$\sigma_{cls,Max}19$	-10993.8	-806.6	272.7	-12.8
	$\sigma_{cls,Med}19$	-10993.8	-806.6	272.7	-5.8
Combinazioni Frequenti					
125	Ft. 21	-10069.2	-5564.6	164.7	898.7
	$\sigma_{s,c}21$	-10069.2	-5564.6	164.7	-584.5
	$\sigma_{cls,Max}21$	-10069.2	-5564.6	164.7	-50.8
	$\sigma_{cls,Med}21$	-10069.2	-5564.6	164.7	-24.1
225	Ft. 22	-8320.1	-1012.7	9.6	14.1
	$\sigma_{s,c}21$	-8775.5	-943.9	41.2	-138.3
	$\sigma_{cls,Max}21$	-8775.5	-943.9	41.2	-10.4
	$\sigma_{cls,Med}22$	-8320.1	-1012.7	9.6	-5.1
Combinazioni Quasi Permanenti					
125	Ft. 23	-9373.9	-5417.5	187.2	893.4
	$\sigma_{s,c}23$	-9373.9	-5417.5	187.2	-570.7
	$\sigma_{cls,Max}23$	-9373.9	-5417.5	187.2	-49.8
	$\sigma_{cls,Med}23$	-9373.9	-5417.5	187.2	-23.4
225	Ft. 23	-8080.2	-1005.0	-24.3	17.8
	$\sigma_{s,c}23$	-8080.2	-1005.0	-24.3	-137.2
	$\sigma_{cls,Max}23$	-8080.2	-1005.0	-24.3	-10.4
	$\sigma_{cls,Med}23$	-8080.2	-1005.0	-24.3	-5.1

Pilastro: 26/126 / L 3.00[m] / Sezione 3 B 30 H 30 [cm]

Af: 4 ø 18 + 4 ø 16 =18.22 [cm²] < 1ϕ18 x 4 V + 1ϕ16 x 2 B + 1ϕ16 x 2 H >
Staffe: ø 8/12.5 x 50.0 - ø 8/15.0 x 200.0 - ø 8/12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
26	18	-2074.0	6934.9	25.2	8.69	1.13	0.86
126	18	-1230.3	6934.9	-25.2	9.45	1.00	0.87

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	54.2	7250.7	0.01	1.00	49.3	7250.7	0.01	ø 8/12.5	0.171
0.75	2.75	1.00	54.2	6042.3	0.01	1.00	49.3	6042.3	0.01	ø 8/15.0	0.142
2.75	3.25	1.00	54.2	7250.7	0.01	1.00	49.3	7250.7	0.01	ø 8/12.5	0.171

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
26	Ft. 19	-2737.0	607.9	5.2	211.5
	$\sigma_{s,c}$19	-2737.0	607.9	5.2	-157.7
	$\sigma_{cls,Max}$19	-2737.0	607.9	5.2	-16.1
	$\sigma_{cls,Med}$19	-2737.0	607.9	5.2	-8.0
126	Ft. 19	-1893.2	574.5	-10.1	237.1
	$\sigma_{s,c}$19	-1893.2	574.5	-10.1	-141.6
	$\sigma_{cls,Max}$19	-1893.2	574.5	-10.1	-15.2
	$\sigma_{cls,Med}$19	-1893.2	574.5	-10.1	-7.5
Combinazioni Frequenti					
26	Ft. 21	-2484.7	560.2	6.6	197.1
	$\sigma_{s,c}$21	-2484.7	560.2	6.6	-145.1
	$\sigma_{cls,Max}$21	-2484.7	560.2	6.6	-14.9
	$\sigma_{cls,Med}$21	-2484.7	560.2	6.6	-7.3
126	Ft. 21	-1641.0	526.3	-10.6	222.5
	$\sigma_{s,c}$21	-1641.0	526.3	-10.6	-128.9
	$\sigma_{cls,Max}$21	-1641.0	526.3	-10.6	-13.9
	$\sigma_{cls,Med}$21	-1641.0	526.3	-10.6	-6.8
Combinazioni Quasi Permanenti					
26	Ft. 23	-2389.1	541.5	7.0	191.4
	$\sigma_{s,c}$23	-2389.1	541.5	7.0	-140.3
	$\sigma_{cls,Max}$23	-2389.1	541.5	7.0	-14.4
	$\sigma_{cls,Med}$23	-2389.1	541.5	7.0	-7.1
126	Ft. 23	-1545.4	507.4	-10.6	216.7
	$\sigma_{s,c}$23	-1545.4	507.4	-10.6	-123.9
	$\sigma_{cls,Max}$23	-1545.4	507.4	-10.6	-13.4
	$\sigma_{cls,Med}$23	-1545.4	507.4	-10.6	-6.6

Pilastro: 126/226 / L 2.95[m] / Sezione 3 B 30 H 30 [cm]

Af: 12 ø 16 =24.13 [cm²] < 2ϕ16 x 4 V + 1ϕ16 x 2 B + 1ϕ16 x 2 H >
Staffe: ø 8/10.0 x 295.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
126	18	-8567.8	9357.4	3547.3	123.59	1.00	0.98
226	16	-7426.0	10.2	-4533.9	1.00	1.00	0.37

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	2.95	1.00	3091.2	9063.4	0.34	1.00	7927.2	9063.4	0.87	ø 8/10.0	0.214

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
126	Ft. 19	-11483.7	-1529.4	244.6	322.9
	$\sigma_{s,c}19$	-11483.7	-1529.4	244.6	-466.4
	$\sigma_{cls,Max}19$	-11483.7	-1529.4	244.6	-42.7
	$\sigma_{cls,Med}19$	-11483.7	-1529.4	244.6	-18.9
226	Ft. 20	-10166.3	53.3	-237.7	-75.2
	$\sigma_{s,c}19$	-10707.4	67.7	-254.8	-177.9
	$\sigma_{cls,Max}19$	-10707.4	67.7	-254.8	-13.4
	$\sigma_{cls,Med}19$	-10707.4	67.7	-254.8	-8.5
	Combinazioni Frequenti				
126	Ft. 21	-10104.4	-1426.7	204.0	316.3
	$\sigma_{s,c}21$	-10104.4	-1426.7	204.0	-424.6
	$\sigma_{cls,Max}21$	-10104.4	-1426.7	204.0	-39.2
	$\sigma_{cls,Med}21$	-10104.4	-1426.7	204.0	-17.5
226	Ft. 22	-8967.4	36.0	-191.0	-71.0
	$\sigma_{s,c}21$	-9328.2	45.6	-202.4	-149.8
	$\sigma_{cls,Max}21$	-9328.2	45.6	-202.4	-11.1
	$\sigma_{cls,Med}21$	-9328.2	45.6	-202.4	-7.4
	Combinazioni Quasi Permanenti				
126	Ft. 23	-9637.6	-1385.8	190.4	311.6
	$\sigma_{s,c}23$	-9637.6	-1385.8	190.4	-409.2
	$\sigma_{cls,Max}23$	-9637.6	-1385.8	190.4	-37.9
	$\sigma_{cls,Med}23$	-9637.6	-1385.8	190.4	-17.0
226	Ft. 23	-8861.3	36.4	-185.7	-70.5
	$\sigma_{s,c}23$	-8861.3	36.4	-185.7	-140.2
	$\sigma_{cls,Max}23$	-8861.3	36.4	-185.7	-10.4
	$\sigma_{cls,Med}23$	-8861.3	36.4	-185.7	-7.0

Pilastro: 27/127 / L 3.00[m] / Sezione 3 B 30 H 30 [cm]

Af: 4 ø 18 + 4 ø 16 =18.22 [cm²] < 1ϕ18 x 4 V + 1ϕ16 x 2 B + 1ϕ16 x 2 H >
Staffe: ø 8/12.5 x 50.0 - ø 8/15.0 x 200.0 - ø 8/12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
27	18	-2032.7	5305.2	10.8	7.17	1.00	0.65
127	18	-1189.0	5305.2	-6.1	7.82	1.00	0.66

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	51.8	7250.7	0.01	1.00	39.7	7250.7	0.01	ø 8/12.5	0.171
0.75	2.75	1.00	51.8	6042.3	0.01	1.00	39.7	6042.3	0.01	ø 8/15.0	0.142
2.75	3.25	1.00	51.8	7250.7	0.01	1.00	39.7	7250.7	0.01	ø 8/12.5	0.171

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
27	Ft. 19	-2757.7	605.4	8.8	209.8
	$\sigma_{s,c}$19	-2757.7	605.4	8.8	-158.2
	$\sigma_{cls,Max}$19	-2757.7	605.4	8.8	-16.1
	$\sigma_{cls,Med}$19	-2757.7	605.4	8.8	-7.9
127	Ft. 19	-1914.0	566.9	-3.8	230.2
	$\sigma_{s,c}$19	-1914.0	566.9	-3.8	-139.1
	$\sigma_{cls,Max}$19	-1914.0	566.9	-3.8	-14.8
	$\sigma_{cls,Med}$19	-1914.0	566.9	-3.8	-7.4
Combinazioni Frequenti					
27	Ft. 21	-2484.7	554.1	9.1	194.3
	$\sigma_{s,c}$21	-2484.7	554.1	9.1	-144.6
	$\sigma_{cls,Max}$21	-2484.7	554.1	9.1	-14.8
	$\sigma_{cls,Med}$21	-2484.7	554.1	9.1	-7.3
127	Ft. 21	-1641.0	516.7	-4.8	215.3
	$\sigma_{s,c}$21	-1641.0	516.7	-4.8	-125.4
	$\sigma_{cls,Max}$21	-1641.0	516.7	-4.8	-13.5
	$\sigma_{cls,Med}$21	-1641.0	516.7	-4.8	-6.7
Combinazioni Quasi Permanenti					
27	Ft. 23	-2383.4	534.0	9.2	188.0
	$\sigma_{s,c}$23	-2383.4	534.0	9.2	-139.4
	$\sigma_{cls,Max}$23	-2383.4	534.0	9.2	-14.3
	$\sigma_{cls,Med}$23	-2383.4	534.0	9.2	-7.0
127	Ft. 23	-1539.7	497.0	-5.2	209.2
	$\sigma_{s,c}$23	-1539.7	497.0	-5.2	-120.1
	$\sigma_{cls,Max}$23	-1539.7	497.0	-5.2	-13.0
	$\sigma_{cls,Med}$23	-1539.7	497.0	-5.2	-6.4

Pilastro: 127/227 / L 2.95[m] / Sezione 3 B 30 H 30 [cm]

Af: 4 ø 18 + 4 ø 16 =18.22 [cm²] < 1ϕ18 x 4 V + 1ϕ16 x 2 B + 1ϕ16 x 2 H >
Staffe: ø 8/12.5 x 295.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
127	16	-10728.4	-5766.5	4487.7	13.91	1.00	0.90
227	16	-9952.1	-119.5	-4360.9	1.00	1.00	0.45

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	2.95	1.00	2653.2	7250.7	0.37	1.00	6565.2	7250.7	0.91	ø 8/12.5	0.171

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
127	Ft. 19	-12694.2	-1425.7	252.9	281.3
	$\sigma_{s,c}$19	-12694.2	-1425.7	252.9	-493.8
	$\sigma_{cls,Max}$19	-12694.2	-1425.7	252.9	-44.7
	$\sigma_{cls,Med}$19	-12694.2	-1425.7	252.9	-19.5
227	Ft. 20	-11213.0	198.5	-267.6	-63.5
	$\sigma_{s,c}$19	-11917.9	225.1	-289.5	-240.5
	$\sigma_{cls,Max}$19	-11917.9	225.1	-289.5	-18.7
	$\sigma_{cls,Med}$19	-11917.9	225.1	-289.5	-10.2
	Combinazioni Frequenti				
127	Ft. 21	-10903.7	-1312.6	221.4	286.8
	$\sigma_{s,c}$21	-10903.7	-1312.6	221.4	-445.4
	$\sigma_{cls,Max}$21	-10903.7	-1312.6	221.4	-40.8
	$\sigma_{cls,Med}$21	-10903.7	-1312.6	221.4	-17.9
227	Ft. 22	-9657.5	163.9	-238.6	-54.6
	$\sigma_{s,c}$21	-10127.4	181.6	-253.2	-203.9
	$\sigma_{cls,Max}$21	-10127.4	181.6	-253.2	-15.9
	$\sigma_{cls,Med}$21	-10127.4	181.6	-253.2	-8.6
	Combinazioni Quasi Permanenti				
127	Ft. 23	-10296.9	-1267.7	209.4	285.3
	$\sigma_{s,c}$23	-10296.9	-1267.7	209.4	-427.2
	$\sigma_{cls,Max}$23	-10296.9	-1267.7	209.4	-39.3
	$\sigma_{cls,Med}$23	-10296.9	-1267.7	209.4	-17.2
227	Ft. 23	-9520.7	164.1	-238.6	-52.8
	$\sigma_{s,c}$23	-9520.7	164.1	-238.6	-190.7
	$\sigma_{cls,Max}$23	-9520.7	164.1	-238.6	-14.8
	$\sigma_{cls,Med}$23	-9520.7	164.1	-238.6	-8.1

Pilastro: 28/128 / L 3.00[m] / Sezione 1 B 30 H 50 [cm]

Af: 6 ø 18 =15.27 [cm²] < 1ϕ18 x 4 V + 0ϕ18 x 2 B + 1ϕ18 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./20.0 x 200.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
28	18	-3281.3	8126.1	-16.1	3.04	1.66	0.59
128	18	-1875.1	8126.1	16.1	3.15	1.00	0.62

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.25	0.75	1.00	94.2	12915.4	0.01	1.00	68.8	14501.5	0.00	ø 8 2br.x4br./12.5	0.177
0.75	2.75	1.00	94.2	8072.1	0.01	1.00	68.8	9063.4	0.01	ø 8 2br.x4br./20.0	0.111
2.75	3.25	1.00	94.2	12915.4	0.01	1.00	68.8	14501.5	0.00	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
28	Ft. 19	-5142.2	2322.0	-13.2	598.2
	$\sigma_{s,c}$19	-5142.2	2322.0	-13.2	-303.2
	$\sigma_{cls,Max}$19	-5142.2	2322.0	-13.2	-27.2
	$\sigma_{cls,Med}$19	-5142.2	2322.0	-13.2	-13.5
128	Ft. 19	-3735.9	2286.1	19.4	677.1
	$\sigma_{s,c}$19	-3735.9	2286.1	19.4	-291.0
	$\sigma_{cls,Max}$19	-3735.9	2286.1	19.4	-26.9
	$\sigma_{cls,Med}$19	-3735.9	2286.1	19.4	-13.2
Combinazioni Frequenti					
28	Ft. 21	-4588.6	2078.6	-7.2	535.3
	$\sigma_{s,c}$21	-4588.6	2078.6	-7.2	-270.3
	$\sigma_{cls,Max}$21	-4588.6	2078.6	-7.2	-24.3
	$\sigma_{cls,Med}$21	-4588.6	2078.6	-7.2	-12.0
128	Ft. 21	-3182.3	2024.2	13.1	606.9
	$\sigma_{s,c}$21	-3182.3	2024.2	13.1	-255.8
	$\sigma_{cls,Max}$21	-3182.3	2024.2	13.1	-23.8
	$\sigma_{cls,Med}$21	-3182.3	2024.2	13.1	-11.7
Combinazioni Quasi Permanenti					
28	Ft. 23	-4381.2	1983.0	-5.0	510.0
	$\sigma_{s,c}$23	-4381.2	1983.0	-5.0	-257.4
	$\sigma_{cls,Max}$23	-4381.2	1983.0	-5.0	-23.1
	$\sigma_{cls,Med}$23	-4381.2	1983.0	-5.0	-11.5
128	Ft. 23	-2975.0	1921.1	10.8	578.6
	$\sigma_{s,c}$23	-2975.0	1921.1	10.8	-242.0
	$\sigma_{cls,Max}$23	-2975.0	1921.1	10.8	-22.5
	$\sigma_{cls,Med}$23	-2975.0	1921.1	10.8	-11.1

Pilastro: 128/228 / L 2.95[m] / Sezione 1 B 30 H 50 [cm]

Af: 4 ø 18 + 4 ø 16 =18.22 [cm²] < 1ϕ18 x 4 V + 0ϕ16 x 2 B + 2ϕ16 x 2 H >
Staffe: ø 8 2br.x4br./12.5 x 50.0 - ø 8 2br.x4br./15.0 x 195.0 - ø 8 2br.x4br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
128	11	-13107.5	-10153.3	-6818.1	1.00	1.00	0.92
228	11	-11813.8	6472.5	6557.3	1.00	1.00	0.74

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.50	1.00	6750.1	12915.4	0.52	1.00	7082.6	14501.5	0.49	ø 8 2br.x4br./12.5	0.177
0.50	2.45	1.00	6750.1	10762.8	0.63	1.00	7082.6	12084.6	0.59	ø 8 2br.x4br./15.0	0.148
2.45	2.95	1.00	6750.1	12915.4	0.52	1.00	7082.6	14501.5	0.49	ø 8 2br.x4br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
	Combinazioni Rare				
128	Ft. 19	-15530.2	-6313.0	144.6	1419.1
	$\sigma_{s,c}$19	-15530.2	-6313.0	144.6	-837.3
	$\sigma_{cls,Max}$19	-15530.2	-6313.0	144.6	-73.7
	$\sigma_{cls,Med}$19	-15530.2	-6313.0	144.6	-35.4
228	Ft. 19	-14236.4	3650.3	53.5	549.0
	$\sigma_{s,c}$19	-14236.4	3650.3	53.5	-500.8
	$\sigma_{cls,Max}$19	-14236.4	3650.3	53.5	-41.6
	$\sigma_{cls,Med}$19	-14236.4	3650.3	53.5	-20.3
	Combinazioni Frequenti				
128	Ft. 21	-13600.9	-5520.1	148.0	1244.4
	$\sigma_{s,c}$21	-13600.9	-5520.1	148.0	-736.7
	$\sigma_{cls,Max}$21	-13600.9	-5520.1	148.0	-64.9
	$\sigma_{cls,Med}$21	-13600.9	-5520.1	148.0	-30.9
228	Ft. 21	-12307.1	2900.9	4.5	384.9
	$\sigma_{s,c}$21	-12307.1	2900.9	4.5	-394.6
	$\sigma_{cls,Max}$21	-12307.1	2900.9	4.5	-32.3
	$\sigma_{cls,Med}$21	-12307.1	2900.9	4.5	-16.1
	Combinazioni Quasi Permanenti				
128	Ft. 23	-12945.8	-5203.3	153.9	1169.3
	$\sigma_{s,c}$23	-12945.8	-5203.3	153.9	-698.1
	$\sigma_{cls,Max}$23	-12945.8	-5203.3	153.9	-61.4
	$\sigma_{cls,Med}$23	-12945.8	-5203.3	153.9	-29.2
228	Ft. 23	-11652.0	2599.1	-22.4	321.5
	$\sigma_{s,c}$23	-11652.0	2599.1	-22.4	-359.0
	$\sigma_{cls,Max}$23	-11652.0	2599.1	-22.4	-29.2
	$\sigma_{cls,Med}$23	-11652.0	2599.1	-22.4	-14.4

Pilastro: 29/129 / L 3.50[m] / Sezione 2 B 50 H 30 [cm]

Af: 6 ø 18 =15.27 [cm²] < 1ϕ18 x 4 V + 1ϕ18 x 2 B + 0ϕ18 x 2 H >
Staffe: ø 8 4br.x2br./12.5 x 58.3 - ø 8 4br.x2br./20.0 x 233.3 - ø 8 4br.x2br./12.5 x 58.3

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
29	11	-3825.5	-20.6	164.6	1.00	5.66	0.02
129	16	532.2	5.0	169.5	1.00	1.00	0.02

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.58	1.00	30.3	14501.5	0.00	1.00	192.9	12915.4	0.01	ø 8 4br.x2br./12.5	0.177
0.58	2.92	1.00	30.3	9063.4	0.00	1.00	192.9	8072.1	0.02	ø 8 4br.x2br./20.0	0.111
2.92	3.50	1.00	30.3	14501.5	0.00	1.00	192.9	12915.4	0.01	ø 8 4br.x2br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
29	Ft. 20	-2522.4	6.3	-26.8	-19.0
	$\sigma_{s,c}$19	-2613.6	7.3	-27.1	-25.7
	$\sigma_{cls,Max}$19	-2613.6	7.3	-27.1	-1.8
	$\sigma_{cls,Med}$19	-2613.6	7.3	-27.1	-1.5
129	Ft. 20	-1116.1	-2.7	-3.7	-9.1
	$\sigma_{s,c}$19	-1207.4	-3.2	-7.2	-11.4
	$\sigma_{cls,Max}$19	-1207.4	-3.2	-7.2	-0.8
	$\sigma_{cls,Med}$19	-1207.4	-3.2	-7.2	-0.7
Combinazioni Frequenti					
29	Ft. 22	-2348.7	4.6	-25.8	-17.8
	$\sigma_{s,c}$21	-2409.5	5.3	-26.1	-23.6
	$\sigma_{cls,Max}$21	-2409.5	5.3	-26.1	-1.6
	$\sigma_{cls,Med}$21	-2409.5	5.3	-26.1	-1.4
129	Ft. 22	-942.5	-1.6	2.6	-7.8
	$\sigma_{s,c}$21	-1003.3	-1.9	0.3	-8.9
	$\sigma_{cls,Max}$21	-1003.3	-1.9	0.3	-0.6
	$\sigma_{cls,Med}$21	-1003.3	-1.9	0.3	-0.6
Combinazioni Quasi Permanenti					
29	Ft. 23	-2337.2	4.6	-25.7	-17.7
	$\sigma_{s,c}$23	-2337.2	4.6	-25.7	-22.9
	$\sigma_{cls,Max}$23	-2337.2	4.6	-25.7	-1.6
	$\sigma_{cls,Med}$23	-2337.2	4.6	-25.7	-1.4
129	Ft. 23	-930.9	-1.5	2.9	-7.7
	$\sigma_{s,c}$23	-930.9	-1.5	2.9	-8.5
	$\sigma_{cls,Max}$23	-930.9	-1.5	2.9	-0.6
	$\sigma_{cls,Med}$23	-930.9	-1.5	2.9	-0.5

Pilastro: 129/229 / L 2.95[m] / Sezione 2 B 50 H 30 [cm]

Af: 4 ø 18 + 4 ø 16 =18.22 [cm²] < 1ϕ18 x 4 V + 2ϕ16 x 2 B + 0ϕ16 x 2 H >
Staffe: ø 8 4br.x2br./12.5 x 50.0 - ø 8 4br.x2br./15.0 x 195.0 - ø 8 4br.x2br./12.5 x 50.0

Verifiche a Presso-Flessione S.L.U.

Nodo	Comb	N	M_{12}	M_{13}	α_{12}	α_{13}	Sd/Sr
129	16	-3355.3	-984.2	13689.5	1.00	1.00	0.90
229	13	-7064.5	2673.3	6156.0	1.00	1.00	0.46

Verifiche a Taglio

Da [m]	A [m]	$cotg(\theta)_{12}$	V_{d12} [kg]	V_{Rd12} [kg]	S/R_{12} [kg]	$cotg(\theta)_{13}$	V_{d13} [kg]	V_{Rd13} [kg]	S/R_{13} [kg]	Staffe	ω_{wd}
0.00	0.50	1.00	6231.0	14501.5	0.43	1.00	9695.9	12915.4	0.75	ø 8 4br.x2br./12.5	0.177
0.50	2.45	1.00	6231.0	12084.6	0.52	1.00	9695.9	10762.8	0.90	ø 8 4br.x2br./15.0	0.148
2.45	2.95	1.00	6231.0	14501.5	0.43	1.00	9695.9	12915.4	0.75	ø 8 4br.x2br./12.5	0.177

Verifiche a Presso-Flessione S.L.E.

Nodo	Combinazione	N [kg]	M_{12} [kgm]	M_{13} [kgm]	σ [kg/cm²]
Combinazioni Rare					
129	Ft. 19	-6883.7	-141.3	209.7	-26.1
	$\sigma_{s,c}19$	-6883.7	-141.3	209.7	-90.4
	$\sigma_{cls,Max}19$	-6883.7	-141.3	209.7	-6.8
	$\sigma_{cls,Med}19$	-6883.7	-141.3	209.7	-3.9
229	Ft. 19	-5589.9	763.1	670.6	226.6
	$\sigma_{s,c}19$	-5589.9	763.1	670.6	-228.8
	$\sigma_{cls,Max}19$	-5589.9	763.1	670.6	-20.8
	$\sigma_{cls,Med}19$	-5589.9	763.1	670.6	-7.4
Combinazioni Frequenti					
129	Ft. 21	-6237.3	-75.7	137.2	-33.5
	$\sigma_{s,c}21$	-6237.3	-75.7	137.2	-72.0
	$\sigma_{cls,Max}21$	-6237.3	-75.7	137.2	-5.2
	$\sigma_{cls,Med}21$	-6237.3	-75.7	137.2	-3.5
229	Ft. 21	-4943.5	617.7	664.4	191.0
	$\sigma_{s,c}21$	-4943.5	617.7	664.4	-201.9
	$\sigma_{cls,Max}21$	-4943.5	617.7	664.4	-18.1
	$\sigma_{cls,Med}21$	-4943.5	617.7	664.4	-6.2
Combinazioni Quasi Permanenti					
129	Ft. 23	-6026.8	-48.6	94.3	-38.1
	$\sigma_{s,c}23$	-6026.8	-48.6	94.3	-63.8
	$\sigma_{cls,Max}23$	-6026.8	-48.6	94.3	-4.5
	$\sigma_{cls,Med}23$	-6026.8	-48.6	94.3	-3.4
229	Ft. 23	-4733.0	558.7	697.3	183.1
	$\sigma_{s,c}23$	-4733.0	558.7	697.3	-195.5
	$\sigma_{cls,Max}23$	-4733.0	558.7	697.3	-17.4
	$\sigma_{cls,Med}23$	-4733.0	558.7	697.3	-5.9

- En.Ex.Sys. WinStrand
- Verifiche pilastri

Verifiche resistenza dei nodi

Per le verifiche di fessurazione diagonale usa le formule TU 2018 7.4.11-7.4.12

Nodo	Pilastro di riferimento	Ingombro nodo		Materiali		Staffe	Verifica compressione diagonale															Verifica fessurazione diagonale												
		B [cm]	H [cm]	f_{ck}	Acciaio		$v_{d,x}$	$\alpha_{j,x}$	η_x	$b_{j,x}$ [cm]	$h_{j,x}$ [cm]	$V_{jbd,Edx}$ [kg]	$V_{jbd,Rdx}$ [kg]	$v_{d,y}$	$\alpha_{j,y}$	η_y	$b_{j,y}$ [cm]	$h_{j,y}$ [cm]	$V_{jbd,Edy}$ [kg]	$V_{jbd,Rdy}$ [kg]	v	b_x [cm]	h_x [cm]	$As_{1,x}$ [cm²]	$As_{2,x}$ [cm²]	$V_{jbd,Edx}$ [kg]	$V_{jbd,Rdx}$ [kg]	b_y [cm]	h_y [cm]	$As_{1,y}$ [cm²]	$As_{2,y}$ [cm²]	$V_{jbd,Edy}$ [kg]	$V_{jbd,Rdy}$ [kg]
103	3 103	50	60	C25/30	B 450 C	ø 10/7.5	0.081	0.48	0.432	85	41	190546.8	37215.7								0.04434	85	16	9.24		38345.4	24586.1						
104	4 104	50	60	C25/30	B 450 C	ø 10/7.5								0.082	0.48	0.432	80	51	223066.2	39363.5	0.04953							80	16	9.24		38180.4	24586.1
107	7 107	30	40	C25/30	B 450 C	ø 10/7.5	0.172	0.48	0.432	55	21	54301.6	57842.6								0.03207	55	16	13.64		57199.0	12293.1						
108	8 108	40	40	C25/30	B 450 C	ø 10/7.5	0.123	0.60	0.540	60	31	124255.2	157353.2								0.17849	60	16	16.93		135388.0	18439.6						
109	9 109	40	40	C25/30	B 450 C	ø 10/7.5	0.137	0.60	0.540	60	31	122100.4	157691.2								0.19688	60	16	16.93		133064.2	18439.6						
110	10 110	30	40	C25/30	B 450 C	ø 10/7.5	0.211	0.48	0.432	55	21	50128.1	47176.9								0.02747	55	16	11.16		46975.9	12293.1						
114	14 114	30	40	C25/30	B 450 C	ø 10/7.5	0.176	0.48	0.432	55	21	53877.1	25869.1	0.176	0.60	0.540	30	31	58024.5	66324.7	0.23318	55	16	6.20		21706.4	12293.1	30	36	6.64		55598.6	24586.1
115	15 115	40	40	C25/30	B 450 C	ø 10/7.5	0.145	0.60	0.540	60	31	120929.1	145314.7								0.19979	60	16	15.39		122472.4	18439.6						
116	16 116	40	40	C25/30	B 450 C	ø 10/7.5	0.130	0.60	0.540	60	31	123267.5	164127.5								0.19144	60	16	16.93		139363.4	18439.6						
117	17 117	30	50	C25/30	B 450 C	ø 10/7.5	0.167	0.48	0.432	65	21	64776.4	47323.0	0.167	0.48	0.432	30	41	58634.8	17503.2	0.08982	65	16	11.16		44580.3	18439.6	30	36	4.15		16585.4	30732.6
118	18 118	50	30	C25/30	B 450 C	ø 10/7.5	0.015	0.48	0.432	55	41	134969.6	27487.3	0.011	0.48	0.432	45	21	56568.6	13503.4	0.11007	55	36	6.42		25219.2	24586.1	45	36	3.15		12360.0	24586.1
119	19 119	50	30	C25/30	B 450 C	ø 10/7.5	0.095	0.60	0.540	55	41	155838.3	114699.8								0.11552	55	36	11.38		105018.6	24586.1						
120	20 120	60	50	C25/30	B 450 C	ø 10/7.5	0.085	0.60	0.540	80	51	284281.1	103824.6								0.10496	80	36	12.32		97113.8	49172.2						
121	21 121	50	60	C25/30	B 450 C	ø 10/7.5	0.052	0.48	0.432	85	41	198088.9	42614.3	0.052	0.48	0.432	50	51	145223.1	18399.9	0.12402	85	16	9.92		38458.6	24586.1	50	36	4.44		17229.9	49172.2
203	103 203	50	60	C25/30	B 450 C	ø 10/7.5	0.046	0.48	0.432	85	41	199622.4	72865.2	0.050	0.48	0.432	50	51	145620.3	36734.6	0.09110	85	16	16.93		67573.5	24586.1	50	36	8.60		34337.6	49172.2
204	104 204	50	60	C25/30	B 450 C	ø 10/7.5	0.053	0.60	0.540	85	41	250734.0	132470.2								0.06650	85	16	18.47		125469.5	24586.1						
205	105 205	30	75	C25/30	B 450 C	ø 10/7.5	0.033	0.60	0.540	85	21	131108.3	84481.4								0.05135	85	36	10.05		81042.9	36879.2						
206	106 206	30	75	C25/30	B 450 C	ø 10/7.5	0.034	0.48	0.432	85	21	103819.9	49303.9	0.029	0.48	0.432	30	66	116756.8	37716.3	0.08397	85	16	11.72		47052.5	24586.1	30	36	8.89		35685.7	18439.6
207	107 207	30	40	C25/30	B 450 C	ø 10/7.5	0.057	0.48	0.432	55	21	65244.1	55737.5	0.077	0.60	0.540	30	31	65471.7	82685.1	0.21363	55	16	12.96		46249.6	12293.1	30	36	7.39		69426.8	24586.1
208	108 208	40	40	C25/30	B 450 C	ø 10/7.5	0.054	0.60	0.540	60	31	134095.4	158402.4								0.07950	60	16	18.47		148908.7	18439.6						
209	109 209	40	40	C25/30	B 450 C	ø 10/7.5	0.073	0.60	0.540	60	31	131532.5	158538.3								0.10262	60	16	18.47		145967.9	18439.6						
210	110 210	30	40	C25/30	B 450 C	ø 10/7.5	0.079	0.48	0.432	55	21	63340.5	44469.8	0.078	0.60	0.540	30	31	65393.7	92221.7	0.25519	55	16	10.48		35891.4	12293.1	30	36	9.58		74143.1	24586.1
211	111 211	30	50	C25/30	B 450 C	ø 10/7.5								0.031	0.60	0.540	55	41	166754.1	83707.7	0.03712							55	36	10.44		81662.4	24586.1
214	114 214	30	40	C25/30	B 450 C	ø 10/7.5	0.063	0.48	0.432	55	21	64682.3	37753.9	0.061	0.60	0.540	50	31	111001.2	64953.6	0.17065	55	16	8.94		33220.0	12293.1	50	16	7.56		56160.3	12293.1
215	115 215	40	40	C25/30	B 450 C	ø 10/7.5	0.068	0.60	0.540	60	31	132179.1	139039.7								0.08870	60	16	15.39		129271.7	18439.6						

216	116 216	40	40	C25/30	B 450 C	ø 10/7.5	0.067	0.60	0.540	60	31	132350.9	138721.9								0.09891	60	16	15.39		128135.0	18439.6						
217	117 217	30	50	C25/30	B 450 C	ø 10/7.5	0.055	0.48	0.432	65	21	77314.2	43775.6	0.068	0.60	0.540	30	41	87599.9	96203.6	0.20379	65	16	10.18		36671.7	18439.6	30	36	10.35		80737.4	30732.6
218	118 218	50	30	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	55	41	137365.1	27684.9	0.000	0.48	0.432	45	21	57296.7	18071.3	0.04605	55	36	6.43		26665.1	24586.1	45	36	4.20		17405.6	24586.1
219	119 219	50	30	C25/30	B 450 C	ø 10/7.5	0.048	0.60	0.540	55	41	163891.5	118178.9								0.06450	55	36	11.46		112445.9	24586.1						
220	120 220	60	50	C25/30	B 450 C	ø 10/7.5	0.051	0.60	0.540	80	51	294730.6	104539.1								0.06713	80	36	15.74		99502.8	49172.2						
221	121 221	50	60	C25/30	B 450 C	ø 10/7.5	0.043	0.48	0.432	85	41	200338.3	51589.3	0.049	0.48	0.432	50	51	145869.2	39913.9	0.08169	85	16	12.02		48343.9	24586.1	50	36	9.52		38309.3	49172.2
303	203 303	30	50	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	45	21	57296.7	19877.9	0.000	0.48	0.432	30	41	74926.4	22147.9	0.04981	45	36	4.62		19085.8	18439.6	30	36	5.15		21265.4	18439.6
304	204 304	50	30	C25/30	B 450 C	ø 10/7.5	0.000	0.60	0.540	30	41	93198.9	79511.5								0.00000	30	36	9.24		79511.5	18439.6						
305	205 305	30	75	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	85	21	107186.4	32055.3	0.000	0.48	0.432	65	66	261018.2	33129.8	0.04744	85	36	7.45		30838.8	61465.3	65	16	7.70		31872.6	18439.6
306	206 306	30	75	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	85	21	108227.0	32055.3	0.000	0.48	0.432	30	66	120837.2	33129.8	0.03415	85	16	7.45		31179.5	24586.1	30	36	7.70		32224.6	18439.6
307	207 307	30	40	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	55	21	70029.3	39755.7	0.000	0.60	0.540	30	31	70702.6	67591.6	0.09019	55	16	9.24		36887.3	12293.1	30	36	6.47		62714.9	24586.1
308	208 308	40	40	C25/30	B 450 C	ø 10/7.5	0.000	0.60	0.540	60	31	141405.2	145771.0								0.00000	60	16	16.93		145771.0	18439.6						
309	209 309	40	40	C25/30	B 450 C	ø 10/7.5	0.000	0.60	0.540	60	31	141405.2	145771.0	0.000	0.60	0.540	60	31	141405.2	106015.3	0.00000	60	16	16.93	16.93	145771.0	18439.6	60	16	12.32	12.32	106015.3	18439.6
310	210 310	30	40	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	55	21	70029.3	32055.3	0.000	0.60	0.540	30	31	70702.6	67877.9	0.09690	55	16	7.45		29570.4	12293.1	30	36	6.53		62616.0	24586.1
311	211 311	30	50	C25/30	B 450 C	ø 10/7.5								0.000	0.60	0.540	55	41	171706.4	65039.7	0.00000							55	36	7.56		65039.7	24586.1
314	214 314	30	40	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	40	21	50930.4	19877.9	0.000	0.48	0.432	50	31	94270.2	32519.9	0.05780	40	36	4.62		18958.6	24586.1	50	16	7.56		31016.0	12293.1
315	215 315	40	40	C25/30	B 450 C	ø 10/7.5	0.000	0.60	0.540	60	31	141405.2	72885.5	0.000	0.48	0.432	40	31	75416.1	24995.4	0.08136	60	36	9.24		68141.7	30732.6	40	36	5.81		23368.5	30732.6
316	216 316	40	40	C25/30	B 450 C	ø 10/7.5	0.000	0.60	0.540	60	31	141405.2	139145.1	0.000	0.48	0.432	60	31	113124.2	26015.9	0.09157	60	16	15.39		128952.0	18439.6	60	16	6.04		24110.1	18439.6
317	217 317	30	50	C25/30	B 450 C	ø 10/7.5	0.000	0.48	0.432	65	21	81966.1	26712.7	0.000	0.60	0.540	30	41	93198.9	76045.4	0.07737	65	16	6.21		25059.4	18439.6	30	36	8.43		71338.7	30732.6
319	219 319	40	30	C25/30	B 450 C	ø 10/12.5	0.000	0.48	0.432	30	31	56562.1	19877.9	0.000	0.48	0.432	40	21	50930.4	19877.9	0.05886	30	36	4.62		18941.9	18439.6	40	36	4.62		18941.9	18439.6
320	220 320	50	30	C25/30	B 450 C	ø 10/15.0	0.000	0.60	0.540	30	41	93658.0	43703.7								0.00000	30	36	5.54		43703.7	18439.6						
321	221 321	30	50	C25/30	B 450 C	ø 10/12.5	0.000	0.48	0.432	45	21	57296.7	13553.5	0.000	0.48	0.432	30	41	74926.4	27684.9	0.04895	45	36	3.15		13022.8	18439.6	30	36	6.43		26600.8	18439.6

Combinazioni agli Stati Limite di Danno

Massimi spostamenti differenziali orizzontali

- Fattore moltiplicativo spostamenti dovuti al sisma b 1
- c 1
- Controllo degli spostamenti di interpiano dU inferiore a 0.005 H

	U_x		U_y		U_z		$\|U_{xyz}\|$	
Comb.	**Nodi**	**U_x [cm]**	**Nodi**	**U_y [cm]**	**Nodi**	**U_z [cm]**	**Nodi**	**$\|U_{xyz}\|$ [cm]**
24	124-224	0.40	133-233	0.25	2-102	0.00	127-227	0.47
25	135-235	0.47	19-119	-0.46	7-107	-0.00	101-201	0.59
26	124-224	0.30	19-119	0.84	5-105	0.01	19-119	0.84
27	135-235	-0.42	19-119	0.96	7-107	0.01	19-119	0.96
28	135-235	-0.47	19-119	0.46	7-107	0.00	101-201	0.59
29	124-224	-0.40	133-233	-0.25	2-102	-0.00	127-227	0.47
30	135-235	0.42	19-119	-0.96	7-107	-0.01	19-119	0.96
31	124-224	-0.30	19-119	-0.84	5-105	-0.01	19-119	0.84

Spostamenti Max in direzione U_x [cm]

Nodi	**Comb.**	**24**	**25**	**26**	**27**	**28**	**29**	**30**	**31**
124 224	24	**0.40**	0.28	0.30	0.10	-0.28	-0.40	-0.10	-0.30
135 235	25	0.28	**0.47**	-0.19	-0.42	-0.47	-0.28	0.42	0.19
124 224	26	0.40	0.28	**0.30**	0.10	-0.28	-0.40	-0.10	-0.30
135 235	27	0.28	0.47	-0.19	**-0.42**	-0.47	-0.28	0.42	0.19
135 235	28	0.28	0.47	-0.19	-0.42	**-0.47**	-0.28	0.42	0.19
124 224	29	0.40	0.28	0.30	0.10	-0.28	**-0.40**	-0.10	-0.30
135 235	30	0.28	0.47	-0.19	-0.42	-0.47	-0.28	**0.42**	0.19

124 224	31	0.4 0	0.2 8	0.3 0	0.1 0	-0.2 8	-0.4 0	-0.1 0	**-0. 30**

Spostamenti Max in direzione U_y [cm]

Nodi	Comb.	24	25	26	27	28	29	30	31
133 233	24	**0.2 5**	0.0 1	0.4 5	0.3 7	-0.0 1	-0.2 5	-0.3 7	-0.4 5
19 119	25	0.0 8	**-0. 46**	0.8 4	0.9 6	0.4 6	-0.0 8	-0.9 6	-0.8 4
19 119	26	0.0 8	-0.4 6	**0.8 4**	0.9 6	0.4 6	-0.0 8	-0.9 6	-0.8 4
19 119	27	0.0 8	-0.4 6	0.8 4	**0.9 6**	0.4 6	-0.0 8	-0.9 6	-0.8 4
19 119	28	0.0 8	-0.4 6	0.8 4	0.9 6	**0.4 6**	-0.0 8	-0.9 6	-0.8 4
133 233	29	0.2 5	0.0 1	0.4 5	0.3 7	-0.0 1	**-0. 25**	-0.3 7	-0.4 5
19 119	30	0.0 8	-0.4 6	0.8 4	0.9 6	0.4 6	-0.0 8	**-0. 96**	-0.8 4
19 119	31	0.0 8	-0.4 6	0.8 4	0.9 6	0.4 6	-0.0 8	-0.9 6	**-0. 84**

Spostamenti Max in direzione U_z [cm]

Nodi	Comb.	24	25	26	27	28	29	30	31
2 102	24	**0.0 0**	0.0 0	0.0 1	0.0 1	-0.0 0	-0.0 0	-0.0 1	-0.0 1
7 107	25	0.0 0	**-0. 00**	0.0 1	0.0 1	0.0 0	-0.0 0	-0.0 1	-0.0 1
5 105	26	0.0 0	0.0 0	**0.0 1**	0.0 1	-0.0 0	-0.0 0	-0.0 1	-0.0 1
7 107	27	0.0 0	-0.0 0	0.0 1	**0.0 1**	0.0 0	-0.0 0	-0.0 1	-0.0 1
7 107	28	0.0 0	-0.0 0	0.0 1	0.0 1	**0.0 0**	-0.0 0	-0.0 1	-0.0 1
2 102	29	0.0 0	0.0 0	0.0 1	0.0 1	-0.0 0	**-0. 00**	-0.0 1	-0.0 1
7 107	30	0.0 0	-0.0 0	0.0 1	0.0 1	0.0 0	-0.0 0	**-0. 01**	-0.0 1
5 105	31	0.0 0	0.0 0	0.0 1	0.0 1	-0.0 0	-0.0 0	-0.0 1	**-0. 01**

Spostamenti Max in direzione $|U_{xyz}|$ [cm]

Nodi	Comb.	24	25	26	27	28	29	30	31
127 227	24	**0.4 7**	0.2 8	0.5 4	0.3 9	0.2 8	0.4 7	0.3 9	0.5 4

101 201	25	0.30	**0.59**	0.74	0.89	0.59	0.30	0.89	0.74
19 119	26	0.08	0.46	**0.84**	0.96	0.46	0.08	0.96	0.84
19 119	27	0.08	0.46	0.84	**0.96**	0.46	0.08	0.96	0.84
101 201	28	0.30	0.59	0.74	0.89	**0.59**	0.30	0.89	0.74
127 227	29	0.47	0.28	0.54	0.39	0.28	**0.47**	0.39	0.54
19 119	30	0.08	0.46	0.84	0.96	0.46	0.08	**0.96**	0.84
19 119	31	0.08	0.46	0.84	0.96	0.46	0.08	0.96	**0.84**

Spostamenti Massimi :

Combinazione di Carico 27 Fra i nodi 19 119 $|U_{xyz}|$ Spostamento 0.96 [cm]

Non si sono rilevati spostamenti di interpiano superiori a 0.005000 H

du/H x 1000 Max in direzione U_x

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	24	25	26	27	28	29	30	31
124 224	0.00	0.00	345.00	345.00	24	**1.162**	0.809	0.884	0.293	-0.809	-1.162	-0.293	-0.884
135 235	0.00	0.00	345.00	345.00	25	0.822	**1.356**	-0.563	-1.216	-1.356	-0.822	1.216	0.563
124 224	0.00	0.00	345.00	345.00	26	1.162	0.809	**0.884**	0.293	-0.809	-1.162	-0.293	-0.884
135 235	0.00	0.00	345.00	345.00	27	0.822	1.356	-0.563	**-1.216**	-1.356	-0.822	1.216	0.563
135 235	0.00	0.00	345.00	345.00	28	0.822	1.356	-0.563	-1.216	**-1.356**	-0.822	1.216	0.563
124 224	0.00	0.00	345.00	345.00	29	1.162	0.809	0.884	0.293	-0.809	**-1.162**	-0.293	-0.884
135 235	0.00	0.00	345.00	345.00	30	0.822	1.356	-0.563	-1.216	-1.356	-0.822	**1.216**	0.563
124 224	0.00	0.00	345.00	345.00	31	1.162	0.809	0.884	0.293	-0.809	-1.162	-0.293	**-0.884**

du/H x 1000 Max in direzione U_y

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	24	25	26	27	28	29	30	31
133 233	0.00	0.00	345.00	345.00	24	**0.736**	0.019	1.308	1.081	-0.019	-0.736	-1.081	-1.308
19 119	0.00	0.00	375.00	375.00	25	0.209	**-1.235**	2.253	2.561	1.235	-0.209	-2.561	-2.253
19 119	0.00	0.00	375.00	375.00	26	0.209	-1.235	**2.253**	2.561	1.235	-0.209	-2.561	-2.253

19 119	0.00	0.00	375.00	375.00	27	0.209	-1.235	2.253	**2.561**	1.235	-0.209	-2.561	-2.253
19 119	0.00	0.00	375.00	375.00	28	0.209	-1.235	2.253	2.561	**1.235**	-0.209	-2.561	-2.253
133 233	0.00	0.00	345.00	345.00	29	0.736	0.019	1.308	1.081	-0.019	**-0.736**	-1.081	-1.308
19 119	0.00	0.00	375.00	375.00	30	0.209	-1.235	2.253	2.561	1.235	-0.209	**-2.561**	-2.253
19 119	0.00	0.00	375.00	375.00	31	0.209	-1.235	2.253	2.561	1.235	-0.209	-2.561	**-2.253**

du/H x 1000 Max in direzione U_z

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	24	25	26	27	28	29	30	31
2 102	0.00	0.00	375.00	375.00	24	**0.013**	0.002	0.021	0.017	-0.002	-0.013	-0.017	-0.021
7 107	0.00	0.00	375.00	375.00	25	0.002	**-0.009**	0.017	0.019	0.009	-0.002	-0.019	-0.017
5 105	0.00	0.00	375.00	375.00	26	0.013	0.001	**0.021**	0.017	-0.001	-0.013	-0.017	-0.021
7 107	0.00	0.00	375.00	375.00	27	0.002	-0.009	0.017	**0.019**	0.009	-0.002	-0.019	-0.017
7 107	0.00	0.00	375.00	375.00	28	0.002	-0.009	0.017	0.019	**0.009**	-0.002	-0.019	-0.017
2 102	0.00	0.00	375.00	375.00	29	0.013	0.002	0.021	0.017	-0.002	**-0.013**	-0.017	-0.021
7 107	0.00	0.00	375.00	375.00	30	0.002	-0.009	0.017	0.019	0.009	-0.002	**-0.019**	-0.017
5 105	0.00	0.00	375.00	375.00	31	0.013	0.001	0.021	0.017	-0.001	-0.013	-0.017	**-0.021**

du/H x 1000 Max in direzione $|U_{xyz}|$

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	24	25	26	27	28	29	30	31
127 227	0.00	0.00	345.00	345.00	24	**1.375**	0.809	1.578	1.120	0.809	1.375	1.120	1.578
101 201	0.00	0.00	345.00	345.00	25	0.868	**1.700**	2.141	2.592	1.700	0.868	2.592	2.141
19 119	0.00	0.00	375.00	375.00	26	0.213	1.235	**2.253**	2.561	1.235	0.213	2.561	2.253
19 119	0.00	0.00	375.00	375.00	27	0.213	1.235	2.253	**2.561**	1.235	0.213	2.561	2.253
101 201	0.00	0.00	345.00	345.00	28	0.868	1.700	2.141	2.592	**1.700**	0.868	2.592	2.141
127 227	0.00	0.00	345.00	345.00	29	1.375	0.809	1.578	1.120	0.809	**1.375**	1.120	1.578
19 119	0.00	0.00	375.00	375.00	30	0.213	1.235	2.253	2.561	1.235	0.213	**2.561**	2.253

19 119	0.0 0	0.0 0	375. 00	375. 00	31	0.21 3	1.23 5	2.25 3	2.56 1	1.23 5	0.21 3	2.56 1	**2.2 53**

Combinazioni agli Stati Limite di Operatività

Massimi spostamenti differenziali orizzontali

- Fattore moltiplicativo spostamenti dovuti al sisma b 1
- c 1
- Controllo degli spostamenti di interpiano dU inferiore a 0.005 H

	U_x		U_y		U_z		$\lvert U_{xyz} \rvert$	
Comb.	**Nodi**	**U_x [cm]**	**Nodi**	**U_y [cm]**	**Nodi**	**U_z [cm]**	**Nodi**	**$\lvert U_{xyz} \rvert$ [cm]**
32	124-224	0.30	133-233	0.19	2-102	0.00	127-227	0.36
33	135-235	0.35	19-119	-0.35	7-107	-0.00	101-201	0.44
34	124-224	0.23	19-119	0.63	5-105	0.01	19-119	0.63
35	135-235	-0.31	19-119	0.72	7-107	0.01	19-119	0.72
36	135-235	-0.35	19-119	0.35	7-107	0.00	101-201	0.44
37	124-224	-0.30	133-233	-0.19	2-102	-0.00	127-227	0.36
38	135-235	0.31	19-119	-0.72	7-107	-0.01	19-119	0.72
39	124-224	-0.23	19-119	-0.63	5-105	-0.01	19-119	0.63

Spostamenti Max in direzione U_x [cm]

Nodi	**Comb.**	**32**	**33**	**34**	**35**	**36**	**37**	**38**	**39**
124 224	32	**0.30**	0.21	0.23	0.08	-0.21	-0.30	-0.08	-0.23
135 235	33	0.21	**0.35**	-0.15	-0.31	-0.35	-0.21	0.31	0.15
124 224	34	0.30	0.21	**0.23**	0.08	-0.21	-0.30	-0.08	-0.23
135 235	35	0.21	0.35	-0.15	**-0.31**	-0.35	-0.21	0.31	0.15
135 235	36	0.21	0.35	-0.15	-0.31	**-0.35**	-0.21	0.31	0.15
124 224	37	0.30	0.21	0.23	0.08	-0.21	**-0.30**	-0.08	-0.23

135 235	38	0.21	0.35	-0.15	-0.31	-0.35	-0.21	**0.31**	0.15
124 224	39	0.30	0.21	0.23	0.08	-0.21	-0.30	-0.08	**-0.23**

Spostamenti Max in direzione U_y [cm]

Nodi	Comb.	32	33	34	35	36	37	38	39
133 233	32	**0.19**	0.01	0.34	0.28	-0.01	-0.19	-0.28	-0.34
19 119	33	0.06	**-0.35**	0.63	0.72	0.35	-0.06	-0.72	-0.63
19 119	34	0.06	-0.35	**0.63**	0.72	0.35	-0.06	-0.72	-0.63
19 119	35	0.06	-0.35	0.63	**0.72**	0.35	-0.06	-0.72	-0.63
19 119	36	0.06	-0.35	0.63	0.72	**0.35**	-0.06	-0.72	-0.63
133 233	37	0.19	0.01	0.34	0.28	-0.01	**-0.19**	-0.28	-0.34
19 119	38	0.06	-0.35	0.63	0.72	0.35	-0.06	**-0.72**	-0.63
19 119	39	0.06	-0.35	0.63	0.72	0.35	-0.06	-0.72	**-0.63**

Spostamenti Max in direzione U_z [cm]

Nodi	Comb.	32	33	34	35	36	37	38	39
2 102	32	**0.00**	0.00	0.01	0.00	-0.00	-0.00	-0.00	-0.01
7 107	33	0.00	**-0.00**	0.00	0.01	0.00	-0.00	-0.01	-0.00
5 105	34	0.00	0.00	**0.01**	0.00	-0.00	-0.00	-0.00	-0.01
7 107	35	0.00	-0.00	0.00	**0.01**	0.00	-0.00	-0.01	-0.00
7 107	36	0.00	-0.00	0.00	0.01	**0.00**	-0.00	-0.01	-0.00
2 102	37	0.00	0.00	0.01	0.00	-0.00	**-0.00**	-0.00	-0.01
7 107	38	0.00	-0.00	0.00	0.01	0.00	-0.00	**-0.01**	-0.00
5 105	39	0.00	0.00	0.01	0.00	-0.00	-0.00	-0.00	**-0.01**

Spostamenti Max in direzione $|U_{xyz}|$ [cm]

Nodi	Comb.	32	33	34	35	36	37	38	39

127 227	32	**0.36**	0.21	0.41	0.29	0.21	0.36	0.29	0.41
101 201	33	0.22	**0.44**	0.55	0.67	0.44	0.22	0.67	0.55
19 119	34	0.06	0.35	**0.63**	0.72	0.35	0.06	0.72	0.63
19 119	35	0.06	0.35	0.63	**0.72**	0.35	0.06	0.72	0.63
101 201	36	0.22	0.44	0.55	0.67	**0.44**	0.22	0.67	0.55
127 227	37	0.36	0.21	0.41	0.29	0.21	**0.36**	0.29	0.41
19 119	38	0.06	0.35	0.63	0.72	0.35	0.06	**0.72**	0.63
19 119	39	0.06	0.35	0.63	0.72	0.35	0.06	0.72	**0.63**

Spostamenti Massimi :

Combinazione di Carico 35 Fra i nodi 19 119 $|U_{xyz}|$ Spostamento 0.72 [cm]

Non si sono rilevati spostamenti di interpiano superiori a 0.005000 H

du/H x 1000 Max in direzione U_x

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	32	33	34	35	36	37	38	39
124 224	0.00	0.00	345.00	345.00	32	**0.875**	0.610	0.664	0.218	-0.610	-0.875	-0.218	-0.664
135 235	0.00	0.00	345.00	345.00	33	0.617	**1.016**	-0.421	-0.911	-1.016	-0.617	0.911	0.421
124 224	0.00	0.00	345.00	345.00	34	0.875	0.610	**0.664**	0.218	-0.610	-0.875	-0.218	-0.664
135 235	0.00	0.00	345.00	345.00	35	0.617	1.016	-0.421	**-0.911**	-1.016	-0.617	0.911	0.421
135 235	0.00	0.00	345.00	345.00	36	0.617	1.016	-0.421	-0.911	**-1.016**	-0.617	0.911	0.421
124 224	0.00	0.00	345.00	345.00	37	0.875	0.610	0.664	0.218	-0.610	**-0.875**	-0.218	-0.664
135 235	0.00	0.00	345.00	345.00	38	0.617	1.016	-0.421	-0.911	-1.016	-0.617	**0.911**	0.421
124 224	0.00	0.00	345.00	345.00	39	0.875	0.610	0.664	0.218	-0.610	-0.875	-0.218	**-0.664**

du/H x 1000 Max in direzione U_y

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	32	33	34	35	36	37	38	39
133 233	0.00	0.00	345.00	345.00	32	**0.552**	0.015	0.980	0.809	-0.015	-0.552	-0.809	-0.980
19 119	0.00	0.00	375.00	375.00	33	0.157	**-0.924**	1.686	1.916	0.924	-0.157	-1.916	-1.686

19 119	0.00	0.00	375.00	375.00	34	0.157	-0.924	**1.686**	1.916	0.924	-0.157	-1.916	-1.686
19 119	0.00	0.00	375.00	375.00	35	0.157	-0.924	1.686	**1.916**	0.924	-0.157	-1.916	-1.686
19 119	0.00	0.00	375.00	375.00	36	0.157	-0.924	1.686	1.916	**0.924**	-0.157	-1.916	-1.686
133 233	0.00	0.00	345.00	345.00	37	0.552	0.015	0.980	0.809	-0.015	**-0.552**	-0.809	-0.980
19 119	0.00	0.00	375.00	375.00	38	0.157	-0.924	1.686	1.916	0.924	-0.157	**-1.916**	-1.686
19 119	0.00	0.00	375.00	375.00	39	0.157	-0.924	1.686	1.916	0.924	-0.157	-1.916	**-1.686**

du/H x 1000 Max in direzione U_z

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	32	33	34	35	36	37	38	39
2 102	0.00	0.00	375.00	375.00	32	**0.010**	0.001	0.016	0.012	-0.001	-0.010	-0.012	-0.016
7 107	0.00	0.00	375.00	375.00	33	0.001	**-0.006**	0.012	0.014	0.006	-0.001	-0.014	-0.012
5 105	0.00	0.00	375.00	375.00	34	0.010	0.001	**0.016**	0.013	-0.001	-0.010	-0.013	-0.016
7 107	0.00	0.00	375.00	375.00	35	0.001	-0.006	0.012	**0.014**	0.006	-0.001	-0.014	-0.012
7 107	0.00	0.00	375.00	375.00	36	0.001	-0.006	0.012	0.014	**0.006**	-0.001	-0.014	-0.012
2 102	0.00	0.00	375.00	375.00	37	0.010	0.001	0.016	0.012	-0.001	**-0.010**	-0.012	-0.016
7 107	0.00	0.00	375.00	375.00	38	0.001	-0.006	0.012	0.014	0.006	-0.001	**-0.014**	-0.012
5 105	0.00	0.00	375.00	375.00	39	0.010	0.001	0.016	0.013	-0.001	-0.010	-0.013	**-0.016**

du/H x 1000 Max in direzione $|U_{xyz}|$

Nodi	dx [cm]	dy [cm]	dz [cm]	L [cm]	Comb.	32	33	34	35	36	37	38	39
127 227	0.00	0.00	345.00	345.00	32	**1.034**	0.611	1.183	0.838	0.611	1.034	0.838	1.183
101 201	0.00	0.00	345.00	345.00	33	0.651	**1.273**	1.602	1.940	1.273	0.651	1.940	1.602
19 119	0.00	0.00	375.00	375.00	34	0.159	0.924	**1.686**	1.916	0.924	0.159	1.916	1.686
19 119	0.00	0.00	375.00	375.00	35	0.159	0.924	1.686	**1.916**	0.924	0.159	1.916	1.686
101 201	0.00	0.00	345.00	345.00	36	0.651	1.273	1.602	1.940	**1.273**	0.651	1.940	1.602
127 227	0.00	0.00	345.00	345.00	37	1.034	0.611	1.183	0.838	0.611	**1.034**	0.838	1.183

19 119	0.0 0	0.0 0	375. 00	375. 00	38	0.15 9	0.92 4	1.68 6	1.91 6	0.92 4	0.15 9	**1.9 16**	1.68 6
19 119	0.0 0	0.0 0	375. 00	375. 00	39	0.15 9	0.92 4	1.68 6	1.91 6	0.92 4	0.15 9	1.91 6	**1.6 86**

Verifiche combinazioni di carico statiche

Verifica

Dati terreno

Terreno	SABBIE E GHIAIE
Angolo d'attrito φ	31.70 [°]
Coesione c	0.0 [kg/cm²]
Coesione non drenata c_u	0.2 [kg/cm²]
Carico addizionale di superficie q	1400.0 [kg/m²]
Profondità D	0.50 [m]
Peso proprio terreno γ	2250.0 [kg/m³]

Fattori parziale di sicurezza del terreno verifiche a scorrimento

$\gamma_{R,Scor}$	1.000
$k_1$fattore riduzione di φ	0.667
$k_2$fattore riduzione di c	0.600
$k_3$fattore riduzione di c_u	0.600

Fattori parziale di sicurezza del terreno

$\gamma_{tg\varphi}$	1.000
γ_c	1.000
γ_{cu}	1.000

Fattori parziale di sicurezza

Verifica di capacità portante	2.300
Verifica a scorrimento	1.100

Fattori di correzione dinamici per combinazioni statiche

z_c	1.000
z_q	1.000
z_g	1.000

Utilizzo fattore correttivo Bowles per fondazioni di grandi dimensioni (B ≥ 2.00m) $r_\gamma = 1-0.25Log_{10}(B/2)$

Verifiche

Legenda	
B_{eq}	Base del plinto equivalente
H_{eq}	Altezza del plinto equivalente
$H_{Trasporto}$	Quota azioni esterne rispetto alla sezione di verifica
Comb.	Combinazione di carico
N	Azione verticale
M_x	Momento flettente M_x
M_y	Momento flettente M_y
Q_{Ed}	Carico verticale di progetto
$Q_{Rd,T}$	Capacità portante Terzaghi
$Q_{Rd,M}$	Capacità portante Mejerhoff
$Q_{Rd,EC7}$	Capacità portante EuroCodice 7
$Q_{Rd,V}$	Capacità portante Vesic
$Q_{Rd,T,PP}$	Capacità portante Terzaghi con correzione Paolucci-Pecker
$Q_{Rd,M,PP}$	Capacità portante Mejerhoff con correzione Paolucci-Pecker
$Q_{Rd,EC7,PP}$	Capacità portante EuroCodice 7 con correzione Paolucci-Pecker
$Q_{Rd,V,PP}$	Capacità portante Vesic con correzione Paolucci-Pecker
$Q_{Rd,T,MN,CI}$	Capacità portante Terzaghi con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,M,MN,CI}$	Capacità portante Mejerhoff con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,EC7,MN,CI}$	Capacità portante EuroCodice 7 con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,V,MN,CI}$	Capacità portante Vesic con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,T,MN,C}$	Capacità portante Terzaghi con correzione Maugeri-Novità con effetto cinematico
$Q_{Rd,M,MN,C}$	Capacità portante Mejerhoff con correzione Maugeri-Novità con effetto cinematico
$Q_{Rd,EC7,MN,C}$	Capacità portante EuroCodice 7 con correzione Maugeri-Novità con effetto cinematico
$Q_{Rd,V,MN,C}$	Capacità portante Vesic con correzione Maugeri-Novità con effetto cinematico
F_x	Azione di scorrimento F_x
F_y	Azione di scorrimento F_y
$H_{Ed,d=\sqrt{Fx,Fy}}$	Azione di scorrimento totale $H_{Ed}= \sqrt{(F_x^2+F_y^2)}$
H_{Rd}	Resistenza allo scorrimento

Elemento	**B_{Eq} [m]**	**H_{Eq} [m]**	**$H_{Trasporto}$ [m]**	**Comb.**	**N [kg]**	**M_x [kgm]**	**M_y [kgm]**	**Q_{Ed} [kg]**	**$(S/R)_{EC7}$ [kg]**	**F_x [kg]**	**F_y [kg]**	**H_{Ed} [kg]**	**$(S/R)_{Scor}$**
12,18	0.90	6.70	0.50	1	59257.4	-9539.1	0.0	59257.4	0.401	0.0	0.0	0.0	0.000

				2	56890.1	-9848.1	0.0	56890.1	0.386	0.0	0.0	0.0	0.000
				19	44749.9	-7413.9	0.0	44749.9	0.303	0.0	0.0	0.0	0.000
				20	43171.6	-7619.8	-0.0	43171.6	0.293	0.0	0.0	0.0	0.000
				21	42038.9	-7655.8	0.0	42038.9	0.286	0.0	0.0	0.0	0.000
				22	40986.7	-7793.1	0.0	40986.7	0.280	0.0	0.0	0.0	0.000
				23	40968.8	-7770.6	0.0	40968.8	0.280	0.0	0.0	0.0	0.000
17,10	0.90	4.07	0.50	1	35483.1	903.0	0.0	35483.1	0.377	0.0	0.0	0.0	0.000
				2	33690.7	813.9	-0.0	33690.7	0.357	0.0	0.0	0.0	0.000
				19	26669.8	658.4	0.0	26669.8	0.283	0.0	0.0	0.0	0.000
				20	25474.9	599.0	-0.0	25474.9	0.270	0.0	0.0	0.0	0.000
				21	24636.6	539.7	-0.0	24636.6	0.261	0.0	0.0	0.0	0.000
				22	23839.9	500.1	0.0	23839.9	0.253	0.0	0.0	0.0	0.000
				23	23830.7	495.8	-0.0	23830.7	0.252	0.0	0.0	0.0	0.000
17,25	0.90	4.16	0.50	1	35933.7	-1151.7	0.0	35933.7	0.374	0.0	0.0	0.0	0.000
				2	34348.0	-908.5	0.1	34348.0	0.357	0.0	0.0	0.0	0.000
				19	27055.0	-822.7	0.0	27055.0	0.282	0.0	0.0	0.0	0.000
				20	25997.9	-660.6	0.0	25997.9	0.270	0.0	0.0	0.0	0.000
				21	25141.2	-621.2	0.0	25141.2	0.261	0.0	0.0	0.0	0.000
				22	24436.5	-513.1	0.0	24436.5	0.253	0.0	0.0	0.0	0.000
				23	24402.7	-528.4	-0.0	24402.7	0.253	0.0	0.0	0.0	0.000
12,28	0.90	5.93	0.50	1	47552.9	-122.5	0.0	47552.9	0.346	0.0	0.0	0.0	0.000
				2	45539.5	314.3	0.0	45539.5	0.331	0.0	0.0	0.0	0.000
				19	35833.8	-9.8	0.0	35833.8	0.260	0.0	0.0	0.0	0.000
				20	34491.6	281.4	0.0	34491.6	0.251	0.0	0.0	0.0	0.000
				21	33400.5	251.9	0.0	33400.5	0.243	0.0	0.0	0.0	0.000
				22	32505.7	446.1	0.0	32505.7	0.237	0.0	0.0	0.0	0.000

				23	32462.1	396.4	0.0	32462.1	0.237	0.0	0.0	0.0	0.000
5,12	0.90	2.10	0.50	1	22505.7	-903.3	0.0	22505.7	0.461	0.0	0.0	0.0	0.000
				2	21445.9	-901.3	0.0	21445.9	0.440	0.0	0.0	0.0	0.000
				19	16952.3	-695.7	0.0	16952.3	0.347	0.0	0.0	0.0	0.000
				20	16245.7	-694.3	0.0	16245.7	0.333	0.0	0.0	0.0	0.000
				21	15783.4	-698.8	0.0	15783.4	0.324	0.0	0.0	0.0	0.000
				22	15312.4	-697.9	0.0	15312.4	0.315	0.0	0.0	0.0	0.000
				23	15314.3	-699.1	0.0	15314.3	0.315	0.0	0.0	0.0	0.000
11,27	0.90	5.93	0.50	1	44797.9	2115.2	0.0	44797.9	0.330	0.0	0.0	0.0	0.000
				2	42957.3	2363.4	0.0	42957.3	0.318	0.0	0.0	0.0	0.000
				19	33778.3	1650.5	0.0	33778.3	0.249	0.0	0.0	0.0	0.000
				20	32551.2	1816.0	0.0	32551.2	0.241	0.0	0.0	0.0	0.000
				21	31553.1	1714.9	0.0	31553.1	0.233	0.0	0.0	0.0	0.000
				22	30735.0	1825.2	0.0	30735.0	0.228	0.0	0.0	0.0	0.000
				23	30695.0	1778.2	0.0	30695.0	0.227	0.0	0.0	0.0	0.000
4,11	0.90	2.10	0.50	1	21732.1	-1283.8	0.0	21732.1	0.453	0.0	0.0	0.0	0.000
				2	20722.7	-1251.5	0.0	20722.7	0.432	0.0	0.0	0.0	0.000
				19	16374.5	-977.9	0.0	16374.5	0.341	0.0	0.0	0.0	0.000
				20	15701.6	-956.4	0.0	15701.6	0.328	0.0	0.0	0.0	0.000
				21	15261.8	-946.8	0.0	15261.8	0.319	0.0	0.0	0.0	0.000
				22	14813.2	-932.5	0.0	14813.2	0.310	0.0	0.0	0.0	0.000
				23	14815.1	-933.5	0.0	14815.1	0.310	0.0	0.0	0.0	0.000
10,26	0.90	5.93	0.50	1	45128.9	1391.0	0.0	45128.9	0.331	0.0	0.0	0.0	0.000
				2	43308.3	1651.3	0.0	43308.3	0.319	0.0	0.0	0.0	0.000
				19	34042.6	1102.4	0.0	34042.6	0.250	0.0	0.0	0.0	0.000
				20	32828.9	1275.9	0.0	32828.9	0.241	0.0	0.0	0.0	0.000

				21	31849.3	1196.7	0.0	31849.3	0.234	0.0	0.0	0.0	0.000
				22	31040.1	1312.4	0.0	31040.1	0.229	0.0	0.0	0.0	0.000
				23	31002.3	1269.1	0.0	31002.3	0.228	0.0	0.0	0.0	0.000
3,10	0.90	2.10	0.50	1	21961.0	-1361.8	0.0	21961.0	0.459	0.0	0.0	0.0	0.000
				2	20959.9	-1325.9	0.0	20959.9	0.438	0.0	0.0	0.0	0.000
				19	16551.5	-1036.2	0.0	16551.5	0.346	0.0	0.0	0.0	0.000
				20	15884.1	-1012.3	0.0	15884.1	0.332	0.0	0.0	0.0	0.000
				21	15441.2	-999.5	0.0	15441.2	0.323	0.0	0.0	0.0	0.000
				22	14996.3	-983.6	0.0	14996.3	0.314	0.0	0.0	0.0	0.000
				23	14996.8	-984.3	0.0	14996.8	0.314	0.0	0.0	0.0	0.000
2,17	0.90	3.87	0.50	1	39211.6	-4200.5	0.0	39211.6	0.456	0.0	0.0	0.0	0.000
				2	37342.6	-4125.6	0.0	37342.6	0.435	0.0	0.0	0.0	0.000
				19	29500.7	-3200.5	0.0	29500.7	0.343	0.0	0.0	0.0	0.000
				20	28254.7	-3150.6	0.0	28254.7	0.329	0.0	0.0	0.0	0.000
				21	27344.5	-3100.1	0.0	27344.5	0.319	0.0	0.0	0.0	0.000
				22	26513.8	-3066.8	0.0	26513.8	0.310	0.0	0.0	0.0	0.000
				23	26496.1	-3063.0	0.0	26496.1	0.309	0.0	0.0	0.0	0.000
16,24	0.90	4.16	0.50	1	35947.9	-2820.5	0.0	35947.9	0.383	0.0	0.0	0.0	0.000
				2	34240.9	-2374.6	0.0	34240.9	0.363	0.0	0.0	0.0	0.000
				19	26989.4	-1998.0	0.0	26989.4	0.287	0.0	0.0	0.0	0.000
				20	25851.5	-1700.7	0.0	25851.5	0.274	0.0	0.0	0.0	0.000
				21	24820.3	-1436.3	0.0	24820.3	0.262	0.0	0.0	0.0	0.000
				22	24061.7	-1238.1	0.0	24061.7	0.253	0.0	0.0	0.0	0.000
				23	24001.1	-1223.3	0.0	24001.1	0.252	0.0	0.0	0.0	0.000
9,16	0.90	2.54	0.50	1	24385.1	-210.3	0.0	24385.1	0.404	0.0	0.0	0.0	0.000
				2	23035.8	-245.5	0.0	23035.8	0.383	0.0	0.0	0.0	0.000

				19	18233.0	-174.3	0.0	18233.0	0.303	0.0	0.0	0.0	0.000
				20	17333.5	-197.8	0.0	17333.5	0.288	0.0	0.0	0.0	0.000
				21	16515.6	-215.3	0.0	16515.6	0.275	0.0	0.0	0.0	0.000
				22	15915.9	-230.9	0.0	15915.9	0.265	0.0	0.0	0.0	0.000
				23	15867.4	-231.3	0.0	15867.4	0.264	0.0	0.0	0.0	0.000
1,9	0.90	1.33	0.50	1	15105.1	-395.3	0.0	15105.1	0.472	0.0	0.0	0.0	0.000
				2	14352.5	-378.7	0.0	14352.5	0.449	0.0	0.0	0.0	0.000
				19	11325.5	-297.7	0.0	11325.5	0.354	0.0	0.0	0.0	0.000
				20	10823.8	-286.7	0.0	10823.8	0.338	0.0	0.0	0.0	0.000
				21	10363.7	-276.9	0.0	10363.7	0.324	0.0	0.0	0.0	0.000
				22	10029.2	-269.6	0.0	10029.2	0.314	0.0	0.0	0.0	0.000
				23	10001.3	-269.0	0.0	10001.3	0.313	0.0	0.0	0.0	0.000
8,23	0.90	6.70	0.50	1	51554.4	-12062.7	0.0	51554.4	0.357	0.0	0.0	0.0	0.000
				2	49567.7	-10430.5	0.0	49567.7	0.340	0.0	0.0	0.0	0.000
				19	38946.6	-8752.5	0.0	38946.6	0.269	0.0	0.0	0.0	0.000
				20	37622.1	-7664.4	0.0	37622.1	0.258	0.0	0.0	0.0	0.000
				21	36630.9	-7047.3	0.0	36630.9	0.250	0.0	0.0	0.0	0.000
				22	35747.9	-6321.9	0.0	35747.9	0.243	0.0	0.0	0.0	0.000
				23	35723.9	-6346.0	0.0	35723.9	0.243	0.0	0.0	0.0	0.000
15,22	0.90	5.20	0.50	1	41482.2	-4821.5	0.0	41482.2	0.358	0.0	0.0	0.0	0.000
				2	39867.7	-4289.3	0.0	39867.7	0.343	0.0	0.0	0.0	0.000
				19	31341.4	-3542.6	0.0	31341.4	0.270	0.0	0.0	0.0	0.000
				20	30265.1	-3187.8	0.0	30265.1	0.260	0.0	0.0	0.0	0.000
				21	29492.2	-3005.2	0.0	29492.2	0.253	0.0	0.0	0.0	0.000
				22	28774.7	-2768.6	0.0	28774.7	0.246	0.0	0.0	0.0	0.000
				23	28762.4	-2780.6	0.0	28762.4	0.246	0.0	0.0	0.0	0.000

7,15	0.90	1.50	0.50	1	17965.4	-737.6	0.0	17965.4	0.511	0.0	0.0	0.0	0.000
				2	17150.0	-715.1	0.0	17150.0	0.488	0.0	0.0	0.0	0.000
				19	13541.5	-559.9	0.0	13541.5	0.385	0.0	0.0	0.0	0.000
				20	12997.9	-544.9	0.0	12997.9	0.370	0.0	0.0	0.0	0.000
				21	12638.2	-535.6	0.0	12638.2	0.360	0.0	0.0	0.0	0.000
				22	12275.8	-525.6	0.0	12275.8	0.350	0.0	0.0	0.0	0.000
				23	12276.4	-525.8	0.0	12276.4	0.350	0.0	0.0	0.0	0.000
13,20	0.90	5.20	0.50	1	44450.3	-8233.8	0.0	44450.3	0.394	0.0	0.0	0.0	0.000
				2	43194.4	-7953.3	0.0	43194.4	0.383	0.0	0.0	0.0	0.000
				19	33760.2	-6243.7	0.0	33760.2	0.300	0.0	0.0	0.0	0.000
				20	32923.0	-6056.7	0.0	32923.0	0.292	0.0	0.0	0.0	0.000
				21	32354.6	-5952.4	0.0	32354.6	0.287	0.0	0.0	0.0	0.000
				22	31796.5	-5827.8	0.0	31796.5	0.282	0.0	0.0	0.0	0.000
				23	31794.2	-5832.3	0.0	31794.2	0.282	0.0	0.0	0.0	0.000
16,17	0.90	6.39	0.50	1	51135.4	486.5	0.0	51135.4	0.346	0.0	0.0	0.0	0.000
				2	48509.2	250.3	0.0	48509.2	0.328	0.0	0.0	0.0	0.000
				19	38359.8	219.5	0.0	38359.8	0.259	0.0	0.0	0.0	0.000
				20	36609.0	62.1	0.0	36609.0	0.247	0.0	0.0	0.0	0.000
				21	35175.6	-297.4	-0.0	35175.6	0.238	0.0	0.0	0.0	0.000
				22	34008.4	-402.4	-0.0	34008.4	0.230	0.0	0.0	0.0	0.000
				23	33949.3	-459.1	-0.0	33949.3	0.230	0.0	0.0	0.0	0.000
14,15	0.90	4.08	0.50	1	41015.8	38.6	0.0	41015.8	0.429	0.0	0.0	0.0	0.000
				2	39103.8	47.5	0.0	39103.8	0.409	0.0	0.0	0.0	0.000
				19	30896.9	32.7	0.0	30896.9	0.323	0.0	0.0	0.0	0.000
				20	29622.2	38.6	0.0	29622.2	0.310	0.0	0.0	0.0	0.000
				21	28772.3	42.3	0.0	28772.3	0.301	0.0	0.0	0.0	0.000

				22	27922.6	46.2	0.0	27922.6	0.292	0.0	0.0	0.0	0.000
				23	27922.5	46.2	0.0	27922.5	0.292	0.0	0.0	0.0	0.000
13,14	0.90	4.52	0.50	1	44581.0	784.1	0.0	44581.0	0.425	0.0	0.0	0.0	0.000
				2	42882.1	1026.8	0.0	42882.1	0.410	0.0	0.0	0.0	0.000
				19	33713.5	687.2	0.0	33713.5	0.322	0.0	0.0	0.0	0.000
				20	32580.9	849.0	0.0	32580.9	0.312	0.0	0.0	0.0	0.000
				21	31830.2	960.6	0.0	31830.2	0.305	0.0	0.0	0.0	0.000
				22	31075.1	1068.5	0.0	31075.1	0.298	0.0	0.0	0.0	0.000
				23	31076.1	1069.3	0.0	31076.1	0.299	0.0	0.0	0.0	0.000
11,12	0.90	3.61	0.50	1	32868.1	-1004.5	-0.0	32868.1	0.393	0.0	0.0	0.0	0.000
				2	31182.2	-928.3	-0.0	31182.2	0.373	0.0	0.0	0.0	0.000
				19	24703.9	-746.4	-0.0	24703.9	0.295	0.0	0.0	0.0	0.000
				20	23580.0	-695.6	-0.0	23580.0	0.282	0.0	0.0	0.0	0.000
				21	22821.0	-660.8	-0.0	22821.0	0.273	0.0	0.0	0.0	0.000
				22	22071.8	-626.9	-0.0	22071.8	0.264	0.0	0.0	0.0	0.000
				23	22069.6	-626.8	-0.0	22069.6	0.264	0.0	0.0	0.0	0.000
10,11	0.90	3.35	0.50	1	28470.9	49.6	0.0	28470.9	0.360	0.0	0.0	0.0	0.000
				2	27084.5	56.2	0.0	27084.5	0.343	0.0	0.0	0.0	0.000
				19	21424.5	40.1	0.0	21424.5	0.271	0.0	0.0	0.0	0.000
				20	20500.2	44.4	0.0	20500.2	0.260	0.0	0.0	0.0	0.000
				21	19876.4	46.2	0.0	19876.4	0.252	0.0	0.0	0.0	0.000
				22	19260.2	49.1	0.0	19260.2	0.244	0.0	0.0	0.0	0.000
				23	19258.5	48.8	0.0	19258.5	0.244	0.0	0.0	0.0	0.000
8,9	0.90	5.16	0.50	1	55638.3	3831.6	0.0	55638.3	0.475	0.0	0.0	0.0	0.000
				2	52600.2	3392.2	0.0	52600.2	0.449	0.0	0.0	0.0	0.000
				19	41690.5	2853.8	0.0	41690.5	0.356	0.0	0.0	0.0	0.000

				20	39665.1	2560.9	0.0	39665.1	0.338	0.0	0.0	0.0	0.000
				21	38075.6	2560.4	0.0	38075.6	0.325	0.0	0.0	0.0	0.000
				22	36725.3	2365.2	0.0	36725.3	0.313	0.0	0.0	0.0	0.000
				23	36672.2	2408.4	0.0	36672.2	0.313	0.0	0.0	0.0	0.000
7,8	0.90	5.48	0.50	1	65289.6	5534.1	0.0	65289.6	0.528	0.0	0.0	0.0	0.000
				2	62098.9	5846.5	0.0	62098.9	0.504	0.0	0.0	0.0	0.000
				19	49132.9	4371.0	0.0	49132.9	0.398	0.0	0.0	0.0	0.000
				20	47005.8	4579.3	0.0	47005.8	0.382	0.0	0.0	0.0	0.000
				21	45591.0	4743.0	0.0	45591.0	0.371	0.0	0.0	0.0	0.000
				22	44172.9	4881.9	0.0	44172.9	0.361	0.0	0.0	0.0	0.000
				23	44173.6	4887.4	0.0	44173.6	0.361	0.0	0.0	0.0	0.000
5,6	0.90	6.45	0.50	1	71804.0	-7643.5	-0.0	71804.0	0.496	0.0	0.0	0.0	0.000
				2	69407.9	-7897.0	-0.0	69407.9	0.481	0.0	0.0	0.0	0.000
				19	54442.5	-5978.8	-0.0	54442.5	0.377	0.0	0.0	0.0	0.000
				20	52845.1	-6147.9	-0.0	52845.1	0.366	0.0	0.0	0.0	0.000
				21	51876.1	-6302.9	-0.0	51876.1	0.360	0.0	0.0	0.0	0.000
				22	50811.2	-6415.9	-0.0	50811.2	0.353	0.0	0.0	0.0	0.000
				23	50832.5	-6425.1	-0.0	50832.5	0.354	0.0	0.0	0.0	0.000
4,5	0.90	3.61	0.50	1	43776.2	116.8	0.0	43776.2	0.516	0.0	0.0	0.0	0.000
				2	41901.1	103.9	0.0	41901.1	0.494	0.0	0.0	0.0	0.000
				19	33044.7	85.0	0.0	33044.7	0.389	0.0	0.0	0.0	0.000
				20	31794.7	76.4	0.0	31794.7	0.375	0.0	0.0	0.0	0.000
				21	31001.8	69.6	0.0	31001.8	0.365	0.0	0.0	0.0	0.000
				22	30168.5	63.8	0.0	30168.5	0.355	0.0	0.0	0.0	0.000
				23	30177.5	63.6	0.0	30177.5	0.355	0.0	0.0	0.0	0.000
3,4	0.90	3.35	0.50	1	40626.2	280.1	0.0	40626.2	0.516	0.0	0.0	0.0	0.000

				2	38910.6	276.9	0.0	38910.6	0.494	0.0	0.0	0.0	0.000
				19	30673.4	212.9	0.0	30673.4	0.389	0.0	0.0	0.0	0.000
				20	29529.7	210.8	0.0	29529.7	0.375	0.0	0.0	0.0	0.000
				21	28798.3	204.4	0.0	28798.3	0.366	0.0	0.0	0.0	0.000
				22	28035.8	203.0	0.0	28035.8	0.356	0.0	0.0	0.0	0.000
				23	28042.7	202.0	0.0	28042.7	0.356	0.0	0.0	0.0	0.000
2,3	0.90	3.66	0.50	1	46226.6	459.9	0.0	46226.6	0.540	0.0	0.0	0.0	0.000
				2	44246.8	423.6	0.0	44246.8	0.516	0.0	0.0	0.0	0.000
				19	34870.0	329.4	0.0	34870.0	0.407	0.0	0.0	0.0	0.000
				20	33550.1	305.2	0.0	33550.1	0.391	0.0	0.0	0.0	0.000
				21	32628.6	247.8	0.0	32628.6	0.380	0.0	0.0	0.0	0.000
				22	31748.6	231.6	0.0	31748.6	0.370	0.0	0.0	0.0	0.000
				23	31739.4	222.4	0.0	31739.4	0.370	0.0	0.0	0.0	0.000
1,2	0.90	6.39	0.50	1	70651.7	-237.5	-0.0	70651.7	0.477	0.0	0.0	0.0	0.000
				2	67713.7	-454.1	-0.0	67713.7	0.458	0.0	0.0	0.0	0.000
				19	53240.3	-333.3	-0.0	53240.3	0.360	0.0	0.0	0.0	0.000
				20	51281.7	-477.8	-0.0	51281.7	0.347	0.0	0.0	0.0	0.000
				21	49622.4	-837.5	-0.0	49622.4	0.337	0.0	0.0	0.0	0.000
				22	48316.6	-933.9	-0.0	48316.6	0.328	0.0	0.0	0.0	0.000
				23	48238.1	-992.3	-0.0	48238.1	0.328	0.0	0.0	0.0	0.000

Verifiche combinazioni di carico dinamiche

Verifica in condizioni **drenate**

Dati terreno

Terreno	SABBIE E GHIAIE
Angolo d'attrito φ	31.70 [°]
Coesione c	0.0 [kg/cm²]
Coesione non drenata c_u	0.2 [kg/cm²]
Carico addizionale di superficie q	1400.0 [kg/m²]
Profondità D	0.50 [m]
Peso proprio terreno γ	2250.0 [kg/m³]

Fattori parziale di sicurezza del terreno verifiche a scorrimento

$\gamma_{R,Scor}$	1.000
$k_1$fattore riduzione di φ	0.667
$k_2$fattore riduzione di c	0.600
$k_3$fattore riduzione di c_u	0.600

Fattori parziale di sicurezza del terreno

$\gamma_{tg\varphi}$	1.000
γ_c	1.000
γ_{cu}	1.000

Fattori parziale di sicurezza

Verifica di capacità portante	2.300
Verifica a scorrimento	1.100

Fattori di correzione dinamici per combinazioni statiche

z_c	1.000
z_q	1.000
z_g	1.000

Utilizzo fattore correttivo Bowles per fondazioni di grandi dimensioni (B ≥ 2.00m) $r_\gamma = 1-0.25Log_{10}(B/2)$

Verifiche

	Legenda
B_{eq}	Base del plinto equivalente
H_{eq}	Altezza del plinto equivalente
$H_{Trasporto}$	Quota azioni esterne rispetto alla sezione di verifica
Comb.	Combinazione di carico
N	Azione verticale
M_x	Momento flettente M_x
M_y	Momento flettente M_y
Q_{Ed}	Carico verticale di progetto
$Q_{Rd,T}$	Capacità portante Terzaghi
$Q_{Rd,M}$	Capacità portante Mejerhoff
$Q_{Rd,EC7}$	Capacità portante EuroCodice 7
$Q_{Rd,V}$	Capacità portante Vesic
$Q_{Rd,T,PP}$	Capacità portante Terzaghi con correzione Paolucci-Pecker
$Q_{Rd,M,PP}$	Capacità portante Mejerhoff con correzione Paolucci-Pecker
$Q_{Rd,EC7,PP}$	Capacità portante EuroCodice 7 con correzione Paolucci-Pecker
$Q_{Rd,V,PP}$	Capacità portante Vesic con correzione Paolucci-Pecker
$Q_{Rd,T,MN,CI}$	Capacità portante Terzaghi con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,M,MN,CI}$	Capacità portante Mejerhoff con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,EC7,MN,CI}$	Capacità portante EuroCodice 7 con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,V,MN,CI}$	Capacità portante Vesic con correzione Maugeri-Novità con effetto cinematico+inerziale
$Q_{Rd,T,MN,C}$	Capacità portante Terzaghi con correzione Maugeri-Novità con effetto cinematico
$Q_{Rd,M,MN,C}$	Capacità portante Mejerhoff con correzione Maugeri-Novità con effetto cinematico
$Q_{Rd,EC7,MN,C}$	Capacità portante EuroCodice 7 con correzione Maugeri-Novità con effetto cinematico
$Q_{Rd,V,MN,C}$	Capacità portante Vesic con correzione Maugeri-Novità con effetto cinematico
F_x	Azione di scorrimento F_x
F_y	Azione di scorrimento F_y
$H_{Ed,d}=\sqrt{F_x,F_y}$	Azione di scorrimento totale $H_{Ed}= \sqrt{(F_x^2+F_y^2)}$

H_{Rd}	Resistenza allo scorrimento

Elemento	B_{Eq} [m]	H_{Eq} [m]	$H_{Trasporto}$ [m]	Comb.	N [kg]	M_x [kgm]	M_y [kgm]	Q_{Ed} [kg]	$(S/R)_{EC7,PP}$ [kg]	$(S/R)_{EC7,MN,C}$ [kg]	$(S/R)_{EC7,MN,CI}$ [kg]	F_x [kg]	F_y [kg]	H_{Ed} [kg]	$(S/R)_{Scor}$
12,18	0.90	6.70	0.50	3	40019.6	-5756.4	0.0	40019.6	0.269	0.371	0.269	0.0	0.0	0.0	0.000
				4	40630.2	-7752.7	0.0	40630.2	0.277	0.382	0.277	0.0	0.0	0.0	0.000
				5	39872.2	-4672.0	0.0	39872.2	0.266	0.366	0.266	0.0	0.0	0.0	0.000
				6	40356.5	-5738.8	0.0	40356.5	0.271	0.373	0.271	0.0	0.0	0.0	0.000
				7	41633.8	-9312.1	-0.0	41633.8	0.287	0.395	0.287	0.0	0.0	0.0	0.000
				8	42244.4	-11308.4	0.0	42244.4	0.296	0.406	0.296	0.0	0.0	0.0	0.000
				9	41907.5	-11325.9	0.0	41907.5	0.293	0.403	0.293	0.0	0.0	0.0	0.000
				10	42391.8	-12392.6	-0.0	42391.8	0.299	0.411	0.299	0.0	0.0	0.0	0.000
				11	39743.5	-5066.1	-0.0	39743.5	0.266	0.366	0.266	0.0	0.0	0.0	0.000
				12	40503.0	-7548.7	0.0	40503.0	0.276	0.380	0.276	0.0	0.0	0.0	0.000
				13	39563.6	-3727.3	-0.0	39563.6	0.262	0.361	0.262	0.0	0.0	0.0	0.000
				14	40168.8	-5062.3	0.0	40168.8	0.269	0.370	0.269	0.0	0.0	0.0	0.000
				15	41760.9	-9516.1	0.0	41760.9	0.288	0.397	0.288	0.0	0.0	0.0	0.000
				16	42520.4	-11998.6	0.0	42520.4	0.299	0.411	0.299	0.0	0.0	0.0	0.000
				17	42095.2	-12002.5	0.0	42095.2	0.296	0.407	0.296	0.0	0.0	0.0	0.000
				18	42700.4	-13337.5	0.0	42700.4	0.303	0.417	0.303	0.0	0.0	0.0	0.000
				24	40719.4	-7502.3	-0.0	40719.4	0.277	0.382	0.277	0.0	0.0	0.0	0.000
				25	40945.1	-8239.6	0.0	40945.1	0.280	0.386	0.280	0.0	0.0	0.0	0.000
				26	40666.0	-7105.3	0.0	40666.0	0.276	0.380	0.276	0.0	0.0	0.0	0.000
				27	40845.8	-7502.1	0.0	40845.8	0.278	0.383	0.278	0.0	0.0	0.0	0.000
				28	41318.9	-8825.0	-0.0	41318.9	0.284	0.391	0.284	0.0	0.0	0.0	0.000
				29	41544.5	-9562.5	0.1	41544.5	0.287	0.395	0.287	0.0	0.0	0.0	0.000
				30	41418.1	-9562.6	0.0	41418.1	0.286	0.394	0.286	0.0	0.0	0.0	0.000

				31	41598.0	-9959.4	-0.0	41598.0	0.288	0.397	0.288	0.0	0.0	0.0	0.000
				32	40081.3	-5865.0	0.0	40081.3	0.270	0.371	0.270	0.0	0.0	0.0	0.000
				33	40594.7	-7522.4	0.0	40594.7	0.277	0.381	0.277	0.0	0.0	0.0	0.000
				34	40038.2	-5218.4	-0.0	40038.2	0.268	0.369	0.268	0.0	0.0	0.0	0.000
				35	40514.5	-6321.6	-0.0	40514.5	0.274	0.376	0.274	0.0	0.0	0.0	0.000
				36	41669.3	-9542.2	0.0	41669.3	0.288	0.396	0.288	0.0	0.0	0.0	0.000
				37	42182.6	-11199.6	-0.0	42182.6	0.295	0.406	0.295	0.0	0.0	0.0	0.000
				38	41749.4	-10743.2	0.0	41749.4	0.291	0.400	0.291	0.0	0.0	0.0	0.000
				39	42225.8	-11846.3	0.0	42225.8	0.297	0.408	0.297	0.0	0.0	0.0	0.000
17,10	0.90	4.07	0.50	3	23537.6	831.6	0.0	23537.6	0.251	0.344	0.251	0.0	0.0	0.0	0.000
				4	23769.6	932.6	-0.0	23769.6	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				5	23476.5	483.5	-0.0	23476.5	0.249	0.341	0.249	0.0	0.0	0.0	0.000
				6	23656.2	286.2	-0.0	23656.2	0.250	0.342	0.250	0.0	0.0	0.0	0.000
				7	24136.3	174.0	-0.0	24136.3	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				8	24368.3	275.1	0.0	24368.3	0.257	0.352	0.257	0.0	0.0	0.0	0.000
				9	24249.7	820.4	0.0	24249.7	0.259	0.354	0.259	0.0	0.0	0.0	0.000
				10	24429.3	623.2	0.0	24429.3	0.259	0.355	0.259	0.0	0.0	0.0	0.000
				11	23436.4	899.2	0.0	23436.4	0.250	0.343	0.250	0.0	0.0	0.0	0.000
				12	23724.9	1024.9	0.0	23724.9	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				13	23360.5	466.4	0.0	23360.5	0.247	0.339	0.247	0.0	0.0	0.0	0.000
				14	23583.9	221.2	-0.0	23583.9	0.248	0.340	0.248	0.0	0.0	0.0	0.000
				15	24181.0	81.7	-0.0	24181.0	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				16	24469.4	207.4	-0.0	24469.4	0.258	0.353	0.258	0.0	0.0	0.0	0.000
				17	24322.0	885.4	-0.0	24322.0	0.260	0.355	0.260	0.0	0.0	0.0	0.000
				18	24545.4	640.2	0.0	24545.4	0.261	0.357	0.261	0.0	0.0	0.0	0.000
				24	23799.6	655.9	-0.0	23799.6	0.253	0.346	0.253	0.0	0.0	0.0	0.000

				25	23885.2	693.3	0.0	23885.2	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				26	23777.0	527.5	-0.0	23777.0	0.252	0.345	0.252	0.0	0.0	0.0	0.000
				27	23843.4	454.7	-0.0	23843.4	0.252	0.346	0.252	0.0	0.0	0.0	0.000
				28	24020.7	413.3	0.0	24020.7	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				29	24106.3	450.6	-0.0	24106.3	0.255	0.349	0.255	0.0	0.0	0.0	0.000
				30	24062.5	651.9	0.0	24062.5	0.256	0.350	0.256	0.0	0.0	0.0	0.000
				31	24128.9	579.1	-0.0	24128.9	0.256	0.351	0.256	0.0	0.0	0.0	0.000
				32	23608.5	780.0	-0.0	23608.5	0.252	0.344	0.252	0.0	0.0	0.0	0.000
				33	23800.6	863.8	-0.0	23800.6	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				34	23558.3	494.3	-0.0	23558.3	0.250	0.342	0.250	0.0	0.0	0.0	0.000
				35	23707.3	333.2	0.0	23707.3	0.250	0.343	0.250	0.0	0.0	0.0	0.000
				36	24105.3	242.8	-0.0	24105.3	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				37	24297.4	326.5	-0.0	24297.4	0.256	0.351	0.256	0.0	0.0	0.0	0.000
				38	24198.6	773.5	-0.0	24198.6	0.258	0.353	0.258	0.0	0.0	0.0	0.000
				39	24347.6	612.2	-0.0	24347.6	0.258	0.354	0.258	0.0	0.0	0.0	0.000
17,25	0.90	4.16	0.50	3	25657.5	320.7	0.0	25657.5	0.265	0.363	0.265	0.0	0.0	0.0	0.000
				4	25230.5	-609.4	-0.0	25230.5	0.262	0.359	0.262	0.0	0.0	0.0	0.000
				5	25507.9	1091.1	0.0	25507.9	0.267	0.366	0.267	0.0	0.0	0.0	0.000
				6	24952.7	821.3	-0.0	24952.7	0.260	0.356	0.260	0.0	0.0	0.0	0.000
				7	23806.6	-578.6	-0.0	23806.6	0.247	0.338	0.247	0.0	0.0	0.0	0.000
				8	23379.6	-1508.7	0.1	23379.6	0.247	0.339	0.247	0.0	0.0	0.0	0.000
				9	24084.5	-2009.3	0.1	24084.5	0.257	0.352	0.257	0.0	0.0	0.0	0.000
				10	23529.2	-2279.1	0.0	23529.2	0.253	0.346	0.253	0.0	0.0	0.0	0.000
				11	25934.8	543.6	0.0	25934.8	0.269	0.368	0.269	0.0	0.0	0.0	0.000
				12	25403.8	-613.1	-0.0	25403.8	0.264	0.361	0.264	0.0	0.0	0.0	0.000
				13	25748.9	1501.5	0.0	25748.9	0.272	0.372	0.272	0.0	0.0	0.0	0.000

				14	25058.4	1166.0	-0.0	25058.4	0.263	0.360	0.263	0.0	0.0	0.0	0.000
				15	23633.4	-574.9	-0.0	23633.4	0.245	0.336	0.245	0.0	0.0	0.0	0.000
				16	23102.4	-1731.5	0.0	23102.4	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				17	23978.7	-2354.0	-0.0	23978.7	0.258	0.353	0.258	0.0	0.0	0.0	0.000
				18	23288.3	-2689.5	-0.0	23288.3	0.252	0.346	0.252	0.0	0.0	0.0	0.000
				24	24939.1	-256.2	0.0	24939.1	0.257	0.352	0.257	0.0	0.0	0.0	0.000
				25	24781.4	-599.6	0.1	24781.4	0.257	0.352	0.257	0.0	0.0	0.0	0.000
				26	24883.9	28.2	0.1	24883.9	0.255	0.350	0.255	0.0	0.0	0.0	0.000
				27	24678.9	-71.4	0.0	24678.9	0.253	0.347	0.253	0.0	0.0	0.0	0.000
				28	24255.7	-588.4	0.0	24255.7	0.252	0.345	0.252	0.0	0.0	0.0	0.000
				29	24098.1	-931.8	-0.0	24098.1	0.252	0.345	0.252	0.0	0.0	0.0	0.000
				30	24358.3	-1116.6	-0.0	24358.3	0.255	0.350	0.255	0.0	0.0	0.0	0.000
				31	24153.3	-1216.2	0.0	24153.3	0.254	0.347	0.254	0.0	0.0	0.0	0.000
				32	25457.6	165.6	-0.0	25457.6	0.262	0.359	0.262	0.0	0.0	0.0	0.000
				33	25104.6	-604.2	-0.0	25104.6	0.260	0.357	0.260	0.0	0.0	0.0	0.000
				34	25335.8	801.3	0.0	25335.8	0.264	0.361	0.264	0.0	0.0	0.0	0.000
				35	24878.3	576.5	0.0	24878.3	0.258	0.353	0.258	0.0	0.0	0.0	0.000
				36	23932.6	-583.8	-0.0	23932.6	0.248	0.340	0.248	0.0	0.0	0.0	0.000
				37	23579.5	-1353.5	0.0	23579.5	0.249	0.340	0.249	0.0	0.0	0.0	0.000
				38	24158.9	-1764.5	0.0	24158.9	0.257	0.351	0.257	0.0	0.0	0.0	0.000
				39	23701.4	-1989.3	-0.0	23701.4	0.253	0.346	0.253	0.0	0.0	0.0	0.000
12,28	0.90	5.93	0.50	3	35453.2	2822.5	0.0	35453.2	0.264	0.363	0.264	0.0	0.0	0.0	0.000
				4	33780.6	1365.6	0.0	33780.6	0.249	0.342	0.249	0.0	0.0	0.0	0.000
				5	35999.4	3350.7	0.0	35999.4	0.270	0.371	0.270	0.0	0.0	0.0	0.000
				6	34794.9	2346.5	0.0	34794.9	0.258	0.355	0.258	0.0	0.0	0.0	0.000
				7	31438.2	-524.8	0.0	31438.2	0.230	0.316	0.230	0.0	0.0	0.0	0.000

				8	29765.6	-1981.8	0.0	29765.6	0.221	0.304	0.221	0.0	0.0	0.0	0.000
				9	30424.0	-1505.7	0.0	30424.0	0.225	0.309	0.225	0.0	0.0	0.0	0.000
				10	29219.5	-2510.0	0.0	29219.5	0.218	0.300	0.218	0.0	0.0	0.0	0.000
				11	36146.8	3409.5	0.0	36146.8	0.271	0.372	0.271	0.0	0.0	0.0	0.000
				12	34066.8	1597.6	0.0	34066.8	0.251	0.345	0.251	0.0	0.0	0.0	0.000
				13	36825.3	4065.1	0.0	36825.3	0.278	0.381	0.278	0.0	0.0	0.0	0.000
				14	35326.8	2815.2	0.0	35326.8	0.263	0.362	0.263	0.0	0.0	0.0	0.000
				15	31152.0	-756.9	0.0	31152.0	0.228	0.313	0.228	0.0	0.0	0.0	0.000
				16	29072.1	-2568.7	0.0	29072.1	0.217	0.299	0.217	0.0	0.0	0.0	0.000
				17	29892.0	-1974.4	0.0	29892.0	0.222	0.305	0.222	0.0	0.0	0.0	0.000
				18	28393.5	-3224.3	0.0	28393.5	0.214	0.294	0.214	0.0	0.0	0.0	0.000
				24	33659.7	1308.0	0.0	33659.7	0.248	0.340	0.248	0.0	0.0	0.0	0.000
				25	33042.1	769.9	0.0	33042.1	0.242	0.332	0.242	0.0	0.0	0.0	0.000
				26	33861.1	1502.7	0.0	33861.1	0.250	0.343	0.250	0.0	0.0	0.0	0.000
				27	33416.2	1131.5	0.0	33416.2	0.245	0.337	0.245	0.0	0.0	0.0	0.000
				28	32176.7	70.8	0.0	32176.7	0.234	0.321	0.234	0.0	0.0	0.0	0.000
				29	31559.1	-467.2	0.0	31559.1	0.230	0.317	0.230	0.0	0.0	0.0	0.000
				30	31802.6	-290.7	0.0	31802.6	0.232	0.318	0.232	0.0	0.0	0.0	0.000
				31	31357.7	-661.9	0.0	31357.7	0.229	0.315	0.229	0.0	0.0	0.0	0.000
				32	34980.5	2450.7	0.0	34980.5	0.260	0.357	0.260	0.0	0.0	0.0	0.000
				33	33599.1	1243.4	0.0	33599.1	0.247	0.340	0.247	0.0	0.0	0.0	0.000
				34	35415.8	2860.4	0.0	35415.8	0.264	0.363	0.264	0.0	0.0	0.0	0.000
				35	34407.5	2004.4	0.0	34407.5	0.255	0.350	0.255	0.0	0.0	0.0	0.000
				36	31619.7	-402.7	0.0	31619.7	0.231	0.317	0.231	0.0	0.0	0.0	0.000
				37	30238.3	-1609.9	0.0	30238.3	0.224	0.307	0.224	0.0	0.0	0.0	0.000
				38	30811.3	-1163.6	0.0	30811.3	0.227	0.311	0.227	0.0	0.0	0.0	0.000

				39	29803.0	-2019.6	0.0	29803.0	0.221	0.304	0.221	0.0	0.0	0.0	0.000
5,12	0.90	2.10	0.50	3	14775.5	-442.0	0.0	14775.5	0.300	0.406	0.300	0.0	0.0	0.0	0.000
				4	15490.3	-698.8	0.0	15490.3	0.318	0.431	0.318	0.0	0.0	0.0	0.000
				5	14117.7	-281.3	0.0	14117.7	0.284	0.384	0.284	0.0	0.0	0.0	0.000
				6	14268.6	-400.3	0.0	14268.6	0.289	0.391	0.289	0.0	0.0	0.0	0.000
				7	15278.5	-838.7	0.0	15278.5	0.317	0.429	0.317	0.0	0.0	0.0	0.000
				8	15993.3	-1095.4	0.0	15993.3	0.336	0.455	0.336	0.0	0.0	0.0	0.000
				9	16500.2	-1137.1	0.0	16500.2	0.347	0.469	0.347	0.0	0.0	0.0	0.000
				10	16651.1	-1256.1	0.0	16651.1	0.352	0.476	0.352	0.0	0.0	0.0	0.000
				11	14627.4	-362.3	0.0	14627.4	0.295	0.400	0.295	0.0	0.0	0.0	0.000
				12	15516.1	-681.7	0.0	15516.1	0.319	0.431	0.319	0.0	0.0	0.0	0.000
				13	13809.5	-162.4	0.0	13809.5	0.275	0.373	0.275	0.0	0.0	0.0	0.000
				14	13997.1	-310.4	0.0	13997.1	0.282	0.381	0.282	0.0	0.0	0.0	0.000
				15	15252.7	-855.8	0.0	15252.7	0.317	0.429	0.317	0.0	0.0	0.0	0.000
				16	16141.4	-1175.2	0.0	16141.4	0.341	0.461	0.341	0.0	0.0	0.0	0.000
				17	16771.7	-1227.1	0.0	16771.7	0.354	0.479	0.354	0.0	0.0	0.0	0.000
				18	16959.3	-1375.1	0.0	16959.3	0.361	0.488	0.361	0.0	0.0	0.0	0.000
				24	15159.9	-647.9	0.0	15159.9	0.311	0.421	0.311	0.0	0.0	0.0	0.000
				25	15423.6	-742.9	0.0	15423.6	0.318	0.430	0.318	0.0	0.0	0.0	0.000
				26	14917.2	-588.4	0.0	14917.2	0.305	0.413	0.305	0.0	0.0	0.0	0.000
				27	14972.8	-632.4	0.0	14972.8	0.307	0.416	0.307	0.0	0.0	0.0	0.000
				28	15345.3	-794.6	0.0	15345.3	0.317	0.430	0.317	0.0	0.0	0.0	0.000
				29	15608.9	-889.6	0.0	15608.9	0.325	0.439	0.325	0.0	0.0	0.0	0.000
				30	15796.0	-905.1	0.0	15796.0	0.329	0.444	0.329	0.0	0.0	0.0	0.000
				31	15851.6	-949.1	0.0	15851.6	0.330	0.447	0.330	0.0	0.0	0.0	0.000
				32	14897.7	-487.8	0.0	14897.7	0.303	0.410	0.303	0.0	0.0	0.0	0.000

				33	15476.2	-709.1	0.0	15476.2	0.318	0.431	0.318	0.0	0.0	0.0	0.000
				34	14361.0	-348.8	0.0	14361.0	0.290	0.392	0.290	0.0	0.0	0.0	0.000
				35	14479.5	-451.0	0.0	14479.5	0.294	0.398	0.294	0.0	0.0	0.0	0.000
				36	15292.6	-828.3	0.0	15292.6	0.317	0.429	0.317	0.0	0.0	0.0	0.000
				37	15871.1	-1049.7	0.0	15871.1	0.333	0.450	0.333	0.0	0.0	0.0	0.000
				38	16289.4	-1086.5	0.0	16289.4	0.342	0.462	0.342	0.0	0.0	0.0	0.000
				39	16407.8	-1188.7	0.0	16407.8	0.346	0.468	0.346	0.0	0.0	0.0	0.000
11,27	0.90	5.93	0.50	3	39367.3	13886.8	0.0	39367.3	0.324	0.444	0.324	0.0	0.0	0.0	0.000
				4	38078.8	12711.8	0.0	38078.8	0.311	0.427	0.311	0.0	0.0	0.0	0.000
				5	35345.2	7315.4	0.0	35345.2	0.275	0.378	0.275	0.0	0.0	0.0	0.000
				6	30609.2	507.8	0.0	30609.2	0.224	0.307	0.224	0.0	0.0	0.0	0.000
				7	23580.6	-8805.2	0.0	23580.6	0.195	0.268	0.195	0.0	0.0	0.0	0.000
				8	22292.1	-9980.2	0.0	22292.1	0.190	0.261	0.190	0.0	0.0	0.0	0.000
				9	31050.2	3398.8	0.0	31050.2	0.234	0.321	0.234	0.0	0.0	0.0	0.000
				10	26314.2	-3408.8	0.0	26314.2	0.200	0.274	0.200	0.0	0.0	0.0	0.000
				11	41446.0	16792.2	0.0	41446.0	0.347	0.477	0.347	0.0	0.0	0.0	0.000
				12	39843.7	15331.1	0.0	39843.7	0.331	0.455	0.331	0.0	0.0	0.0	0.000
				13	36444.7	8621.1	0.0	36444.7	0.287	0.394	0.287	0.0	0.0	0.0	0.000
				14	30555.6	156.0	0.0	30555.6	0.222	0.306	0.222	0.0	0.0	0.0	0.000
				15	21815.7	-11424.5	0.0	21815.7	0.192	0.263	0.192	0.0	0.0	0.0	0.000
				16	20213.4	-12885.6	0.0	20213.4	0.186	0.255	0.186	0.0	0.0	0.0	0.000
				17	31103.8	3750.6	0.0	31103.8	0.235	0.323	0.235	0.0	0.0	0.0	0.000
				18	25214.7	-4714.4	0.0	25214.7	0.195	0.268	0.195	0.0	0.0	0.0	0.000
				24	33981.6	6358.8	0.0	33981.6	0.263	0.361	0.263	0.0	0.0	0.0	0.000
				25	33505.9	5925.0	0.0	33505.9	0.258	0.355	0.258	0.0	0.0	0.0	0.000
				26	32496.8	3932.9	0.0	32496.8	0.246	0.338	0.246	0.0	0.0	0.0	0.000

				27	30748.3	1419.7	0.0	30748.3	0.227	0.312	0.227	0.0	0.0	0.0	0.000
				28	28153.5	-2018.4	0.0	28153.5	0.209	0.288	0.209	0.0	0.0	0.0	0.000
				29	27677.8	-2452.2	0.0	27677.8	0.207	0.285	0.207	0.0	0.0	0.0	0.000
				30	30911.1	2486.9	0.0	30911.1	0.231	0.317	0.231	0.0	0.0	0.0	0.000
				31	29162.6	-26.2	0.0	29162.6	0.212	0.291	0.212	0.0	0.0	0.0	0.000
				32	37863.6	11779.8	0.0	37863.6	0.306	0.421	0.306	0.0	0.0	0.0	0.000
				33	36800.0	10811.3	0.0	36800.0	0.296	0.406	0.296	0.0	0.0	0.0	0.000
				34	34552.9	6370.1	0.0	34552.9	0.267	0.367	0.267	0.0	0.0	0.0	0.000
				35	30651.6	764.7	0.0	30651.6	0.224	0.309	0.224	0.0	0.0	0.0	0.000
				36	24859.4	-6904.7	0.0	24859.4	0.199	0.273	0.199	0.0	0.0	0.0	0.000
				37	23795.8	-7873.1	0.0	23795.8	0.194	0.266	0.194	0.0	0.0	0.0	0.000
				38	31007.8	3141.9	0.0	31007.8	0.233	0.320	0.233	0.0	0.0	0.0	0.000
				39	27106.5	-2463.5	0.0	27106.5	0.203	0.279	0.203	0.0	0.0	0.0	0.000
4,11	0.90	2.10	0.50	3	14344.7	-749.0	0.0	14344.7	0.297	0.402	0.297	0.0	0.0	0.0	0.000
				4	14985.8	-1047.2	0.0	14985.8	0.315	0.427	0.315	0.0	0.0	0.0	0.000
				5	13748.4	-492.7	0.0	13748.4	0.280	0.379	0.280	0.0	0.0	0.0	0.000
				6	13878.4	-571.2	0.0	13878.4	0.284	0.385	0.284	0.0	0.0	0.0	0.000
				7	14777.9	-1010.6	0.0	14777.9	0.311	0.420	0.311	0.0	0.0	0.0	0.000
				8	15419.0	-1308.8	0.0	15419.0	0.329	0.445	0.329	0.0	0.0	0.0	0.000
				9	15885.3	-1486.6	0.0	15885.3	0.342	0.462	0.342	0.0	0.0	0.0	0.000
				10	16015.2	-1565.1	0.0	16015.2	0.346	0.468	0.346	0.0	0.0	0.0	0.000
				11	14213.9	-680.8	0.0	14213.9	0.293	0.397	0.293	0.0	0.0	0.0	0.000
				12	15011.1	-1051.6	0.0	15011.1	0.316	0.427	0.316	0.0	0.0	0.0	0.000
				13	13472.3	-362.1	0.0	13472.3	0.272	0.369	0.272	0.0	0.0	0.0	0.000
				14	13633.9	-459.7	0.0	13633.9	0.277	0.375	0.277	0.0	0.0	0.0	0.000
				15	14752.6	-1006.1	0.0	14752.6	0.310	0.419	0.310	0.0	0.0	0.0	0.000

				16	15549.8	-1376.9	0.0	15549.8	0.333	0.451	0.333	0.0	0.0	0.0	0.000
				17	16129.7	-1598.1	0.0	16129.7	0.349	0.472	0.349	0.0	0.0	0.0	0.000
				18	16291.3	-1695.7	0.0	16291.3	0.355	0.479	0.355	0.0	0.0	0.0	0.000
				24	14683.5	-925.5	0.0	14683.5	0.307	0.415	0.307	0.0	0.0	0.0	0.000
				25	14920.2	-1035.6	0.0	14920.2	0.314	0.425	0.314	0.0	0.0	0.0	0.000
				26	14463.3	-830.9	0.0	14463.3	0.301	0.407	0.301	0.0	0.0	0.0	0.000
				27	14511.3	-859.9	0.0	14511.3	0.302	0.409	0.302	0.0	0.0	0.0	0.000
				28	14843.4	-1022.1	0.0	14843.4	0.312	0.422	0.312	0.0	0.0	0.0	0.000
				29	15080.2	-1132.2	0.0	15080.2	0.319	0.431	0.319	0.0	0.0	0.0	0.000
				30	15252.4	-1197.9	0.0	15252.4	0.324	0.438	0.324	0.0	0.0	0.0	0.000
				31	15300.4	-1226.9	0.0	15300.4	0.325	0.440	0.325	0.0	0.0	0.0	0.000
				32	14437.3	-796.9	0.0	14437.3	0.300	0.405	0.300	0.0	0.0	0.0	0.000
				33	14969.2	-1043.7	0.0	14969.2	0.315	0.426	0.315	0.0	0.0	0.0	0.000
				34	13941.8	-585.1	0.0	13941.8	0.286	0.387	0.286	0.0	0.0	0.0	0.000
				35	14048.9	-650.2	0.0	14048.9	0.289	0.391	0.289	0.0	0.0	0.0	0.000
				36	14794.5	-1014.1	0.0	14794.5	0.311	0.421	0.311	0.0	0.0	0.0	0.000
				37	15326.4	-1260.8	0.0	15326.4	0.326	0.441	0.326	0.0	0.0	0.0	0.000
				38	15714.7	-1407.5	0.0	15714.7	0.337	0.456	0.337	0.0	0.0	0.0	0.000
				39	15821.9	-1472.7	0.0	15821.9	0.341	0.460	0.341	0.0	0.0	0.0	0.000
10,26	0.90	5.93	0.50	3	33686.8	3725.9	0.0	33686.8	0.254	0.349	0.254	0.0	0.0	0.0	0.000
				4	32901.5	2438.4	0.0	32901.5	0.245	0.337	0.245	0.0	0.0	0.0	0.000
				5	33091.5	4044.4	0.0	33091.5	0.250	0.344	0.250	0.0	0.0	0.0	0.000
				6	31796.0	3029.9	0.0	31796.0	0.238	0.328	0.238	0.0	0.0	0.0	0.000
				7	29368.4	344.0	0.0	29368.4	0.214	0.294	0.214	0.0	0.0	0.0	0.000
				8	28583.2	-943.5	0.0	28583.2	0.210	0.288	0.210	0.0	0.0	0.0	0.000
				9	30474.0	-247.4	0.0	30474.0	0.222	0.305	0.222	0.0	0.0	0.0	0.000

				10	29178.5	-1262.0	0.0	29178.5	0.215	0.295	0.215	0.0	0.0	0.0	0.000
				11	34308.2	4294.5	0.0	34308.2	0.260	0.357	0.260	0.0	0.0	0.0	0.000
				12	33331.7	2693.4	0.0	33331.7	0.249	0.342	0.249	0.0	0.0	0.0	0.000
				13	33568.0	4690.6	0.0	33568.0	0.256	0.351	0.256	0.0	0.0	0.0	0.000
				14	31957.0	3429.0	0.0	31957.0	0.241	0.331	0.241	0.0	0.0	0.0	0.000
				15	28938.3	89.1	0.0	28938.3	0.210	0.289	0.210	0.0	0.0	0.0	0.000
				16	27961.8	-1512.0	0.0	27961.8	0.207	0.284	0.207	0.0	0.0	0.0	0.000
				17	30313.0	-646.5	0.0	30313.0	0.222	0.305	0.222	0.0	0.0	0.0	0.000
				18	28702.0	-1908.1	0.0	28702.0	0.213	0.293	0.213	0.0	0.0	0.0	0.000
				24	32077.3	2253.4	0.0	32077.3	0.238	0.328	0.238	0.0	0.0	0.0	0.000
				25	31787.3	1778.1	0.0	31787.3	0.235	0.323	0.235	0.0	0.0	0.0	0.000
				26	31857.4	2370.9	0.0	31857.4	0.237	0.326	0.237	0.0	0.0	0.0	0.000
				27	31379.0	1996.1	0.0	31379.0	0.233	0.320	0.233	0.0	0.0	0.0	0.000
				28	30482.6	1004.4	0.0	30482.6	0.224	0.308	0.224	0.0	0.0	0.0	0.000
				29	30192.7	529.0	0.0	30192.7	0.221	0.303	0.221	0.0	0.0	0.0	0.000
				30	30891.0	786.3	0.0	30891.0	0.226	0.311	0.226	0.0	0.0	0.0	0.000
				31	30412.6	411.6	0.0	30412.6	0.222	0.305	0.222	0.0	0.0	0.0	0.000
				32	33245.7	3325.8	0.0	33245.7	0.250	0.343	0.250	0.0	0.0	0.0	0.000
				33	32597.3	2263.1	0.0	32597.3	0.242	0.333	0.242	0.0	0.0	0.0	0.000
				34	32751.5	3583.4	0.0	32751.5	0.247	0.339	0.247	0.0	0.0	0.0	0.000
				35	31679.6	2741.5	0.0	31679.6	0.237	0.325	0.237	0.0	0.0	0.0	0.000
				36	29672.7	519.4	0.0	29672.7	0.217	0.298	0.217	0.0	0.0	0.0	0.000
				37	29024.3	-543.4	0.0	29024.3	0.212	0.292	0.212	0.0	0.0	0.0	0.000
				38	30590.4	41.0	0.0	30590.4	0.222	0.306	0.222	0.0	0.0	0.0	0.000
				39	29518.5	-800.9	0.0	29518.5	0.216	0.297	0.216	0.0	0.0	0.0	0.000
3,10	0.90	2.10	0.50	3	14416.6	-751.1	0.0	14416.6	0.298	0.404	0.298	0.0	0.0	0.0	0.000

				4	15223.3	-1069.9	0.0	15223.3	0.321	0.434	0.321	0.0	0.0	0.0	0.000
				5	13645.7	-501.4	0.0	13645.7	0.278	0.377	0.278	0.0	0.0	0.0	0.000
				6	13791.8	-606.1	0.0	13791.8	0.283	0.383	0.283	0.0	0.0	0.0	0.000
				7	14903.4	-1100.3	0.0	14903.4	0.315	0.426	0.315	0.0	0.0	0.0	0.000
				8	15710.2	-1419.1	0.0	15710.2	0.337	0.456	0.337	0.0	0.0	0.0	0.000
				9	16334.9	-1564.1	0.0	16334.9	0.353	0.477	0.353	0.0	0.0	0.0	0.000
				10	16481.0	-1668.8	0.0	16481.0	0.358	0.483	0.358	0.0	0.0	0.0	0.000
				11	14259.0	-669.8	0.0	14259.0	0.294	0.397	0.294	0.0	0.0	0.0	0.000
				12	15262.2	-1066.2	0.0	15262.2	0.321	0.434	0.321	0.0	0.0	0.0	0.000
				13	13300.4	-359.2	0.0	13300.4	0.269	0.364	0.269	0.0	0.0	0.0	0.000
				14	13482.0	-489.4	0.0	13482.0	0.275	0.372	0.275	0.0	0.0	0.0	0.000
				15	14864.5	-1103.9	0.0	14864.5	0.314	0.425	0.314	0.0	0.0	0.0	0.000
				16	15867.8	-1500.4	0.0	15867.8	0.342	0.462	0.342	0.0	0.0	0.0	0.000
				17	16644.7	-1680.8	0.0	16644.7	0.361	0.488	0.361	0.0	0.0	0.0	0.000
				18	16826.4	-1811.0	0.0	16826.4	0.367	0.496	0.367	0.0	0.0	0.0	0.000
				24	14824.5	-961.8	0.0	14824.5	0.311	0.420	0.311	0.0	0.0	0.0	0.000
				25	15122.4	-1079.5	0.0	15122.4	0.319	0.431	0.319	0.0	0.0	0.0	0.000
				26	14539.8	-869.5	0.0	14539.8	0.303	0.410	0.303	0.0	0.0	0.0	0.000
				27	14593.8	-908.2	0.0	14593.8	0.305	0.413	0.305	0.0	0.0	0.0	0.000
				28	15004.3	-1090.7	0.0	15004.3	0.317	0.428	0.317	0.0	0.0	0.0	0.000
				29	15302.3	-1208.4	0.0	15302.3	0.325	0.439	0.325	0.0	0.0	0.0	0.000
				30	15532.9	-1262.0	0.0	15532.9	0.331	0.447	0.331	0.0	0.0	0.0	0.000
				31	15586.9	-1300.6	0.0	15586.9	0.332	0.449	0.332	0.0	0.0	0.0	0.000
				32	13903.7	-1047.9	0.0	13903.7	0.294	0.398	0.294	0.0	0.0	0.0	0.000
				33	14572.4	-1312.1	0.0	14572.4	0.313	0.423	0.313	0.0	0.0	0.0	0.000
				34	13701.2	-673.3	0.0	13701.2	0.283	0.383	0.283	0.0	0.0	0.0	0.000

				35	14196.4	-616.3	0.0	14196.4	0.291	0.394	0.291	0.0	0.0	0.0	0.000
				36	15554.3	-858.1	0.0	15554.3	0.323	0.437	0.323	0.0	0.0	0.0	0.000
				37	16223.1	-1122.2	0.0	16223.1	0.341	0.462	0.341	0.0	0.0	0.0	0.000
				38	15930.4	-1553.9	0.0	15930.4	0.344	0.466	0.344	0.0	0.0	0.0	0.000
				39	16425.6	-1496.9	0.0	16425.6	0.353	0.477	0.353	0.0	0.0	0.0	0.000
2,17	0.90	3.87	0.50	3	23494.1	-3055.2	0.0	23494.1	0.276	0.378	0.276	0.0	0.0	0.0	0.000
				4	24816.1	-4338.9	0.0	24816.1	0.299	0.409	0.299	0.0	0.0	0.0	0.000
				5	23681.4	-1332.8	0.0	23681.4	0.268	0.367	0.268	0.0	0.0	0.0	0.000
				6	25163.9	-1140.2	0.0	25163.9	0.283	0.388	0.283	0.0	0.0	0.0	0.000
				7	28435.9	-2413.2	0.0	28435.9	0.327	0.447	0.327	0.0	0.0	0.0	0.000
				8	29758.0	-3697.0	0.0	29758.0	0.349	0.477	0.349	0.0	0.0	0.0	0.000
				9	28088.1	-5612.0	0.0	28088.1	0.343	0.469	0.343	0.0	0.0	0.0	0.000
				10	29570.7	-5419.4	0.0	29570.7	0.358	0.489	0.358	0.0	0.0	0.0	0.000
				11	22731.1	-2977.1	0.0	22731.1	0.268	0.366	0.268	0.0	0.0	0.0	0.000
				12	24375.2	-4573.5	0.0	24375.2	0.296	0.404	0.296	0.0	0.0	0.0	0.000
				13	22964.0	-835.1	0.0	22964.0	0.257	0.352	0.257	0.0	0.0	0.0	0.000
				14	24807.7	-595.6	0.0	24807.7	0.276	0.378	0.276	0.0	0.0	0.0	0.000
				15	28876.9	-2178.6	0.0	28876.9	0.330	0.452	0.330	0.0	0.0	0.0	0.000
				16	30521.0	-3775.1	0.0	30521.0	0.358	0.489	0.358	0.0	0.0	0.0	0.000
				17	28444.3	-6156.6	0.0	28444.3	0.351	0.479	0.351	0.0	0.0	0.0	0.000
				18	30288.1	-5917.1	0.0	30288.1	0.369	0.505	0.369	0.0	0.0	0.0	0.000
				24	25469.4	-3257.7	0.0	25469.4	0.299	0.409	0.299	0.0	0.0	0.0	0.000
				25	25957.6	-3731.7	0.0	25957.6	0.308	0.421	0.308	0.0	0.0	0.0	0.000
				26	25538.6	-2621.6	0.0	25538.6	0.296	0.405	0.296	0.0	0.0	0.0	0.000
				27	26086.1	-2550.4	0.0	26086.1	0.302	0.413	0.302	0.0	0.0	0.0	0.000
				28	27294.4	-3020.5	0.0	27294.4	0.318	0.435	0.318	0.0	0.0	0.0	0.000

				29	27782.7	-3494.5	0.0	27782.7	0.326	0.446	0.326	0.0	0.0	0.0	0.000
				30	27166.0	-4201.7	0.0	27166.0	0.324	0.443	0.324	0.0	0.0	0.0	0.000
				31	27713.5	-4130.5	0.0	27713.5	0.329	0.450	0.329	0.0	0.0	0.0	0.000
				32	24026.1	-3114.1	0.0	24026.1	0.283	0.386	0.283	0.0	0.0	0.0	0.000
				33	25123.3	-4176.7	0.0	25123.3	0.301	0.412	0.301	0.0	0.0	0.0	0.000
				34	24182.0	-1685.9	0.0	24182.0	0.276	0.377	0.276	0.0	0.0	0.0	0.000
				35	25412.7	-1524.3	0.0	25412.7	0.288	0.394	0.288	0.0	0.0	0.0	0.000
				36	28128.7	-2575.4	0.0	28128.7	0.324	0.444	0.324	0.0	0.0	0.0	0.000
				37	29225.9	-3638.0	0.0	29225.9	0.343	0.469	0.343	0.0	0.0	0.0	0.000
				38	27839.3	-5227.9	0.0	27839.3	0.338	0.462	0.338	0.0	0.0	0.0	0.000
				39	29070.1	-5066.3	0.0	29070.1	0.350	0.479	0.350	0.0	0.0	0.0	0.000
16,24	0.90	4.16	0.50	3	24101.7	-1185.0	0.0	24101.7	0.253	0.347	0.253	0.0	0.0	0.0	0.000
				4	24284.2	-2196.7	0.0	24284.2	0.260	0.356	0.260	0.0	0.0	0.0	0.000
				5	23846.8	210.6	0.0	23846.8	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				6	23810.9	395.1	0.0	23810.9	0.246	0.337	0.246	0.0	0.0	0.0	0.000
				7	23982.0	-569.8	0.0	23982.0	0.249	0.341	0.249	0.0	0.0	0.0	0.000
				8	24164.5	-1581.4	0.0	24164.5	0.256	0.350	0.256	0.0	0.0	0.0	0.000
				9	24455.3	-3161.6	0.0	24455.3	0.267	0.365	0.267	0.0	0.0	0.0	0.000
				10	24419.4	-2977.0	0.0	24419.4	0.266	0.364	0.266	0.0	0.0	0.0	0.000
				11	24093.8	-1136.6	0.0	24093.8	0.253	0.346	0.253	0.0	0.0	0.0	0.000
				12	24320.9	-2394.7	0.0	24320.9	0.261	0.358	0.261	0.0	0.0	0.0	0.000
				13	23777.0	598.8	0.0	23777.0	0.247	0.338	0.247	0.0	0.0	0.0	0.000
				14	23732.4	828.3	0.0	23732.4	0.247	0.339	0.247	0.0	0.0	0.0	0.000
				15	23945.3	-371.8	0.0	23945.3	0.247	0.339	0.247	0.0	0.0	0.0	0.000
				16	24172.4	-1629.8	0.0	24172.4	0.256	0.351	0.256	0.0	0.0	0.0	0.000
				17	24533.8	-3594.8	0.0	24533.8	0.270	0.370	0.270	0.0	0.0	0.0	0.000

				18	24489.2	-3365.3	0.0	24489.2	0.268	0.367	0.268	0.0	0.0	0.0	0.000
				24	24121.4	-1310.0	0.0	24121.4	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				25	24188.9	-1683.6	0.0	24188.9	0.256	0.351	0.256	0.0	0.0	0.0	0.000
				26	24027.3	-794.7	0.0	24027.3	0.250	0.343	0.250	0.0	0.0	0.0	0.000
				27	24014.1	-726.5	0.0	24014.1	0.250	0.342	0.250	0.0	0.0	0.0	0.000
				28	24077.3	-1082.9	0.0	24077.3	0.252	0.345	0.252	0.0	0.0	0.0	0.000
				29	24144.8	-1456.5	0.0	24144.8	0.255	0.349	0.255	0.0	0.0	0.0	0.000
				30	24252.1	-2039.9	0.0	24252.1	0.259	0.355	0.259	0.0	0.0	0.0	0.000
				31	24238.8	-1971.8	0.0	24238.8	0.258	0.354	0.258	0.0	0.0	0.0	0.000
				32	24102.6	-1215.6	0.0	24102.6	0.253	0.347	0.253	0.0	0.0	0.0	0.000
				33	24254.2	-2053.9	0.0	24254.2	0.259	0.355	0.259	0.0	0.0	0.0	0.000
				34	23893.9	-61.4	0.0	23893.9	0.245	0.336	0.245	0.0	0.0	0.0	0.000
				35	23866.7	89.5	0.0	23866.7	0.245	0.336	0.245	0.0	0.0	0.0	0.000
				36	24011.9	-712.5	0.0	24011.9	0.250	0.342	0.250	0.0	0.0	0.0	0.000
				37	24163.6	-1550.9	0.0	24163.6	0.256	0.350	0.256	0.0	0.0	0.0	0.000
				38	24399.5	-2856.0	0.0	24399.5	0.265	0.362	0.265	0.0	0.0	0.0	0.000
				39	24372.3	-2705.1	0.0	24372.3	0.264	0.361	0.264	0.0	0.0	0.0	0.000
9,16	0.90	2.54	0.50	3	15816.4	-232.4	0.0	15816.4	0.264	0.358	0.264	0.0	0.0	0.0	0.000
				4	16598.1	-331.8	0.0	16598.1	0.278	0.377	0.278	0.0	0.0	0.0	0.000
				5	14739.7	-95.3	0.0	14739.7	0.244	0.332	0.244	0.0	0.0	0.0	0.000
				6	14598.5	-77.1	0.0	14598.5	0.242	0.328	0.242	0.0	0.0	0.0	0.000
				7	15345.7	-171.7	0.0	15345.7	0.255	0.347	0.255	0.0	0.0	0.0	0.000
				8	16127.3	-271.1	0.0	16127.3	0.269	0.366	0.269	0.0	0.0	0.0	0.000
				9	17345.2	-426.4	0.0	17345.2	0.291	0.396	0.291	0.0	0.0	0.0	0.000
				10	17204.0	-408.2	0.0	17204.0	0.289	0.392	0.289	0.0	0.0	0.0	0.000
				11	15778.6	-227.7	0.0	15778.6	0.263	0.357	0.263	0.0	0.0	0.0	0.000

				12	16750.6	-351.3	0.0	16750.6	0.280	0.381	0.280	0.0	0.0	0.0	0.000
				13	14439.6	-57.1	0.0	14439.6	0.239	0.325	0.239	0.0	0.0	0.0	0.000
				14	14264.0	-34.5	0.0	14264.0	0.235	0.320	0.235	0.0	0.0	0.0	0.000
				15	15193.1	-152.2	0.0	15193.1	0.252	0.343	0.252	0.0	0.0	0.0	0.000
				16	16165.2	-275.8	0.0	16165.2	0.270	0.367	0.270	0.0	0.0	0.0	0.000
				17	17679.8	-469.0	0.0	17679.8	0.297	0.404	0.297	0.0	0.0	0.0	0.000
				18	17504.2	-446.3	0.0	17504.2	0.294	0.400	0.294	0.0	0.0	0.0	0.000
				24	15914.5	-244.6	0.0	15914.5	0.265	0.361	0.265	0.0	0.0	0.0	0.000
				25	16203.1	-281.3	0.0	16203.1	0.271	0.368	0.271	0.0	0.0	0.0	0.000
				26	15516.9	-194.0	0.0	15516.9	0.258	0.351	0.258	0.0	0.0	0.0	0.000
				27	15464.7	-187.2	0.0	15464.7	0.257	0.350	0.257	0.0	0.0	0.0	0.000
				28	15740.6	-222.2	0.0	15740.6	0.262	0.356	0.262	0.0	0.0	0.0	0.000
				29	16029.3	-258.9	0.0	16029.3	0.267	0.364	0.267	0.0	0.0	0.0	0.000
				30	16479.0	-316.2	0.0	16479.0	0.276	0.375	0.276	0.0	0.0	0.0	0.000
				31	16426.9	-309.5	0.0	16426.9	0.275	0.373	0.275	0.0	0.0	0.0	0.000
				32	15843.1	-235.6	0.0	15843.1	0.264	0.359	0.264	0.0	0.0	0.0	0.000
				33	16491.1	-318.0	0.0	16491.1	0.276	0.375	0.276	0.0	0.0	0.0	0.000
				34	14950.5	-122.0	0.0	14950.5	0.248	0.337	0.248	0.0	0.0	0.0	0.000
				35	14833.3	-107.0	0.0	14833.3	0.246	0.334	0.246	0.0	0.0	0.0	0.000
				36	15452.7	-185.5	0.0	15452.7	0.257	0.349	0.257	0.0	0.0	0.0	0.000
				37	16100.7	-267.9	0.0	16100.7	0.269	0.365	0.269	0.0	0.0	0.0	0.000
				38	17110.4	-396.5	0.0	17110.4	0.287	0.390	0.287	0.0	0.0	0.0	0.000
				39	16993.3	-381.5	0.0	16993.3	0.285	0.387	0.285	0.0	0.0	0.0	0.000
1,9	0.90	1.33	0.50	3	9885.4	-280.9	0.0	9885.4	0.310	0.414	0.310	0.0	0.0	0.0	0.000
				4	10755.0	-363.3	0.0	10755.0	0.340	0.454	0.340	0.0	0.0	0.0	0.000
				5	8688.7	-167.5	0.0	8688.7	0.269	0.359	0.269	0.0	0.0	0.0	0.000

				6	8532.5	-152.6	0.0	8532.5	0.264	0.352	0.264	0.0	0.0	0.0	0.000
				7	9364.7	-231.4	0.0	9364.7	0.292	0.390	0.292	0.0	0.0	0.0	0.000
				8	10234.3	-313.7	0.0	10234.3	0.322	0.430	0.322	0.0	0.0	0.0	0.000
				9	11587.3	-442.1	0.0	11587.3	0.368	0.492	0.368	0.0	0.0	0.0	0.000
				10	11431.1	-427.2	0.0	11431.1	0.363	0.485	0.363	0.0	0.0	0.0	0.000
				11	9843.0	-276.9	0.0	9843.0	0.308	0.412	0.308	0.0	0.0	0.0	0.000
				12	10924.4	-379.4	0.0	10924.4	0.346	0.462	0.346	0.0	0.0	0.0	0.000
				13	8354.7	-135.8	0.0	8354.7	0.257	0.344	0.257	0.0	0.0	0.0	0.000
				14	8160.4	-117.3	0.0	8160.4	0.251	0.335	0.251	0.0	0.0	0.0	0.000
				15	9195.4	-215.3	0.0	9195.4	0.286	0.383	0.286	0.0	0.0	0.0	0.000
				16	10276.8	-317.7	0.0	10276.8	0.323	0.432	0.323	0.0	0.0	0.0	0.000
				17	11959.3	-477.3	0.0	11959.3	0.381	0.509	0.381	0.0	0.0	0.0	0.000
				18	11765.1	-458.8	0.0	11765.1	0.374	0.500	0.374	0.0	0.0	0.0	0.000
				24	9995.5	-291.3	0.0	9995.5	0.314	0.419	0.314	0.0	0.0	0.0	0.000
				25	10316.6	-321.7	0.0	10316.6	0.325	0.434	0.325	0.0	0.0	0.0	0.000
				26	9553.5	-249.4	0.0	9553.5	0.299	0.399	0.299	0.0	0.0	0.0	0.000
				27	9495.8	-243.9	0.0	9495.8	0.297	0.396	0.297	0.0	0.0	0.0	0.000
				28	9803.2	-273.0	0.0	9803.2	0.307	0.410	0.307	0.0	0.0	0.0	0.000
				29	10124.3	-303.4	0.0	10124.3	0.318	0.425	0.318	0.0	0.0	0.0	0.000
				30	10623.9	-350.8	0.0	10623.9	0.335	0.448	0.335	0.0	0.0	0.0	0.000
				31	10566.2	-345.3	0.0	10566.2	0.333	0.445	0.333	0.0	0.0	0.0	0.000
				32	9915.2	-283.7	0.0	9915.2	0.311	0.415	0.311	0.0	0.0	0.0	0.000
				33	10636.0	-352.0	0.0	10636.0	0.336	0.448	0.336	0.0	0.0	0.0	0.000
				34	8923.2	-189.7	0.0	8923.2	0.277	0.370	0.277	0.0	0.0	0.0	0.000
				35	8793.7	-177.3	0.0	8793.7	0.272	0.364	0.272	0.0	0.0	0.0	0.000
				36	9483.7	-242.7	0.0	9483.7	0.296	0.396	0.296	0.0	0.0	0.0	0.000

				37	10204.6	-310.9	0.0	10204.6	0.321	0.429	0.321	0.0	0.0	0.0	0.000
				38	11326.0	-417.3	0.0	11326.0	0.359	0.480	0.359	0.0	0.0	0.0	0.000
				39	11196.6	-405.0	0.0	11196.6	0.355	0.474	0.355	0.0	0.0	0.0	0.000
8,23	0.90	6.70	0.50	3	35536.2	-6747.4	0.0	35536.2	0.242	0.333	0.242	0.0	0.0	0.0	0.000
				4	37256.5	-8722.7	0.0	37256.5	0.258	0.354	0.258	0.0	0.0	0.0	0.000
				5	33156.3	-3993.0	0.0	33156.3	0.221	0.305	0.221	0.0	0.0	0.0	0.000
				6	32836.6	-3607.4	0.0	32836.6	0.219	0.301	0.219	0.0	0.0	0.0	0.000
				7	34470.6	-5461.9	0.0	34470.6	0.233	0.320	0.233	0.0	0.0	0.0	0.000
				8	36190.9	-7437.2	0.0	36190.9	0.248	0.341	0.248	0.0	0.0	0.0	0.000
				9	38890.5	-10577.3	0.0	38890.5	0.272	0.374	0.272	0.0	0.0	0.0	0.000
				10	38570.8	-10191.7	0.0	38570.8	0.269	0.370	0.269	0.0	0.0	0.0	0.000
				11	35456.5	-6663.3	0.0	35456.5	0.242	0.333	0.242	0.0	0.0	0.0	0.000
				12	37595.8	-9119.8	0.0	37595.8	0.261	0.359	0.261	0.0	0.0	0.0	0.000
				13	32496.8	-3238.0	0.0	32496.8	0.216	0.297	0.216	0.0	0.0	0.0	0.000
				14	32099.2	-2758.5	0.0	32099.2	0.212	0.292	0.212	0.0	0.0	0.0	0.000
				15	34131.3	-5064.9	0.0	34131.3	0.230	0.316	0.230	0.0	0.0	0.0	0.000
				16	36270.6	-7521.4	0.0	36270.6	0.249	0.342	0.249	0.0	0.0	0.0	0.000
				17	39627.9	-11426.2	0.0	39627.9	0.279	0.383	0.279	0.0	0.0	0.0	0.000
				18	39230.3	-10946.7	0.0	39230.3	0.275	0.379	0.275	0.0	0.0	0.0	0.000
				24	35742.7	-6964.9	0.0	35742.7	0.244	0.336	0.244	0.0	0.0	0.0	0.000
				25	36377.9	-7694.4	0.0	36377.9	0.250	0.344	0.250	0.0	0.0	0.0	0.000
				26	34863.8	-5947.8	0.0	34863.8	0.236	0.325	0.236	0.0	0.0	0.0	0.000
				27	34745.8	-5805.4	0.0	34745.8	0.235	0.324	0.235	0.0	0.0	0.0	0.000
				28	35349.2	-6490.3	0.0	35349.2	0.241	0.331	0.241	0.0	0.0	0.0	0.000
				29	35984.4	-7219.7	0.0	35984.4	0.246	0.339	0.246	0.0	0.0	0.0	0.000
				30	36981.4	-8379.3	0.0	36981.4	0.255	0.351	0.255	0.0	0.0	0.0	0.000

				31	36863.3	-8236.9	0.0	36863.3	0.254	0.350	0.254	0.0	0.0	0.0	0.000
				32	35592.9	-6803.8	0.0	35592.9	0.243	0.334	0.243	0.0	0.0	0.0	0.000
				33	37019.0	-8441.4	0.0	37019.0	0.256	0.352	0.256	0.0	0.0	0.0	0.000
				34	33619.3	-4522.1	0.0	33619.3	0.226	0.310	0.226	0.0	0.0	0.0	0.000
				35	33353.9	-4204.0	0.0	33353.9	0.223	0.307	0.223	0.0	0.0	0.0	0.000
				36	34708.1	-5743.3	0.0	34708.1	0.235	0.323	0.235	0.0	0.0	0.0	0.000
				37	36134.2	-7380.8	0.0	36134.2	0.248	0.341	0.248	0.0	0.0	0.0	0.000
				38	38373.2	-9980.7	0.0	38373.2	0.268	0.368	0.268	0.0	0.0	0.0	0.000
				39	38107.8	-9662.5	0.0	38107.8	0.265	0.365	0.265	0.0	0.0	0.0	0.000
15,22	0.90	5.20	0.50	3	28584.9	-3051.9	0.0	28584.9	0.246	0.337	0.246	0.0	0.0	0.0	0.000
				4	29582.1	-4060.8	0.0	29582.1	0.258	0.353	0.258	0.0	0.0	0.0	0.000
				5	27274.6	-1551.0	0.0	27274.6	0.230	0.316	0.230	0.0	0.0	0.0	0.000
				6	27148.8	-1273.4	0.0	27148.8	0.228	0.313	0.228	0.0	0.0	0.0	0.000
				7	28165.3	-2126.7	0.0	28165.3	0.239	0.329	0.239	0.0	0.0	0.0	0.000
				8	29162.6	-3135.7	0.0	29162.6	0.251	0.344	0.251	0.0	0.0	0.0	0.000
				9	30598.7	-4914.1	0.0	30598.7	0.269	0.369	0.269	0.0	0.0	0.0	0.000
				10	30472.8	-4636.5	0.0	30472.8	0.267	0.366	0.267	0.0	0.0	0.0	0.000
				11	28513.8	-3042.5	0.0	28513.8	0.245	0.337	0.245	0.0	0.0	0.0	0.000
				12	29753.9	-4297.3	0.0	29753.9	0.260	0.356	0.260	0.0	0.0	0.0	0.000
				13	26884.9	-1175.4	0.0	26884.9	0.226	0.310	0.226	0.0	0.0	0.0	0.000
				14	26728.8	-829.7	0.0	26728.8	0.223	0.307	0.223	0.0	0.0	0.0	0.000
				15	27993.5	-1890.3	0.0	27993.5	0.237	0.326	0.237	0.0	0.0	0.0	0.000
				16	29233.7	-3145.0	0.0	29233.7	0.252	0.345	0.252	0.0	0.0	0.0	0.000
				17	31018.6	-5357.8	0.0	31018.6	0.274	0.376	0.274	0.0	0.0	0.0	0.000
				18	30862.5	-5012.1	0.0	30862.5	0.271	0.372	0.271	0.0	0.0	0.0	0.000
				24	28766.8	-3078.6	0.0	28766.8	0.247	0.340	0.247	0.0	0.0	0.0	0.000

				25	29135.0	-3451.2	0.0	29135.0	0.252	0.346	0.252	0.0	0.0	0.0	0.000
				26	28283.1	-2524.1	0.0	28283.1	0.242	0.332	0.242	0.0	0.0	0.0	0.000
				27	28236.8	-2421.5	0.0	28236.8	0.241	0.331	0.241	0.0	0.0	0.0	0.000
				28	28612.4	-2736.4	0.0	28612.4	0.245	0.336	0.245	0.0	0.0	0.0	0.000
				29	28980.6	-3108.9	0.0	28980.6	0.249	0.342	0.249	0.0	0.0	0.0	0.000
				30	29510.6	-3766.1	0.0	29510.6	0.256	0.351	0.256	0.0	0.0	0.0	0.000
				31	29464.3	-3663.4	0.0	29464.3	0.255	0.350	0.255	0.0	0.0	0.0	0.000
				32	28616.4	-3080.0	0.0	28616.4	0.246	0.338	0.246	0.0	0.0	0.0	0.000
				33	29443.2	-3916.4	0.0	29443.2	0.256	0.351	0.256	0.0	0.0	0.0	0.000
				34	27542.6	-1821.0	0.0	27542.6	0.233	0.320	0.233	0.0	0.0	0.0	0.000
				35	27449.0	-1578.4	0.0	27449.0	0.232	0.318	0.232	0.0	0.0	0.0	0.000
				36	28304.3	-2271.1	0.0	28304.3	0.241	0.331	0.241	0.0	0.0	0.0	0.000
				37	29131.0	-3107.6	0.0	29131.0	0.251	0.344	0.251	0.0	0.0	0.0	0.000
				38	30298.4	-4609.1	0.0	30298.4	0.265	0.364	0.265	0.0	0.0	0.0	0.000
				39	30204.8	-4366.5	0.0	30204.8	0.264	0.362	0.264	0.0	0.0	0.0	0.000
7,15	0.90	1.50	0.50	3	12047.9	-537.2	0.0	12047.9	0.344	0.461	0.344	0.0	0.0	0.0	0.000
				4	13667.4	-790.6	0.0	13667.4	0.397	0.532	0.397	0.0	0.0	0.0	0.000
				5	9789.5	-182.8	0.0	9789.5	0.270	0.363	0.270	0.0	0.0	0.0	0.000
				6	9473.3	-132.4	0.0	9473.3	0.260	0.349	0.260	0.0	0.0	0.0	0.000
				7	10993.8	-369.3	0.0	10993.8	0.309	0.415	0.309	0.0	0.0	0.0	0.000
				8	12613.3	-622.7	0.0	12613.3	0.362	0.486	0.362	0.0	0.0	0.0	0.000
				9	15187.9	-1027.4	0.0	15187.9	0.447	0.599	0.447	0.0	0.0	0.0	0.000
				10	14871.7	-977.1	0.0	14871.7	0.437	0.585	0.437	0.0	0.0	0.0	0.000
				11	11979.0	-526.7	0.0	11979.0	0.342	0.458	0.342	0.0	0.0	0.0	0.000
				12	13993.0	-841.9	0.0	13993.0	0.408	0.546	0.408	0.0	0.0	0.0	0.000
				13	9170.5	-86.0	0.0	9170.5	0.250	0.336	0.250	0.0	0.0	0.0	0.000

				14	8777.2	-23.4	0.0	8777.2	0.238	0.319	0.238	0.0	0.0	0.0	0.000
				15	10668.2	-318.0	0.0	10668.2	0.299	0.401	0.299	0.0	0.0	0.0	0.000
				16	12682.2	-633.1	0.0	12682.2	0.365	0.489	0.365	0.0	0.0	0.0	0.000
				17	15884.0	-1136.5	0.0	15884.0	0.470	0.629	0.470	0.0	0.0	0.0	0.000
				18	15490.7	-1073.8	0.0	15490.7	0.457	0.612	0.457	0.0	0.0	0.0	0.000
				24	12226.2	-564.1	0.0	12226.2	0.350	0.469	0.350	0.0	0.0	0.0	0.000
				25	12824.2	-657.7	0.0	12824.2	0.369	0.495	0.369	0.0	0.0	0.0	0.000
				26	11392.2	-433.3	0.0	11392.2	0.322	0.432	0.322	0.0	0.0	0.0	0.000
				27	11275.4	-414.7	0.0	11275.4	0.319	0.427	0.319	0.0	0.0	0.0	0.000
				28	11836.9	-502.2	0.0	11836.9	0.337	0.452	0.337	0.0	0.0	0.0	0.000
				29	12435.0	-595.7	0.0	12435.0	0.357	0.478	0.357	0.0	0.0	0.0	0.000
				30	13385.8	-745.2	0.0	13385.8	0.388	0.520	0.388	0.0	0.0	0.0	0.000
				31	13269.0	-726.6	0.0	13269.0	0.384	0.514	0.384	0.0	0.0	0.0	0.000
				32	12096.2	-544.4	0.0	12096.2	0.346	0.463	0.346	0.0	0.0	0.0	0.000
				33	13438.9	-754.5	0.0	13438.9	0.390	0.522	0.390	0.0	0.0	0.0	0.000
				34	10223.9	-250.7	0.0	10223.9	0.284	0.382	0.284	0.0	0.0	0.0	0.000
				35	9961.8	-209.0	0.0	9961.8	0.276	0.370	0.276	0.0	0.0	0.0	0.000
				36	11222.3	-405.4	0.0	11222.3	0.317	0.425	0.317	0.0	0.0	0.0	0.000
				37	12565.0	-615.5	0.0	12565.0	0.361	0.484	0.361	0.0	0.0	0.0	0.000
				38	14699.4	-950.9	0.0	14699.4	0.431	0.577	0.431	0.0	0.0	0.0	0.000
				39	14437.3	-909.2	0.0	14437.3	0.422	0.566	0.422	0.0	0.0	0.0	0.000
13,20	0.90	5.20	0.50	3	30646.4	-6696.7	0.0	30646.4	0.276	0.378	0.276	0.0	0.0	0.0	0.000
				4	33719.3	-9270.2	0.0	33719.3	0.310	0.426	0.310	0.0	0.0	0.0	0.000
				5	26848.4	-2610.0	0.0	26848.4	0.230	0.316	0.230	0.0	0.0	0.0	0.000
				6	26665.9	-1680.7	0.0	26665.9	0.225	0.310	0.225	0.0	0.0	0.0	0.000
				7	30037.9	-3599.0	0.0	30037.9	0.260	0.356	0.260	0.0	0.0	0.0	0.000

				8	33110.8	-6172.5	0.0	33110.8	0.294	0.403	0.294	0.0	0.0	0.0	0.000
				9	37091.3	-11188.5	0.0	37091.3	0.345	0.474	0.345	0.0	0.0	0.0	0.000
				10	36908.8	-10259.2	0.0	36908.8	0.340	0.467	0.340	0.0	0.0	0.0	0.000
				11	30349.4	-6758.1	0.0	30349.4	0.273	0.375	0.273	0.0	0.0	0.0	0.000
				12	34170.8	-9958.5	0.0	34170.8	0.317	0.434	0.317	0.0	0.0	0.0	0.000
				13	25623.9	-1677.7	0.0	25623.9	0.217	0.298	0.217	0.0	0.0	0.0	0.000
				14	25395.0	-523.4	0.0	25395.0	0.211	0.290	0.211	0.0	0.0	0.0	0.000
				15	29586.4	-2910.7	0.0	29586.4	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				16	33407.8	-6111.1	0.0	33407.8	0.296	0.406	0.296	0.0	0.0	0.0	0.000
				17	38362.2	-12345.8	0.0	38362.2	0.360	0.494	0.360	0.0	0.0	0.0	0.000
				18	38133.3	-11191.5	0.0	38133.3	0.354	0.485	0.354	0.0	0.0	0.0	0.000
				24	31424.7	-6530.5	0.0	31424.7	0.281	0.386	0.281	0.0	0.0	0.0	0.000
				25	32559.5	-7480.8	0.0	32559.5	0.294	0.404	0.294	0.0	0.0	0.0	0.000
				26	30021.3	-5022.0	0.0	30021.3	0.264	0.363	0.264	0.0	0.0	0.0	0.000
				27	29953.2	-4679.4	0.0	29953.2	0.263	0.360	0.263	0.0	0.0	0.0	0.000
				28	31197.7	-5388.4	0.0	31197.7	0.275	0.378	0.275	0.0	0.0	0.0	0.000
				29	32332.5	-6338.7	0.0	32332.5	0.288	0.395	0.288	0.0	0.0	0.0	0.000
				30	33804.0	-8189.8	0.0	33804.0	0.307	0.421	0.307	0.0	0.0	0.0	0.000
				31	33735.9	-7847.2	0.0	33735.9	0.305	0.419	0.305	0.0	0.0	0.0	0.000
				32	30940.4	-6586.1	0.0	30940.4	0.278	0.381	0.278	0.0	0.0	0.0	0.000
				33	33489.0	-8718.2	0.0	33489.0	0.306	0.420	0.306	0.0	0.0	0.0	0.000
				34	27731.6	-3246.3	0.0	27731.6	0.239	0.329	0.239	0.0	0.0	0.0	0.000
				35	27529.9	-2515.7	0.0	27529.9	0.235	0.323	0.235	0.0	0.0	0.0	0.000
				36	30268.2	-4150.9	0.0	30268.2	0.263	0.362	0.263	0.0	0.0	0.0	0.000
				37	32816.9	-6283.1	0.0	32816.9	0.292	0.401	0.292	0.0	0.0	0.0	0.000
				38	36227.3	-10353.4	0.0	36227.3	0.335	0.459	0.335	0.0	0.0	0.0	0.000

				39	36025.6	-9622.9	0.0	36025.6	0.331	0.453	0.331	0.0	0.0	0.0	0.000
16,17	0.90	6.39	0.50	3	34185.4	-532.7	-0.0	34185.4	0.232	0.319	0.232	0.0	0.0	0.0	0.000
				4	35003.7	3.9	0.0	35003.7	0.236	0.325	0.236	0.0	0.0	0.0	0.000
				5	32914.0	-1301.9	-0.0	32914.0	0.225	0.309	0.225	0.0	0.0	0.0	0.000
				6	32642.5	-1424.6	-0.0	32642.5	0.223	0.307	0.223	0.0	0.0	0.0	0.000
				7	33280.5	-941.8	-0.0	33280.5	0.227	0.312	0.227	0.0	0.0	0.0	0.000
				8	34098.8	-405.2	-0.0	34098.8	0.231	0.318	0.231	0.0	0.0	0.0	0.000
				9	35641.7	486.8	0.0	35641.7	0.242	0.332	0.242	0.0	0.0	0.0	0.000
				10	35370.2	364.0	0.0	35370.2	0.239	0.329	0.239	0.0	0.0	0.0	0.000
				11	34195.0	-549.2	-0.0	34195.0	0.232	0.319	0.232	0.0	0.0	0.0	0.000
				12	35212.7	118.0	0.0	35212.7	0.238	0.327	0.238	0.0	0.0	0.0	0.000
				13	32614.5	-1505.0	-0.0	32614.5	0.223	0.307	0.223	0.0	0.0	0.0	0.000
				14	32277.4	-1657.0	-0.0	32277.4	0.221	0.304	0.221	0.0	0.0	0.0	0.000
				15	33071.5	-1055.9	-0.0	33071.5	0.225	0.310	0.225	0.0	0.0	0.0	0.000
				16	34089.2	-388.7	-0.0	34089.2	0.231	0.318	0.231	0.0	0.0	0.0	0.000
				17	36006.8	719.2	0.0	36006.8	0.245	0.336	0.245	0.0	0.0	0.0	0.000
				18	35669.8	567.1	0.0	35669.8	0.242	0.333	0.242	0.0	0.0	0.0	0.000
				24	34157.8	-492.8	-0.0	34157.8	0.232	0.319	0.232	0.0	0.0	0.0	0.000
				25	34460.0	-294.7	-0.0	34460.0	0.233	0.321	0.233	0.0	0.0	0.0	0.000
				26	33688.4	-776.5	-0.0	33688.4	0.229	0.315	0.229	0.0	0.0	0.0	0.000
				27	33588.3	-821.6	-0.0	33588.3	0.228	0.314	0.228	0.0	0.0	0.0	0.000
				28	33824.2	-643.2	-0.0	33824.2	0.230	0.316	0.230	0.0	0.0	0.0	0.000
				29	34126.5	-445.1	-0.0	34126.5	0.231	0.318	0.231	0.0	0.0	0.0	0.000
				30	34695.9	-116.3	-0.0	34695.9	0.234	0.322	0.234	0.0	0.0	0.0	0.000
				31	34595.8	-161.4	-0.0	34595.8	0.234	0.322	0.234	0.0	0.0	0.0	0.000
				32	34152.7	-544.9	-0.0	34152.7	0.232	0.319	0.232	0.0	0.0	0.0	0.000

				33	34833.8	-102.9	-0.0	34833.8	0.235	0.324	0.235	0.0	0.0	0.0	0.000
				34	33112.2	-1162.2	-0.0	33112.2	0.226	0.311	0.226	0.0	0.0	0.0	0.000
				35	32901.5	-1249.3	-0.0	32901.5	0.225	0.309	0.225	0.0	0.0	0.0	0.000
				36	33450.4	-835.1	-0.0	33450.4	0.228	0.313	0.228	0.0	0.0	0.0	0.000
				37	34131.5	-393.1	-0.0	34131.5	0.231	0.318	0.231	0.0	0.0	0.0	0.000
				38	35382.7	311.3	0.0	35382.7	0.239	0.329	0.239	0.0	0.0	0.0	0.000
				39	35172.0	224.2	0.0	35172.0	0.238	0.327	0.238	0.0	0.0	0.0	0.000
14,15	0.90	4.08	0.50	3	27517.5	337.3	0.0	27517.5	0.289	0.396	0.289	0.0	0.0	0.0	0.000
				4	29689.6	-214.6	-0.0	29689.6	0.311	0.426	0.311	0.0	0.0	0.0	0.000
				5	24595.9	973.2	0.0	24595.9	0.262	0.359	0.262	0.0	0.0	0.0	0.000
				6	24263.8	966.5	0.0	24263.8	0.259	0.354	0.259	0.0	0.0	0.0	0.000
				7	26410.4	314.8	0.0	26410.4	0.278	0.380	0.278	0.0	0.0	0.0	0.000
				8	28582.5	-237.0	-0.0	28582.5	0.300	0.411	0.300	0.0	0.0	0.0	0.000
				9	31836.2	-866.2	-0.0	31836.2	0.337	0.462	0.337	0.0	0.0	0.0	0.000
				10	31504.1	-872.9	-0.0	31504.1	0.334	0.457	0.334	0.0	0.0	0.0	0.000
				11	27388.0	406.9	0.0	27388.0	0.288	0.395	0.288	0.0	0.0	0.0	0.000
				12	30089.2	-279.3	-0.0	30089.2	0.316	0.433	0.316	0.0	0.0	0.0	0.000
				13	23754.7	1197.8	0.0	23754.7	0.254	0.348	0.254	0.0	0.0	0.0	0.000
				14	23341.5	1189.7	0.0	23341.5	0.250	0.342	0.250	0.0	0.0	0.0	0.000
				15	26010.9	379.6	0.0	26010.9	0.274	0.375	0.274	0.0	0.0	0.0	0.000
				16	28712.0	-306.6	-0.0	28712.0	0.302	0.413	0.302	0.0	0.0	0.0	0.000
				17	32758.5	-1089.4	-0.0	32758.5	0.348	0.476	0.348	0.0	0.0	0.0	0.000
				18	32345.4	-1097.6	-0.0	32345.4	0.344	0.471	0.344	0.0	0.0	0.0	0.000
				24	27853.5	156.0	0.0	27853.5	0.292	0.400	0.292	0.0	0.0	0.0	0.000
				25	28655.5	-47.7	-0.0	28655.5	0.300	0.411	0.300	0.0	0.0	0.0	0.000
				26	26774.6	390.8	0.0	26774.6	0.282	0.386	0.282	0.0	0.0	0.0	0.000

				27	26651.9	388.4	0.0	26651.9	0.281	0.384	0.281	0.0	0.0	0.0	0.000
				28	27444.5	148.0	0.0	27444.5	0.288	0.394	0.288	0.0	0.0	0.0	0.000
				29	28246.5	-55.7	-0.0	28246.5	0.296	0.405	0.296	0.0	0.0	0.0	0.000
				30	29448.1	-288.1	-0.0	29448.1	0.309	0.423	0.309	0.0	0.0	0.0	0.000
				31	29325.4	-290.6	-0.0	29325.4	0.308	0.422	0.308	0.0	0.0	0.0	0.000
				32	27615.6	278.8	0.0	27615.6	0.290	0.397	0.290	0.0	0.0	0.0	0.000
				33	29413.0	-175.1	-0.0	29413.0	0.308	0.422	0.308	0.0	0.0	0.0	0.000
				34	25193.6	807.2	0.0	25193.6	0.267	0.366	0.267	0.0	0.0	0.0	0.000
				35	24915.0	806.2	0.0	24915.0	0.264	0.362	0.264	0.0	0.0	0.0	0.000
				36	26687.0	275.4	0.0	26687.0	0.280	0.384	0.280	0.0	0.0	0.0	0.000
				37	28484.4	-178.5	-0.0	28484.4	0.299	0.409	0.299	0.0	0.0	0.0	0.000
				38	31185.1	-705.9	-0.0	31185.1	0.330	0.451	0.330	0.0	0.0	0.0	0.000
				39	30906.5	-707.0	-0.0	30906.5	0.327	0.447	0.327	0.0	0.0	0.0	0.000
13,14	0.90	4.52	0.50	3	31251.5	568.9	0.0	31251.5	0.298	0.409	0.298	0.0	0.0	0.0	0.000
				4	33947.7	1787.2	0.0	33947.7	0.329	0.451	0.329	0.0	0.0	0.0	0.000
				5	27118.6	-866.4	-0.0	27118.6	0.260	0.357	0.260	0.0	0.0	0.0	0.000
				6	26272.3	-878.3	-0.0	26272.3	0.252	0.346	0.252	0.0	0.0	0.0	0.000
				7	28430.4	529.2	0.0	28430.4	0.271	0.372	0.271	0.0	0.0	0.0	0.000
				8	31126.6	1747.5	0.0	31126.6	0.302	0.414	0.302	0.0	0.0	0.0	0.000
				9	36105.9	3194.7	0.0	36105.9	0.355	0.487	0.355	0.0	0.0	0.0	0.000
				10	35259.5	3182.8	0.0	35259.5	0.347	0.476	0.347	0.0	0.0	0.0	0.000
				11	31265.8	425.6	0.0	31265.8	0.298	0.408	0.298	0.0	0.0	0.0	0.000
				12	34618.8	1940.7	0.0	34618.8	0.336	0.460	0.336	0.0	0.0	0.0	0.000
				13	26126.7	-1359.5	-0.0	26126.7	0.253	0.347	0.253	0.0	0.0	0.0	0.000
				14	25074.7	-1374.5	-0.0	25074.7	0.243	0.333	0.243	0.0	0.0	0.0	0.000
				15	27759.3	375.7	0.0	27759.3	0.264	0.362	0.264	0.0	0.0	0.0	0.000

				16	31112.3	1890.7	0.0	31112.3	0.302	0.414	0.302	0.0	0.0	0.0	0.000
				17	37303.4	3690.8	0.0	37303.4	0.369	0.505	0.369	0.0	0.0	0.0	0.000
				18	36251.4	3675.8	0.0	36251.4	0.359	0.492	0.359	0.0	0.0	0.0	0.000
				24	31211.8	940.7	0.0	31211.8	0.299	0.410	0.299	0.0	0.0	0.0	0.000
				25	32207.5	1390.6	0.0	32207.5	0.311	0.426	0.311	0.0	0.0	0.0	0.000
				26	29685.7	410.6	0.0	29685.7	0.283	0.387	0.283	0.0	0.0	0.0	0.000
				27	29373.4	406.2	0.0	29373.4	0.280	0.383	0.280	0.0	0.0	0.0	0.000
				28	30170.6	925.8	0.0	30170.6	0.289	0.397	0.289	0.0	0.0	0.0	0.000
				29	31166.3	1375.7	0.0	31166.3	0.301	0.412	0.301	0.0	0.0	0.0	0.000
				30	33004.7	1910.2	0.0	33004.7	0.320	0.439	0.320	0.0	0.0	0.0	0.000
				31	32692.4	1905.8	0.0	32692.4	0.317	0.435	0.317	0.0	0.0	0.0	0.000
				32	31217.3	679.1	0.0	31217.3	0.298	0.409	0.298	0.0	0.0	0.0	0.000
				33	33453.9	1687.9	0.0	33453.9	0.324	0.444	0.324	0.0	0.0	0.0	0.000
				34	27805.4	-515.5	-0.0	27805.4	0.265	0.364	0.265	0.0	0.0	0.0	0.000
				35	27117.4	-530.7	-0.0	27117.4	0.259	0.355	0.259	0.0	0.0	0.0	0.000
				36	28924.2	628.5	0.0	28924.2	0.276	0.379	0.276	0.0	0.0	0.0	0.000
				37	31160.8	1637.3	0.0	31160.8	0.302	0.414	0.302	0.0	0.0	0.0	0.000
				38	35260.7	2847.1	0.0	35260.7	0.346	0.474	0.346	0.0	0.0	0.0	0.000
				39	34572.8	2831.9	0.0	34572.8	0.339	0.465	0.339	0.0	0.0	0.0	0.000
11,12	0.90	3.61	0.50	3	22610.8	-811.7	-0.0	22610.8	0.271	0.371	0.271	0.0	0.0	0.0	0.000
				4	22385.3	-724.2	-0.0	22385.3	0.268	0.366	0.268	0.0	0.0	0.0	0.000
				5	22653.1	-862.7	-0.0	22653.1	0.272	0.372	0.272	0.0	0.0	0.0	0.000
				6	22463.8	-819.0	-0.0	22463.8	0.270	0.368	0.270	0.0	0.0	0.0	0.000
				7	21980.0	-665.8	-0.0	21980.0	0.263	0.359	0.263	0.0	0.0	0.0	0.000
				8	21754.5	-578.3	-0.0	21754.5	0.260	0.355	0.260	0.0	0.0	0.0	0.000
				9	21901.4	-571.0	-0.0	21901.4	0.261	0.357	0.261	0.0	0.0	0.0	0.000

				10	21712.2	-527.3	-0.0	21712.2	0.259	0.354	0.259	0.0	0.0	0.0	0.000
				11	22715.0	-840.1	-0.0	22715.0	0.273	0.373	0.273	0.0	0.0	0.0	0.000
				12	22434.7	-731.3	-0.0	22434.7	0.269	0.367	0.269	0.0	0.0	0.0	0.000
				13	22767.6	-903.6	-0.0	22767.6	0.274	0.374	0.274	0.0	0.0	0.0	0.000
				14	22532.2	-849.1	-0.0	22532.2	0.271	0.370	0.271	0.0	0.0	0.0	0.000
				15	21930.6	-658.8	-0.0	21930.6	0.262	0.359	0.262	0.0	0.0	0.0	0.000
				16	21650.2	-550.0	-0.0	21650.2	0.258	0.353	0.258	0.0	0.0	0.0	0.000
				17	21833.0	-540.9	-0.0	21833.0	0.260	0.356	0.260	0.0	0.0	0.0	0.000
				18	21597.7	-486.5	-0.0	21597.7	0.257	0.352	0.257	0.0	0.0	0.0	0.000
				24	22340.8	-738.2	-0.0	22340.8	0.268	0.366	0.268	0.0	0.0	0.0	0.000
				25	22257.6	-705.9	-0.0	22257.6	0.266	0.364	0.266	0.0	0.0	0.0	0.000
				26	22356.3	-756.9	-0.0	22356.3	0.268	0.366	0.268	0.0	0.0	0.0	0.000
				27	22286.3	-740.8	-0.0	22286.3	0.267	0.365	0.267	0.0	0.0	0.0	0.000
				28	22107.7	-684.2	-0.0	22107.7	0.264	0.362	0.264	0.0	0.0	0.0	0.000
				29	22024.5	-652.0	-0.0	22024.5	0.263	0.360	0.263	0.0	0.0	0.0	0.000
				30	22078.9	-649.4	-0.0	22078.9	0.264	0.361	0.264	0.0	0.0	0.0	0.000
				31	22009.0	-633.2	-0.0	22009.0	0.263	0.360	0.263	0.0	0.0	0.0	0.000
				32	22539.6	-793.9	-0.0	22539.6	0.270	0.369	0.270	0.0	0.0	0.0	0.000
				33	22355.8	-723.3	-0.0	22355.8	0.268	0.366	0.268	0.0	0.0	0.0	0.000
				34	22568.5	-831.8	-0.0	22568.5	0.271	0.370	0.271	0.0	0.0	0.0	0.000
				35	22409.5	-793.6	-0.0	22409.5	0.269	0.367	0.269	0.0	0.0	0.0	0.000
				36	22009.5	-666.8	-0.0	22009.5	0.263	0.360	0.263	0.0	0.0	0.0	0.000
				37	21825.7	-596.1	-0.0	21825.7	0.261	0.356	0.261	0.0	0.0	0.0	0.000
				38	21955.8	-596.4	-0.0	21955.8	0.262	0.358	0.262	0.0	0.0	0.0	0.000
				39	21796.8	-558.2	-0.0	21796.8	0.260	0.355	0.260	0.0	0.0	0.0	0.000
10,11	0.90	3.35	0.50	3	19392.8	-81.5	-0.0	19392.8	0.246	0.336	0.246	0.0	0.0	0.0	0.000

				4	19392.4	19.1	0.0	19392.4	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				5	19364.4	-139.8	-0.0	19364.4	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				6	19339.7	-89.1	-0.0	19339.7	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				7	19310.4	87.5	0.0	19310.4	0.245	0.334	0.245	0.0	0.0	0.0	0.000
				8	19310.0	188.0	0.0	19310.0	0.246	0.335	0.246	0.0	0.0	0.0	0.000
				9	19363.1	195.7	0.0	19363.1	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				10	19338.4	246.4	0.0	19338.4	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				11	19402.9	-114.3	-0.0	19402.9	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				12	19402.4	10.8	0.0	19402.4	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				13	19367.6	-186.8	-0.0	19367.6	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				14	19336.8	-123.8	-0.0	19336.8	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				15	19300.4	95.8	0.0	19300.4	0.245	0.334	0.245	0.0	0.0	0.0	0.000
				16	19299.9	220.9	0.0	19299.9	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				17	19366.0	230.3	0.0	19366.0	0.247	0.337	0.247	0.0	0.0	0.0	0.000
				18	19335.3	293.4	0.0	19335.3	0.247	0.337	0.247	0.0	0.0	0.0	0.000
				24	19366.7	3.5	0.0	19366.7	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				25	19366.6	40.6	0.0	19366.6	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				26	19356.2	-18.0	-0.0	19356.2	0.245	0.334	0.245	0.0	0.0	0.0	0.000
				27	19347.1	0.7	0.0	19347.1	0.245	0.334	0.245	0.0	0.0	0.0	0.000
				28	19336.3	65.9	0.0	19336.3	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				29	19336.1	103.1	0.0	19336.1	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				30	19355.7	105.9	0.0	19355.7	0.246	0.335	0.246	0.0	0.0	0.0	0.000
				31	19346.6	124.6	0.0	19346.6	0.246	0.335	0.246	0.0	0.0	0.0	0.000
				32	19386.2	-58.4	-0.0	19386.2	0.246	0.335	0.246	0.0	0.0	0.0	0.000
				33	19386.1	25.0	0.0	19386.1	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				34	19362.0	-106.4	-0.0	19362.0	0.246	0.335	0.246	0.0	0.0	0.0	0.000

				35	19341.1	-64.4	-0.0	19341.1	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				36	19316.7	81.7	0.0	19316.7	0.245	0.334	0.245	0.0	0.0	0.0	0.000
				37	19316.6	164.9	0.0	19316.6	0.245	0.335	0.245	0.0	0.0	0.0	0.000
				38	19361.7	170.9	0.0	19361.7	0.246	0.336	0.246	0.0	0.0	0.0	0.000
				39	19340.8	213.0	0.0	19340.8	0.246	0.336	0.246	0.0	0.0	0.0	0.000
8,9	0.90	5.16	0.50	3	36276.8	2732.5	0.0	36276.8	0.311	0.426	0.311	0.0	0.0	0.0	0.000
				4	38870.2	3268.4	0.0	38870.2	0.334	0.458	0.334	0.0	0.0	0.0	0.000
				5	32773.1	1874.1	0.0	32773.1	0.279	0.383	0.279	0.0	0.0	0.0	0.000
				6	32363.4	1674.1	0.0	32363.4	0.275	0.377	0.275	0.0	0.0	0.0	0.000
				7	34911.1	2066.1	0.0	34911.1	0.297	0.408	0.297	0.0	0.0	0.0	0.000
				8	37504.5	2602.1	0.0	37504.5	0.320	0.440	0.320	0.0	0.0	0.0	0.000
				9	41417.9	3660.3	0.0	41417.9	0.356	0.489	0.356	0.0	0.0	0.0	0.000
				10	41008.2	3460.5	0.0	41008.2	0.352	0.484	0.352	0.0	0.0	0.0	0.000
				11	36127.7	2748.0	0.0	36127.7	0.309	0.425	0.309	0.0	0.0	0.0	0.000
				12	39352.9	3414.5	0.0	39352.9	0.338	0.465	0.338	0.0	0.0	0.0	0.000
				13	31770.2	1680.7	0.0	31770.2	0.270	0.370	0.270	0.0	0.0	0.0	0.000
				14	31260.4	1432.3	0.0	31260.4	0.265	0.363	0.265	0.0	0.0	0.0	0.000
				15	34428.4	1920.1	0.0	34428.4	0.293	0.402	0.293	0.0	0.0	0.0	0.000
				16	37653.6	2586.5	0.0	37653.6	0.322	0.441	0.322	0.0	0.0	0.0	0.000
				17	42520.9	3902.2	0.0	42520.9	0.366	0.503	0.366	0.0	0.0	0.0	0.000
				18	42011.1	3653.8	0.0	42011.1	0.361	0.496	0.361	0.0	0.0	0.0	0.000
				24	36664.1	2691.2	0.0	36664.1	0.314	0.431	0.314	0.0	0.0	0.0	0.000
				25	37621.9	2889.1	0.0	37621.9	0.322	0.442	0.322	0.0	0.0	0.0	0.000
				26	35370.2	2374.3	0.0	35370.2	0.302	0.414	0.302	0.0	0.0	0.0	0.000
				27	35218.8	2300.5	0.0	35218.8	0.300	0.412	0.300	0.0	0.0	0.0	0.000
				28	36159.5	2445.4	0.0	36159.5	0.309	0.424	0.309	0.0	0.0	0.0	0.000

				29	37117.2	2643.2	0.0	37117.2	0.317	0.436	0.317	0.0	0.0	0.0	0.000
				30	38562.6	3033.9	0.0	38562.6	0.331	0.454	0.331	0.0	0.0	0.0	0.000
				31	38411.2	2960.2	0.0	38411.2	0.329	0.452	0.329	0.0	0.0	0.0	0.000
				32	36393.2	2710.2	0.0	36393.2	0.312	0.428	0.312	0.0	0.0	0.0	0.000
				33	38543.5	3154.0	0.0	38543.5	0.331	0.454	0.331	0.0	0.0	0.0	0.000
				34	33480.0	2006.8	0.0	33480.0	0.285	0.391	0.285	0.0	0.0	0.0	0.000
				35	33133.4	1847.9	0.0	33133.4	0.282	0.387	0.282	0.0	0.0	0.0	0.000
				36	35237.8	2180.4	0.0	35237.8	0.300	0.412	0.300	0.0	0.0	0.0	0.000
				37	37388.1	2624.3	0.0	37388.1	0.320	0.439	0.320	0.0	0.0	0.0	0.000
				38	40647.9	3486.6	0.0	40647.9	0.349	0.480	0.349	0.0	0.0	0.0	0.000
				39	40301.3	3327.6	0.0	40301.3	0.346	0.475	0.346	0.0	0.0	0.0	0.000
7,8	0.90	5.48	0.50	3	43349.7	4887.6	0.0	43349.7	0.354	0.487	0.354	0.0	0.0	0.0	0.000
				4	48955.7	8127.0	0.0	48955.7	0.408	0.560	0.408	0.0	0.0	0.0	0.000
				5	35572.8	299.3	0.0	35572.8	0.280	0.384	0.280	0.0	0.0	0.0	0.000
				6	34512.8	-394.2	-0.0	34512.8	0.272	0.373	0.272	0.0	0.0	0.0	0.000
				7	39816.5	2575.9	0.0	39816.5	0.320	0.439	0.320	0.0	0.0	0.0	0.000
				8	45422.5	5815.3	0.0	45422.5	0.373	0.513	0.373	0.0	0.0	0.0	0.000
				9	54259.4	11097.1	0.0	54259.4	0.459	0.630	0.459	0.0	0.0	0.0	0.000
				10	53199.5	10403.6	0.0	53199.5	0.449	0.616	0.449	0.0	0.0	0.0	0.000
				11	43097.4	4774.5	0.0	43097.4	0.352	0.483	0.352	0.0	0.0	0.0	0.000
				12	50069.0	8803.0	0.0	50069.0	0.419	0.575	0.419	0.0	0.0	0.0	0.000
				13	33425.8	-931.5	-0.0	33425.8	0.265	0.364	0.265	0.0	0.0	0.0	0.000
				14	32107.6	-1793.8	-0.0	32107.6	0.257	0.353	0.257	0.0	0.0	0.0	0.000
				15	38703.2	1899.9	0.0	38703.2	0.309	0.424	0.309	0.0	0.0	0.0	0.000
				16	45674.8	5928.4	0.0	45674.8	0.376	0.516	0.376	0.0	0.0	0.0	0.000
				17	56664.7	12496.7	0.0	56664.7	0.482	0.662	0.482	0.0	0.0	0.0	0.000

				18	55346.4	11634.3	0.0	55346.4	0.469	0.644	0.469	0.0	0.0	0.0	0.000
				24	44003.4	5180.0	0.0	44003.4	0.360	0.495	0.360	0.0	0.0	0.0	0.000
				25	46073.7	6376.3	0.0	46073.7	0.380	0.522	0.380	0.0	0.0	0.0	0.000
				26	41131.5	3485.8	0.0	41131.5	0.333	0.457	0.333	0.0	0.0	0.0	0.000
				27	40740.0	3229.7	0.0	40740.0	0.329	0.452	0.329	0.0	0.0	0.0	0.000
				28	42698.6	4326.5	0.0	42698.6	0.347	0.477	0.347	0.0	0.0	0.0	0.000
				29	44768.8	5522.8	0.0	44768.8	0.367	0.504	0.367	0.0	0.0	0.0	0.000
				30	48032.2	7473.2	0.0	48032.2	0.399	0.548	0.399	0.0	0.0	0.0	0.000
				31	47640.7	7217.1	0.0	47640.7	0.395	0.542	0.395	0.0	0.0	0.0	0.000
				32	43530.5	4962.4	0.0	43530.5	0.356	0.489	0.356	0.0	0.0	0.0	0.000
				33	48178.4	7647.5	0.0	48178.4	0.401	0.550	0.401	0.0	0.0	0.0	0.000
				34	37080.0	1162.3	0.0	37080.0	0.294	0.404	0.294	0.0	0.0	0.0	0.000
				35	36199.1	590.1	0.0	36199.1	0.286	0.392	0.286	0.0	0.0	0.0	0.000
				36	40593.8	3055.3	0.0	40593.8	0.327	0.449	0.327	0.0	0.0	0.0	0.000
				37	45241.8	5740.4	0.0	45241.8	0.372	0.510	0.372	0.0	0.0	0.0	0.000
				38	52573.2	10112.7	0.0	52573.2	0.443	0.608	0.443	0.0	0.0	0.0	0.000
				39	51692.2	9540.6	0.0	51692.2	0.434	0.596	0.434	0.0	0.0	0.0	0.000
5,6	0.90	6.45	0.50	3	39732.1	4928.7	0.0	39732.1	0.276	0.380	0.276	0.0	0.0	0.0	0.000
				4	45354.8	1934.2	0.0	45354.8	0.307	0.423	0.307	0.0	0.0	0.0	0.000
				5	39081.9	1088.0	0.0	39081.9	0.264	0.363	0.264	0.0	0.0	0.0	0.000
				6	44147.3	-5198.6	-0.0	44147.3	0.306	0.421	0.306	0.0	0.0	0.0	0.000
				7	56616.9	-16026.5	-0.0	56616.9	0.414	0.570	0.414	0.0	0.0	0.0	0.000
				8	62239.6	-19020.7	-0.0	62239.6	0.459	0.631	0.459	0.0	0.0	0.0	0.000
				9	57824.3	-8893.2	-0.0	57824.3	0.406	0.558	0.406	0.0	0.0	0.0	0.000
				10	62889.8	-15180.0	-0.0	62889.8	0.454	0.624	0.454	0.0	0.0	0.0	0.000
				11	36995.1	7839.0	0.0	36995.1	0.264	0.364	0.264	0.0	0.0	0.0	0.000

				12	43987.7	4114.7	0.0	43987.7	0.303	0.416	0.303	0.0	0.0	0.0	0.000
				13	36183.1	3068.0	0.0	36183.1	0.248	0.342	0.248	0.0	0.0	0.0	0.000
				14	42479.8	-4745.7	-0.0	42479.8	0.294	0.404	0.294	0.0	0.0	0.0	0.000
				15	57983.9	-18206.7	-0.0	57983.9	0.429	0.589	0.429	0.0	0.0	0.0	0.000
				16	64976.6	-21931.0	-0.0	64976.6	0.484	0.666	0.484	0.0	0.0	0.0	0.000
				17	59491.9	-9346.2	-0.0	59491.9	0.418	0.575	0.418	0.0	0.0	0.0	0.000
				18	65788.6	-17160.3	-0.0	65788.6	0.478	0.657	0.478	0.0	0.0	0.0	0.000
				24	46832.9	-2628.5	-0.0	46832.9	0.319	0.438	0.319	0.0	0.0	0.0	0.000
				25	48909.6	-3734.8	-0.0	48909.6	0.335	0.461	0.335	0.0	0.0	0.0	0.000
				26	46590.3	-4042.6	-0.0	46590.3	0.320	0.440	0.320	0.0	0.0	0.0	0.000
				27	48459.1	-6361.3	-0.0	48459.1	0.338	0.464	0.338	0.0	0.0	0.0	0.000
				28	53062.1	-10357.2	-0.0	53062.1	0.377	0.519	0.377	0.0	0.0	0.0	0.000
				29	55138.8	-11463.7	-0.0	55138.8	0.394	0.541	0.394	0.0	0.0	0.0	0.000
				30	53512.6	-7730.8	-0.0	53512.6	0.374	0.515	0.374	0.0	0.0	0.0	0.000
				31	55381.3	-10049.3	-0.0	55381.3	0.392	0.539	0.392	0.0	0.0	0.0	0.000
				32	41816.7	2641.4	0.0	41816.7	0.285	0.392	0.285	0.0	0.0	0.0	0.000
				33	46490.4	132.0	0.0	46490.4	0.311	0.428	0.311	0.0	0.0	0.0	0.000
				34	41146.6	-333.9	-0.0	41146.6	0.276	0.380	0.276	0.0	0.0	0.0	0.000
				35	45246.0	-5393.6	-0.0	45246.0	0.314	0.432	0.314	0.0	0.0	0.0	0.000
				36	55481.3	-14224.0	-0.0	55481.3	0.402	0.553	0.402	0.0	0.0	0.0	0.000
				37	60155.0	-16732.9	-0.0	60155.0	0.439	0.604	0.439	0.0	0.0	0.0	0.000
				38	56725.6	-8698.5	-0.0	56725.6	0.398	0.547	0.398	0.0	0.0	0.0	0.000
				39	60825.0	-13758.3	-0.0	60825.0	0.437	0.601	0.437	0.0	0.0	0.0	0.000
4,5	0.90	3.61	0.50	3	28231.6	-149.8	-0.0	28231.6	0.333	0.455	0.333	0.0	0.0	0.0	0.000
				4	30745.7	-148.6	-0.0	30745.7	0.363	0.496	0.363	0.0	0.0	0.0	0.000
				5	25866.3	2.8	0.0	25866.3	0.304	0.416	0.304	0.0	0.0	0.0	0.000

				6	26352.9	135.0	0.0	26352.9	0.311	0.425	0.311	0.0	0.0	0.0	0.000
				7	29853.8	290.5	0.0	29853.8	0.353	0.483	0.353	0.0	0.0	0.0	0.000
				8	32367.9	291.8	0.0	32367.9	0.383	0.523	0.383	0.0	0.0	0.0	0.000
				9	34246.6	6.9	0.0	34246.6	0.403	0.551	0.403	0.0	0.0	0.0	0.000
				10	34733.3	139.0	0.0	34733.3	0.410	0.560	0.410	0.0	0.0	0.0	0.000
				11	27727.8	-203.5	-0.0	27727.8	0.328	0.448	0.328	0.0	0.0	0.0	0.000
				12	30854.2	-201.9	-0.0	30854.2	0.364	0.498	0.364	0.0	0.0	0.0	0.000
				13	24786.4	-13.8	-0.0	24786.4	0.292	0.399	0.292	0.0	0.0	0.0	0.000
				14	25391.6	150.4	0.0	25391.6	0.300	0.410	0.300	0.0	0.0	0.0	0.000
				15	29745.3	343.8	0.0	29745.3	0.352	0.481	0.352	0.0	0.0	0.0	0.000
				16	32871.8	345.4	0.0	32871.8	0.389	0.532	0.389	0.0	0.0	0.0	0.000
				17	35207.9	-8.5	-0.0	35207.9	0.414	0.567	0.414	0.0	0.0	0.0	0.000
				18	35813.2	155.5	0.0	35813.2	0.422	0.577	0.422	0.0	0.0	0.0	0.000
				24	29536.0	-10.5	-0.0	29536.0	0.348	0.475	0.348	0.0	0.0	0.0	0.000
				25	30464.3	-10.0	-0.0	30464.3	0.358	0.490	0.358	0.0	0.0	0.0	0.000
				26	28662.7	45.7	0.0	28662.7	0.338	0.462	0.338	0.0	0.0	0.0	0.000
				27	28842.5	94.5	0.0	28842.5	0.340	0.465	0.340	0.0	0.0	0.0	0.000
				28	30135.3	151.9	0.0	30135.3	0.356	0.486	0.356	0.0	0.0	0.0	0.000
				29	31063.6	152.4	0.0	31063.6	0.366	0.501	0.366	0.0	0.0	0.0	0.000
				30	31757.0	47.4	0.0	31757.0	0.374	0.511	0.374	0.0	0.0	0.0	0.000
				31	31936.8	96.1	0.0	31936.8	0.376	0.515	0.376	0.0	0.0	0.0	0.000
				32	28581.5	-107.9	-0.0	28581.5	0.337	0.461	0.337	0.0	0.0	0.0	0.000
				33	30660.7	-103.8	-0.0	30660.7	0.361	0.494	0.361	0.0	0.0	0.0	0.000
				34	26630.9	11.1	0.0	26630.9	0.313	0.429	0.313	0.0	0.0	0.0	0.000
				35	27038.1	117.2	0.0	27038.1	0.319	0.436	0.319	0.0	0.0	0.0	0.000
				36	29938.8	245.7	0.0	29938.8	0.354	0.484	0.354	0.0	0.0	0.0	0.000

				37	32018.0	249.8	0.0	32018.0	0.378	0.517	0.378	0.0	0.0	0.0	0.000
				38	33561.5	24.9	0.0	33561.5	0.395	0.540	0.395	0.0	0.0	0.0	0.000
				39	33968.7	130.8	0.0	33968.7	0.400	0.548	0.400	0.0	0.0	0.0	0.000
3,4	0.90	3.35	0.50	3	26174.1	-122.7	-0.0	26174.1	0.332	0.453	0.332	0.0	0.0	0.0	0.000
				4	28604.9	24.8	0.0	28604.9	0.362	0.494	0.362	0.0	0.0	0.0	0.000
				5	23874.0	-104.3	-0.0	23874.0	0.303	0.413	0.303	0.0	0.0	0.0	0.000
				6	24333.3	58.6	0.0	24333.3	0.308	0.421	0.308	0.0	0.0	0.0	0.000
				7	27705.1	420.8	0.0	27705.1	0.353	0.483	0.353	0.0	0.0	0.0	0.000
				8	30135.9	568.0	0.0	30135.9	0.385	0.526	0.385	0.0	0.0	0.0	0.000
				9	31976.7	386.8	0.0	31976.7	0.407	0.556	0.407	0.0	0.0	0.0	0.000
				10	32436.0	549.7	0.0	32436.0	0.414	0.566	0.414	0.0	0.0	0.0	0.000
				11	25691.6	-206.7	-0.0	25691.6	0.326	0.446	0.326	0.0	0.0	0.0	0.000
				12	28714.6	-23.6	-0.0	28714.6	0.363	0.496	0.363	0.0	0.0	0.0	0.000
				13	22831.2	-184.0	-0.0	22831.2	0.290	0.396	0.290	0.0	0.0	0.0	0.000
				14	23402.3	18.8	0.0	23402.3	0.296	0.404	0.296	0.0	0.0	0.0	0.000
				15	27595.5	469.0	0.0	27595.5	0.352	0.481	0.352	0.0	0.0	0.0	0.000
				16	30618.4	652.2	0.0	30618.4	0.392	0.535	0.392	0.0	0.0	0.0	0.000
				17	32907.7	426.7	0.0	32907.7	0.419	0.573	0.419	0.0	0.0	0.0	0.000
				18	33478.9	629.5	0.0	33478.9	0.428	0.584	0.428	0.0	0.0	0.0	0.000
				24	27423.6	95.2	0.0	27423.6	0.347	0.475	0.347	0.0	0.0	0.0	0.000
				25	28321.2	149.6	0.0	28321.2	0.359	0.491	0.359	0.0	0.0	0.0	0.000
				26	26574.2	102.0	0.0	26574.2	0.337	0.460	0.337	0.0	0.0	0.0	0.000
				27	26743.7	162.2	0.0	26743.7	0.339	0.464	0.339	0.0	0.0	0.0	0.000
				28	27988.8	295.8	0.0	27988.8	0.356	0.486	0.356	0.0	0.0	0.0	0.000
				29	28886.5	350.2	0.0	28886.5	0.368	0.502	0.368	0.0	0.0	0.0	0.000
				30	29566.3	283.3	0.0	29566.3	0.376	0.513	0.376	0.0	0.0	0.0	0.000

				31	29735.9	343.5	0.0	29735.9	0.379	0.517	0.379	0.0	0.0	0.0	0.000
				32	26515.3	-64.0	-0.0	26515.3	0.336	0.459	0.336	0.0	0.0	0.0	0.000
				33	28530.0	58.0	0.0	28530.0	0.361	0.493	0.361	0.0	0.0	0.0	0.000
				34	24607.4	-48.4	-0.0	24607.4	0.312	0.425	0.312	0.0	0.0	0.0	0.000
				35	24986.8	87.1	0.0	24986.8	0.317	0.432	0.317	0.0	0.0	0.0	0.000
				36	27780.0	387.5	0.0	27780.0	0.354	0.484	0.354	0.0	0.0	0.0	0.000
				37	29794.8	509.6	0.0	29794.8	0.380	0.520	0.380	0.0	0.0	0.0	0.000
				38	31323.2	358.5	0.0	31323.2	0.399	0.545	0.399	0.0	0.0	0.0	0.000
				39	31702.6	493.8	0.0	31702.6	0.404	0.552	0.404	0.0	0.0	0.0	0.000
2,3	0.90	3.66	0.50	3	29095.3	-211.4	-0.0	29095.3	0.339	0.464	0.339	0.0	0.0	0.0	0.000
				4	32286.9	-42.1	-0.0	32286.9	0.375	0.513	0.375	0.0	0.0	0.0	0.000
				5	26200.0	-145.1	-0.0	26200.0	0.305	0.417	0.305	0.0	0.0	0.0	0.000
				6	26909.8	81.3	0.0	26909.8	0.313	0.428	0.313	0.0	0.0	0.0	0.000
				7	31461.5	542.7	0.0	31461.5	0.369	0.504	0.369	0.0	0.0	0.0	0.000
				8	34653.1	712.0	0.0	34653.1	0.407	0.556	0.407	0.0	0.0	0.0	0.000
				9	36838.5	419.4	0.0	36838.5	0.430	0.588	0.430	0.0	0.0	0.0	0.000
				10	37548.4	645.8	0.0	37548.4	0.440	0.602	0.440	0.0	0.0	0.0	0.000
				11	28418.3	-323.9	-0.0	28418.3	0.332	0.454	0.332	0.0	0.0	0.0	0.000
				12	32387.3	-113.3	-0.0	32387.3	0.377	0.515	0.377	0.0	0.0	0.0	0.000
				13	24817.7	-241.3	-0.0	24817.7	0.290	0.396	0.290	0.0	0.0	0.0	0.000
				14	25700.5	40.0	0.0	25700.5	0.299	0.408	0.299	0.0	0.0	0.0	0.000
				15	31361.0	614.0	0.0	31361.0	0.368	0.503	0.368	0.0	0.0	0.0	0.000
				16	35330.1	824.6	0.0	35330.1	0.415	0.568	0.415	0.0	0.0	0.0	0.000
				17	38047.9	460.6	0.0	38047.9	0.445	0.608	0.445	0.0	0.0	0.0	0.000
				18	38930.7	742.0	0.0	38930.7	0.457	0.624	0.457	0.0	0.0	0.0	0.000
				24	30847.9	79.9	0.0	30847.9	0.359	0.490	0.359	0.0	0.0	0.0	0.000

				25	32026.5	142.4	0.0	32026.5	0.373	0.510	0.373	0.0	0.0	0.0	0.000
				26	29778.8	104.4	0.0	29778.8	0.346	0.474	0.346	0.0	0.0	0.0	0.000
				27	30040.9	188.0	0.0	30040.9	0.350	0.479	0.350	0.0	0.0	0.0	0.000
				28	31721.8	358.3	0.0	31721.8	0.371	0.507	0.371	0.0	0.0	0.0	0.000
				29	32900.4	420.9	0.0	32900.4	0.385	0.526	0.385	0.0	0.0	0.0	0.000
				30	33707.4	312.7	0.0	33707.4	0.393	0.538	0.393	0.0	0.0	0.0	0.000
				31	33969.6	396.3	0.0	33969.6	0.397	0.543	0.397	0.0	0.0	0.0	0.000
				32	29568.2	-130.6	-0.0	29568.2	0.344	0.471	0.344	0.0	0.0	0.0	0.000
				33	32214.6	9.3	0.0	32214.6	0.374	0.512	0.374	0.0	0.0	0.0	0.000
				34	27168.7	-76.2	-0.0	27168.7	0.316	0.432	0.316	0.0	0.0	0.0	0.000
				35	27758.4	110.4	0.0	27758.4	0.323	0.442	0.323	0.0	0.0	0.0	0.000
				36	31533.7	491.4	0.0	31533.7	0.369	0.505	0.369	0.0	0.0	0.0	0.000
				37	34180.1	631.3	0.0	34180.1	0.401	0.548	0.401	0.0	0.0	0.0	0.000
				38	35990.0	390.3	0.0	35990.0	0.420	0.575	0.420	0.0	0.0	0.0	0.000
				39	36579.6	577.0	0.0	36579.6	0.428	0.586	0.428	0.0	0.0	0.0	0.000
1,2	0.90	6.39	0.50	3	47137.2	-517.0	-0.0	47137.2	0.319	0.439	0.319	0.0	0.0	0.0	0.000
				4	51846.3	-307.5	-0.0	51846.3	0.351	0.482	0.351	0.0	0.0	0.0	0.000
				5	40919.1	-1212.4	-0.0	40919.1	0.279	0.383	0.279	0.0	0.0	0.0	0.000
				6	40298.6	-1598.9	-0.0	40298.6	0.275	0.379	0.275	0.0	0.0	0.0	0.000
				7	45068.7	-1805.3	-0.0	45068.7	0.308	0.424	0.308	0.0	0.0	0.0	0.000
				8	49777.9	-1595.8	-0.0	49777.9	0.339	0.467	0.339	0.0	0.0	0.0	0.000
				9	56616.4	-513.8	-0.0	56616.4	0.383	0.527	0.383	0.0	0.0	0.0	0.000
				10	55995.9	-900.2	-0.0	55995.9	0.380	0.522	0.380	0.0	0.0	0.0	0.000
				11	46815.8	-385.9	-0.0	46815.8	0.317	0.436	0.317	0.0	0.0	0.0	0.000
				12	52672.1	-125.3	-0.0	52672.1	0.356	0.489	0.356	0.0	0.0	0.0	0.000
				13	39082.8	-1250.6	-0.0	39082.8	0.266	0.366	0.266	0.0	0.0	0.0	0.000

				14	38311.0	-1731.0	-0.0	38311.0	0.262	0.361	0.262	0.0	0.0	0.0	0.000
				15	44242.9	-1987.5	-0.0	44242.9	0.303	0.416	0.303	0.0	0.0	0.0	0.000
				16	50099.3	-1726.9	-0.0	50099.3	0.342	0.470	0.342	0.0	0.0	0.0	0.000
				17	58604.0	-381.7	-0.0	58604.0	0.396	0.545	0.396	0.0	0.0	0.0	0.000
				18	57832.2	-862.3	-0.0	57832.2	0.392	0.539	0.392	0.0	0.0	0.0	0.000
				24	47970.1	-857.3	-0.0	47970.1	0.326	0.448	0.326	0.0	0.0	0.0	0.000
				25	49709.1	-779.9	-0.0	49709.1	0.337	0.464	0.337	0.0	0.0	0.0	0.000
				26	45673.7	-1114.1	-0.0	45673.7	0.311	0.427	0.311	0.0	0.0	0.0	0.000
				27	45444.5	-1256.6	-0.0	45444.5	0.309	0.426	0.309	0.0	0.0	0.0	0.000
				28	47205.9	-1332.8	-0.0	47205.9	0.321	0.442	0.321	0.0	0.0	0.0	0.000
				29	48945.0	-1255.4	-0.0	48945.0	0.333	0.458	0.333	0.0	0.0	0.0	0.000
				30	51470.5	-856.1	-0.0	51470.5	0.349	0.480	0.349	0.0	0.0	0.0	0.000
				31	51241.3	-998.8	-0.0	51241.3	0.348	0.479	0.348	0.0	0.0	0.0	0.000
				32	47370.8	-617.5	-0.0	47370.8	0.321	0.442	0.321	0.0	0.0	0.0	0.000
				33	51275.9	-445.0	-0.0	51275.9	0.347	0.477	0.347	0.0	0.0	0.0	0.000
				34	42208.8	-1186.6	-0.0	42208.8	0.287	0.395	0.287	0.0	0.0	0.0	0.000
				35	41689.3	-1501.6	-0.0	41689.3	0.285	0.391	0.285	0.0	0.0	0.0	0.000
				36	45639.2	-1667.8	-0.0	45639.2	0.312	0.429	0.312	0.0	0.0	0.0	0.000
				37	49544.2	-1495.2	-0.0	49544.2	0.338	0.464	0.338	0.0	0.0	0.0	0.000
				38	55225.7	-611.1	-0.0	55225.7	0.374	0.514	0.374	0.0	0.0	0.0	0.000
				39	54706.2	-926.2	-0.0	54706.2	0.371	0.511	0.371	0.0	0.0	0.0	0.000